## Appendix C: Traffic Technical Report

# EXIT 4A - Traffic and Transportation Technical Report 

# I-93 Exit 4A Supplemental Draft Environmental Impact Statement 

Prepared for:
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### 1.0 Introduction

The Interstate 93 (I-93) Exit 4A Project (the "Project") involves a new diamond interchange between Interstate 93 Exits 4 and 5 in the Town of Londonderry, approximately one mile north of Exit 4. The new diamond interchange would provide access to the east side of I-93 only. A 1-mile connector roadway would be built on new alignment from the interchange to Folsom Road, near the intersection of North High Street and Madden Road, in the Town of Derry. Folsom Road, and subsequently Tsienneto Road, would be upgraded, and the intersections would be improved.

The Project was the subject of a Draft Environmental Impact Statement (DEIS) in 2007 (FHWA, 2007). Due to the amount of time that has elapsed since the 2007 DEIS, the FHWA has requested the preparation of updated studies that will be documented in a Supplemental Draft Environmental Impact Statement (SDEIS) in accordance with the National Environmental Policy Act (NEPA). The SDEIS will provide an up-to-date assessment of the environmental effects of the Project and the evaluation of reasonable alternatives that will consider updated information including, but not limited to, traffic, socioeconomic projections, land development proposals in the project area, and changes in environmental resources and regulatory requirements.

The purpose of this report is to document the development of traffic projections and operational analyses for the Project as part of the SDEIS. This report is a compilation of previous memoranda issued as the project proceeded as well as to present the findings of the analyses of the various alternatives.

The traffic analysis tasks described in this report includes the following:

- Collection of traffic count data at various roadways and intersections in the Exit 4A study area to develop 2015 Average Weekday Traffic (AWDT) volumes.
- Use of these 2015 counts to calibrate the Southern New Hampshire Planning Commission (SNHPC)'s regional traffic model to be viable to project future traffic volumes in the 2040 design year with and without the proposed Exit 4A.
- Preparation of land use and socioeconomic projections (conducted concurrently by the Land Use Working Group) for the SNHPC model area and allocated to the Traffic Analysis Zone (TAZ) level for each alternative scenario to be used as the basis for traffic generation and trip assignments to the regional roadway network.
- Development of 2040 No-Build (without Exit 4A) and Build (with Exit 4A) traffic volume assignments on key roadway segments and intersections in the study area network.
- Derivation of AM and PM peak hour traffic volumes on the mainline I-93 and interchange ramps as well as key segments and intersections in the study area for the various Exit 4A alternative layouts for analysis purposes (see Figure 1).
- Analysis of interstate operations using the 2010 Highway Capacity Manual (TRB, 2010) Freeway Facilities methodologies for the existing 2015 and all 2040 NoBuild and Build scenarios. Analysis of signalized and unsignalized intersection operations of the existing 2015 and all 2040 scenarios using HCM methodologies and emulated in the SYNCHRO/Sim-Traffic (Trafficware, 2016)software for
derivation of Level of Service and estimated queue lengths for conceptual design purposes.

In addition to the traffic data collection, Project Team specialists and the Land Use Working Group conducted interviews and compiled socioeconomic (e.g., population and employment) projections that were used by the SNHPC to allocate these trip-generation characteristics to their traffic zone system to generate traffic assignments to the roadway network under both No-Build (without 4A) and the Build alternatives that were included in the DEIS from 2007. A separate Land Use Scenario Technical Report was prepared that documents the land use and socioeconomic forecasting efforts that were used in conjunction with the traffic modeling. (Louis Berger, 2017).

### 2.0 Purpose and Need for the Project

The Purpose and Need for the Project, as described in the 2007 DEIS, is as follows:

- Providing for transportation improvements that will promote the safe and efficient movement of people, goods, and services between I-93 and the towns served by NH Route 102, specifically Derry and Londonderry, that are immediately adjacent to I-93 Exit 4;
- Providing an alternative route to the Interstate system for traffic using NH Route 102 to and from the east, thus removing a large volume of through traffic from the heavily congested downtown Derry street network;
- Providing improved Interstate access for commercially and industrially zoned lands near NH Routes 28 and 102 in both Derry and Londonderry, thus allowing for the planned and orderly development of such lands to further locally-defined economic development goals and tax base diversification; and
- Enhancing and promoting the economic vitality of the downtown Derry area, presently characterized by traffic congestion and decreasing vehicular and pedestrian safety, by separating local destination-oriented traffic from throughtraffic destined for the Interstate system.

For purposes of this project, the downtown Derry area has been defined as NH Route 102 easterly from its intersection with Fordway to the NH 28 (Crystal Avenue/Birch Street) intersection (CLD|Fuss \& O'Neill, 2018). This is also consistent with the defined Central Business District zoning map for the Town of Derry (Town of Derry, 2015).

### 3.0 Traffic Data Collection

The study area for the Project was established and agreed upon as part of the 2007 DEIS document, and encompasses the expected extent of the roadway network that would likely be influenced by the introduction of a new I-93 interchange and associated connector roadways. An updated inventory of the key area roadways and intersections was conducted to ensure that the traffic modeling and subsequent analyses reflect existing conditions.

The various contracts for the I-93 widening project affecting the study area also needed to be considered. The Exit 5 improvements are already in place, and the Exit 4 interchange is being reconstructed now as part of Contract 14633-D. The widening of the mainline I93 to four lanes between Exits 4 and 5 under Contracts 'D' and ' $I$ ' is also underway.

### 3.1 Traffic Counts

The traffic counting program was developed for the project, based on the key roadway segments and intersections in the study area, to assist in the development of 2015 base Average Annual Weekday Traffic (AAWDT) volumes for use in the traffic model calibration. Most of these locations were counted in 2005 as part of the preparation of the original 2007 DEIS document. This effort was coordinated with the annual traffic counting programs conducted by both the NHDOT and SNHPC within the study area, and the new data collected in May and June of 2016 while school was still in session. Some of these locations had already been counted in 2014 or 2015 (NHDOT, 2016a, 2016b, 2016c), so all data was evaluated and subsequently adjusted to reflect 2015 AAWDT conditions.

The Automatic Traffic Recorder (ATR) counts were taken for a 3-5 day period. A listing of the locations is included below and shown in Figure 2.

## Interstate Locations (15)

I-93 NB and SB, south of Exit 4 (NHDOT permanent recorder)
I-93 Exit 4 - NB and SB on- and off-ramps (5)
I-93 Exit 5 - NB and SB on- and off-ramps (4)
I-93 NB and SB between Exits 4 and 5 (2)
I-93 NB and SB north of Exit 5 (2)

## State Highways/Local Streets (22)

Crystal Avenue (NH Route 28), south of Tsienneto Road
Folsom Road, west of NH Route 28
Pinkerton Street, east of Tsienneto Road
Tsienneto Road, east of Pinkerton Street
Chester Road (NH Route 102), east of NH Route 28 Bypass (Sylvestri Circle)
North Main Street (NH Route 28 Bypass), north of Pinkerton Street (Academy Drive)
North Main Street (NH Route 28 Bypass), north of Tsienneto Road
South Main Street (NH Route 28 Bypass), south of Thornton Street
Tsienneto Road, west of NH Route 102
NH Route 102, at Derry Town line
NH Route 28, at Derry/Londonderry Town line
Gilcreast Road, north of NH Route 102
NH Route 102, west of Abbot Street
NH Route 102, east of Griffin Street
Fordway, over Beaver Brook

Franklin Street, north of Folsom Road
Ash Street at Londonderry Town line
Ash Street, east of Londonderry Road
NH Route 28, east of Perkins Road
NH Route 28, south of Rollins Street
NH Route 28, north of Liberty Drive
NH Route 102, east of Hampton Drive
Intersection Turning Movement Counts (TMCs) - AM and PM Peak Periods (19)
The intersection counts were taken in groups of intersections within five general groups or 'zones' in close proximity to each other to facilitate ease of data collection and to minimize significant differences between locations, even if there were intervening roadways or driveways that would not allow balancing between sites. These groups of intersections were numbered as follows and shown in Figure 3:

## Zone 1

\#3 Exit 5 SB ramps
\#4 Exit 5 NB ramps

Zone 2
\#1 Exit 4 SB ramps
\#2 Exit 4 NB ramps

## Zone 3

\#5 NH Route 102/Londonderry Road/St. Charles Street
\#6 NH Route 102 (Broadway)/Fordway/Madden Hill Road
\#7 NH Routes 102/28 (Crystal Avenue/Broadway/Birch Street)
\#8 North High Street/Ash Street Extension
\#9 North High Street/Madden Road
\#10 North High Street/Folsom Road/Franklin Street/Franklin Street Extension
Zone 4
\#11 NH Route 28/Folsom Road/Tsienneto Road (Ross' Corner)
\#12 Tsienneto Road/Pinkerton Street
\#13 NH Route 28/Linlew Drive
\#14 NH Route 28/Ashleigh Drive
\#15 NH Route 28/Scobie Pond Road
Zone 5
\#16 NH Routes 102/28 Bypass/East Derry Road (traffic circle)
\#17 NH Route 28 Bypass/Pinkerton Street/Nesmith Street
\#18 NH Route 28 Bypass/Tsienneto Road
\#19 NH Route 102/Tsienneto Road
Copies of the relevant raw traffic count data are included in Appendix A.
Other new intersections that would be created by some of the Exit 4A alternatives will also need to be evaluated and analyzed. In addition, it was determined as the study progressed that additional intersections at the east end of the study area should be
collected, since they will be influenced by any improvements at the NH Route 102/Tsienneto Road intersection. These intersections were at NH Route 102/North Shore Road (\#26) and at NH Route 102/English Range Road (\#27). This data is also included in Appendix A.

## Adjustment Factors used for Data Reduction

Because of the nature of the regional roadway network, there are several different adjustment factors that need to be applied to the raw counts to derive AWDT. In general, there are seasonal factors, annual growth factors, and axle correction factors, based on the type of roadway being considered. NHDOT develops these factors for various roadway types based on their evaluation of permanent traffic recorder stations across the state. NHDOT differentiates between Rural and Urban Interstates (called Groups 1 and 3, respectively), as well as Rural and Urban Highways (Groups 2 and 4, respectively), for which there is a wealth of short-term and long-term factors that are developed annually by NHDOT as part of their normal practice (NHDOT, 2016d). Appendix B includes the tables showing the various seasonal, annual and axle correction factors applied to the raw traffic counts in this report.

## Seasonal Factors

In this study area, there are Interstate roadways (I-93) as well as state highways and local streets in an urbanized area, so the Group 3 and 4 seasonal factors in Appendix B were applied here. Since counts were taken on specific dates in May, the 2015 seasonal adjustment factors were applied to each count separately based on the date of the count and the type of roadway.

## Annual Growth Factors

Annual growth factors are also applied because of the different years that the counts were taken. There is an NHDOT permanent traffic recorder in the immediate study area on I93 just south of Exit 4 at the Derry/Windham town line, but it may not be indicative of growth on the local street network because the interstate is more prone to fluctuations in regional traffic. A comparison of May 2015 to May 2016 traffic counts on I-93 indicates a $1.1 \%$ growth rate on the Interstate system. It should be noted that this counter is located north of the current construction area, so it should not have been influenced by drivers trying to avoid construction-related delays. This $1.1 \%$ annual growth rate was applied to the 2016 mainline I-93 traffic data only to adjust the data downward to the 2015 base year AWDT.

Another permanent recorder is located on NH Route 28 in Windham south of the study area that should be more representative of the urbanized roadways within the Derry/Londonderry area. A comparison of May 2015 to May 2016 traffic counts at the NH Route 28 location indicates a $2.5 \%$ growth rate, which was then applied to the rest of the study area roadway system to derive the 2015 AWDT.

There are also ramp volume counts at Exits 4 and 5 that need to be seasonally adjusted. In discussions with the NHDOT Bureau of Traffic (NHDOT, 2016e), it was agreed that these ramp volumes would exhibit characteristics more in line with the local street network as opposed to seasonal variations in Interstate traffic. As such, the $2.5 \%$ growth rate was also applied to the ramp volumes to derive the 2015 AWDT.

## Axle Correction Factors

Axle correction factors are also applied to adjust for differences in vehicle classification on various types of roadways to derive a total number of actual vehicles. It is essentially a correction for the assumed number of two-axle vehicles gathered by the field-counting apparatus (such as road tubes) to account for multi-axle vehicles in the traffic stream, based on the FHWA 13-tiered classification system. These factors are developed by NHDOT based on vehicle classification information collected on the various functional classifications of roadways in the state.

Each of the major roadways in the study area has already been functionally classified based on its overall role in the regional roadway network. Since this is an urbanized area, the classifications that are applied here are urban interstate (FC 11), urban principle arterials (FC 14), urban minor arterials (FC 16), collector roadways (FC 17), and local streets (FC 19). The 2015 axle correction factors table is also provided in Appendix B.

## Development of 2015 AAWDT Base Volumes

Table 1 shows a summary of the adjusted 2015 AAWDT volumes derived from applying the various adjustment factors to the 2015 and 2016 raw traffic counts. In some cases, such as for the 2014 counts, the NHDOT has already developed the AAWDT for locations of interest in the study area, which only need to be annually adjusted upward to 2015. This adjustment factor has also been applied to the AM and PM peak hour volumes and ' $k$ ' factors (the percentage of AAWDT during each peak hour for each movement) calculated for comparison to the intersection TMCs for future analysis purposes.

## TABLE 1

## ATR Count Summary - Adjusted 2015 AAWDT and Peak Hour Volumes



Note - Exit 5 SB off-ramp AM peak volume does not include one count that appears anomalous when compared to other counts in same hour Red counts are from NHDOT Town summary data - 2014-2015

### 3.2 Existing Signal Information - Timing and Phasing

Information about the current signal timing and phasing plans at each of the signalized intersections was compiled from records available from the entity with current maintenance responsibility, which is either the NHDOT Bureau of Traffic or the Town of Derry (none of the signals in Londonderry are under their jurisdiction). Current records for one of the locations (NH Route 102/Fordway) were not readily available, so the required information was gathered in the field by observation. This information, combined with the current lane use at each location, was compiled into a data file in the SYNCHRO signal analysis program, which emulates the procedures in Volume 3 (Interrupted Flow) of the Highway Capacity Manual 2000 (HCM) (TRB, 2000) analysis procedures, for use in future analysis. The HCM 2000 procedures are being used for signalized intersections because these procedures can analyze non-standard timing and phasing parameters, since as leading pedestrian start times, which were found in the field, and to be consistent with the analyses in the Interstate Justification Report (Louis Berger, 2018).

### 3.3 Crash Data - 2010-2014 - Data Reduction and Summary

Data compiled by the NH Department of Safety for the last five full calendar years was made available by the NHDOT for the two study area towns. Since the crash records are identified by State Plane coordinates, this data search was narrowed further to include only those crashes located within the limits of the study area, roughly bounded by I-93 to the west, NH Route 102 to the south, NH Routes 28 and 28 Bypass north of Tsienneto Road to the north, and the Tsienneto Road/NH Route 102 intersection to the east. The records were assigned to specific roadway segments or individual intersections if sufficient locational information was available. In some cases these identifiers overlapped, so the sum of the segment and intersection crashes is more than the total.

The findings are summarized in Table 2 below. A total of 716 crashes were identified within the project area within the five-year time span, with only one fatality (a single-car incident in 2014 on NH Route 102 in Londonderry). About $24 \%$ of the crashes were injury or fatality, with almost $87 \%$ of these being on the major roadways in the study area. NH Routes 102 and 28 combined accounted for about $2 / 3$ of the total reported crashes, averaging 48 per year, with the Interstate only accounting for $19 \%$, or 25 per year. The traffic circle at NH Route 28 Bypass and NH Route 102 had the most reported crashes of any intersection during this period, averaging almost 5 per year.

Although there was a consistent number of crashes during three of the five years that data was compiled (between 182 and 185 per year), the other two years show wide fluctuations within this period ( 115 and 52 crashes). Almost $80 \%$ of the crashes involved another motor vehicle, with another $13 \%$ involving a crash with a fixed object. Seven of the crashes involved a bicyclist or pedestrian, while another six involved a crash with an animal.

TABLE 2
EXIT 4A STUDY AREA CRASH SUMMARY 2010-2014

| Location | Fatal Crashes | Injury Crashes | Property <br> Damage Only | Unknown Damage | Total Crashes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Roadways |  |  |  |  |  |
| NH Route 102, Exit 4 to Tsienneto Road. | 1 | 58 | 172 | 9 | 240 |
| NH Route 28, Exit 5 to NH Route 102 | 0 | 40 | 162 | 9 | 211 |
| I-93, Exit 4 to Exit 5 | 0 | 27 | 97 | 3 | 127 |
| NH Route 28 Bypass, NH Route 102 to Auburn Town Line | 0 | 19 | 39 | 0 | 58 |
| Folsom Road/Tsienneto Road | 0 | 3 | 27 | 2 | 32 |
| TOTAL | 1 | 147 | 497 | 23 | 668 |
| \% OF TOTAL | 0.1\% | 22.0\% | 74.4\% | 3.4\% | 100.0\% |
| AVG PER YEAR | 0.2 | 29.4 | 99.4 | 4.6 | 133.6 |
|  |  |  |  |  |  |
| Major Intersections |  |  |  |  |  |
| NH Route 102/NH Route 28 Bypass | 0 | 7 | 16 | 0 | 23 |
| NH Route 28 Bypass/Tsienneto Road | 0 | 3 | 14 | 0 | 17 |
| NH Route 102/NH Route 28 | 0 | 3 | 14 | 0 | 17 |
| NH Route 102/Fordway/High St. | 0 | 3 | 12 | 0 | 15 |
| Tsienneto Road/Pinkerton Street | 0 | 1 | 10 | 0 | 11 |
| Folsom Road/Franklin Street | 0 | 1 | 8 | 1 | 10 |
| NH Route 28/Folsom Road/Tsienneto Road/ (Ross' Corner) | 0 | 1 | 9 | 0 | 10 |
| NH Route 28/Ashleigh Dr. | 0 | 3 | 6 | 1 | 10 |
| NH Route 28/Linlew Dr. | 0 | 0 | 9 | 0 | 9 |
| NH Route 102/Londonderry Road | 0 | 2 | 5 | 1 | 8 |
| NH Route 102/Tsienneto Road | 0 | 1 | 4 | 0 | 5 |
| TOTAL | 0 | 25 | 107 | 3 | 135 |
| \% OF TOTAL | 0.0\% | 18.5\% | 79.3\% | 2.2\% | 100.0\% |
| AVG PER YEAR | 0 | 5 | 21.4 | 0.6 | 27 |
| ADDITIONAL INFO BELOW |  |  |  |  |  |
| Year |  |  |  |  |  |
| 2010 | 0 | 45 | 132 | 5 | 182 |
| 2011 | 0 | 32 | 83 | 0 | 115 |
| 2012 | 0 | 45 | 135 | 5 | 185 |
| 2013 | 0 | 8 | 40 | 4 | 52 |
| 2014 | 1 | 39 | 133 | 9 | 182 |
|  | 1 | 169 | 523 | 23 | 716 |
|  | 23.7\% | (approx. percent that are injury or fatality) |  |  |  |
| Crash Types | Number | \% Total |  |  |  |
| Animal | 6 | 0.84\% |  |  |  |
| Bicyclist | 2 | 0.28\% |  |  |  |
| Fixed Object | 91 | 12.71\% |  |  |  |
| Jackknife | 1 | 0.14\% |  |  |  |
| Other Motor Vehicle | 568 | 79.33\% |  |  |  |
| Other Object | 3 | 0.42\% |  |  |  |
| Overturn | 14 | 1.96\% |  |  |  |
| Parked Motor Vehicle | 9 | 1.26\% |  |  |  |
| Pedestrian | 5 | 0.70\% |  |  |  |
| Spill (two-wheeled vehicles) | 3 | 0.42\% |  |  |  |
| Other | 14 | 1.96\% |  |  |  |
|  | 716 |  |  |  |  |

### 4.0 Development of Base Traffic Networks

The time periods to be analyzed will be the 2015 AM and PM peak hours as determined by the traffic counts. The analysis will focus on operations of both the Interstate system (freeway facilities, ramp terminals, ramp merge/diverge, weaving sections) as well as local intersection Levels of Service, using the methodologies in the current version of the HCM.

There are two different approaches that need to be considered for the Interstate system versus the local roadways. The Interstate section within the study area from south of Exit 4 to north of Exit 5 is a closed system - traffic enters and exits at specific locations, so the entire system needs to balance in both directions. The local roadways are not a closed system; counts between the local intersections may not necessarily balance in most locations because there are other intervening driveways for adjacent land uses and other minor streets where traffic is able to enter or exit the network.

## Interstate Volume Balancing

Within the closed Interstate system, there are two adjustments that need to be made. One is for the overall mainline/ramp system, where a starting point was chosen (in this case, at the NHDOT permanent traffic recorder location south of Exit 4) and add or subtract the on- and off-ramp volumes both northbound and southbound to develop the base AM and PM peak hour networks along I-93.

The second adjustment is to balance volumes between the ramp terminals at both Exits 4 and 5, based on the peak hour volume counts and the recent TMCs that were collected in May 2016. This second process will be discussed later in the report.

Directional counts from the I-93 permanent recorder station during May 2015 were reviewed and compiled to determine the AWDT during that period (taking the Memorial Day holiday count out of consideration). These were adjusted seasonally to develop the 2015 AWDT for both northbound and southbound traffic as the starting point. The ramp counts taken in May 2016 were also seasonally and annually adjusted to the 2015 AWDT and then added and subtracted accordingly going north and south on the Interstate. The resulting mainline 2015 AWDT volumes for the AM and PM peak hours are shown in Figures 4 and 5, respectively. The counts and calculations are provided in Appendix C.

## Ramp Terminal Balancing - Exits 4 and 5

The turning movement volumes at the ramp terminals at Exits 4 and 5 must also balance between the intersections while agreeing with the overall ramp volumes. While the ramp volumes were collected with automatic traffic recorders, which only summarized data on an hourly basis, the turning movements were collected at 15 -minute intervals. Furthermore, the individual intersections also have their own peak hours, which may not necessarily match the adjacent ramp or the hourly ramp volume. Therefore, an overall peak for each interchange was developed from a summary of the turning movement
counts at each location and the turning percentages applied to the balanced interstate ramp volumes derived above. The AM peak period was determined to be from 7:30-8:30, while the PM peak was from 4:45-5:45. The balanced 2015 AM and PM peak hour volumes at the two interchanges are also shown in Figures 4 and 5, respectively. The calculations are also provided in Appendix C.

## Other Intersection Counts

As noted above, the local intersection turning movement counts were collected in groups of intersections in close proximity to each other to minimize significant differences between locations, even if there were intervening roadways or driveways that would not allow balancing between sites. There are only four intersections on the local network where traffic should essentially balance between adjacent intersections:

- Between Ross' Corner (NH Route 28/Folsom/Tsienneto) and at Pinkerton Street;
- Between North High Street/Madden Road and the North High Street/Folsom/ Franklin/Franklin Street Extension intersection;
- Between the NH Route 28 Bypass/NH Route 102 traffic circle and the intersection at NH Route 28 Bypass/Pinkerton Street/Perkins Street to the north; and
- Between NH Route 102/Tsienneto Road easterly to include the North Shore Road and English Range Road intersections.

Counts at these locations were balanced and all counts were adjusted to the 2015 AWDT using the NHDOT seasonal and annual factors for Group 4 Urban Highways noted above. The 2015 AM and PM peak hour volumes at the local intersections are shown in Figures 6 and 7, respectively.

### 5.0 Model Calibration

The SNHPC regional traffic model is an Average Annual Weekday Traffic (AAWDT) model for the greater Manchester, NH area that includes Derry and Londonderry as well as other surrounding towns. The model area has expanded since its use in the 2007 DEIS project to include towns to the south, east and west of the Exit 4A area with added roadway links and TAZs to provide traffic generation capabilities for the SNHPC's planning horizon of 2040.

However, to be a useful travel forecasting tool, the model needs to be able to replicate actual traffic volumes throughout its network within certain reasonable margins of error established by the Federal Highway Administration (FHWA) for regional traffic models. As such, the various 2015 traffic volume counts provided in Table 1 for the Exit 4A study area, among other locations in the SNHPC region, were used as a guide to test the validity of the SNHPC traffic model as a predictive tool of actual 2015 counts found in the region. This was found to be the case, and the findings of the calibration process were presented to the Exi4 4A Working Group in October, 2016. A more detailed memo describing the various calibration procedures undertaken as part of this project is included in Appendix D.

It should be noted that the current SNHPC traffic model is based on expected trip making behavior from observations of past conditions and predicting these out to a future date, in this case the 2040 design year. With the advent of autonomous/connected vehicles (AV/CVs) and the increasing likelihood of them being a larger share of the vehicle fleet within the planning horizon now covered by the model, there is much uncertainty about how and to what extent current and forecasted individual driving habits may be affected by this potentially transformative technology.

A recent study prepared by the Texas A\&M Transportation Institute (Texas A\&M, 2017) looked at the possible implications of AV/CVs on the transportation planning process. Some of the key modeling components they identified that could be affected by the eventual deployment of AV/CVs into the traffic stream include:

- the possible changes on the socio-economic factors that typically influence trip making and vehicle ownership;
- future characteristics of the highway network, including the effect on roadway and intersection capacity, safety and operations;
- the need to consider changes to the model area geography (e.g. traffic zones) based on possible household locational decisions;
- the possible effects on trip generation, distribution and mode choices with the availability of AV/CVs, including the likelihood of zero-occupant vehicles on the roadway network

The current transportation planning process looks at changes to demographics and roadway networks to predict future travel demands, assuming trip making will be similar to today. With AV/CVs becoming a larger component of future transportation options, the current process is not suited to predict future trip-making behavior since there is no way to reasonably predict the impact of these technologies on individual travel demand decisions. There is also the likelihood that populations that now are unable to drive or own a vehicle will have greater mobility options available to them, and therefore may result in more trips on the network than would normally be forecasted.

Therefore, until such time as traffic demand modelling on a regional basis can account for the increased deployment of AV/CVs at some critical mass to be able to better assess the impact on some/all of the trip-making factors noted above, the current transportation planning and regional travel demand modeling process is the best available option for forecasting future traffic on the roadway network for a project such as Exit 4A.

### 6.0 Capacity Analyses - 2015 Base Conditions

In general, traffic analyses focus on the facilities that present the most likely constraints to overall operations on the roadway network. For interstate facilities, traffic operations are governed largely by the combination of mainline traffic flow at a given speed and number of lanes as it may be influenced by merging and diverging traffic at on and offramps at interchanges, as well as any weaving sections between ramps in close proximity to each other. For local roadway networks, traffic flow tends to be governed by
intersection capacity which acts to meter volumes onto adjacent roadway segments based on its ability to allow conflicting movemetns to be served.

The 2010 Highway Capacity Manual (TRB, 2010) provide the technical procedures to analyze traffic operations of freeway facilities (basic freeways, ramp merge/diverge and weaving sections) used in this report. Chapter 10 of the 2010 HCM defines the methodologies used to analyze typical freeway facility operations for extended lengths of continuously connected basic freeway, weaving, merge and diverge segments, such as those along I-93 in the Exit 4A study area. This methodology allows for the analysis of multiple/continuous 15 -minute time periods and is capable of identifying locations where the facility may break down and the impacts of such on the rest of the facility. As such, the analysis determines where the 'weakest link' in the facility may control overall operations along a freeway network in either direction.

The 2000 Highway Capacity Manual (TRB, 2000) provided methodologies for signalized and unsignalized intersections, including roundabouts, that will be used to analyze the NH Route 102/NH Route Bypass 28 traffic circle. Because of the phasing and timing limitations of the existing intersections, the HCM 2000 procedures were used for the signalized and unsignalied intersection analyses, as well as to be consistent with the IJR. Chapters 18 and 19 of the 2000 HCM define the methodologies for signalized and twoway stop controlled intersections.

The Highway Capacity Software (McTrans, 2018) as well as the SYNCHRO/Sim-Traffic programs (Trafficware, 2016) are common software packages used by traffic engineers to evaluate how traffic volumes react under interrupted and uninterrupted flow conditions under various volume, speed, traffic composition, lane use and signal timing conditions. The Level of Service (LOS) criteria for freeway facilities and intersection operations defined in the both versions of the HCM are provided in Appendix E. In general, a LOS C is considered desirable for freeway facilities operations; however, LOS D is considered acceptable for both freeways and intersection operations in urbanized areas.

### 6.1 Mainline Interstate Operations

The 2015 base weekday AM and PM peak hour volumes along I-93 from just south of Exit 4 to north of Exit 5 are shown in Figures 4 and 5.

The existing two-lane I-93 freeway facility was segmented along its length both northbound and southbound, based on the spacing of on- and off-ramps connecting the basic two-lane freeway segments on either side. Northbound, there were five basic freeway segments, two diverge (i.e., off-ramp) and two merge (i.e. on-ramp) segments under existing conditions. Southbound, there is one additional freeway and one more merge segment to account for the SB loop on-ramp at Exit 4 from the east and the segment between the SB on-ramps. Because of the distance between the existing interchanges, there are currently no weaving sections along I-93 in the Exit 4A study area network.

### 6.1. 1 Mainline Freeway Segments

Five freeway segments are contained in the I-93 project study area going northbound, with a sixth one added in the southbound direction because of the additional on-ramp at Exit 4. There will be additional segments created when the Exit 4A alternatives are analyzed.

The demand and geometric factors input for segments and facility analyses include:
Demand

- Vehicles/hour
- Percent trucks and recreatonal vehicles (RVs)
- Driver population factor


## Geometry

- Number of lanes
- Average lane width
- Right-side lateral clearance
- Terrain
- Free-flow speed
- Location of/distance to merge/diverge segments, with number of lanes, length of acceleration/deceleration lanes

A description of the existing facility segments and the detailed reports are summarized in Table 3 and included in Appendix F.

TABLE 3
HCS 2010 - FREEWAY FACILITIES ANALYSIS - 2015 BASE- AM AND PM PEAK HOURS


Note: $\mathrm{d} / \mathrm{c}=$ Demand-to-capacity ratio

### 6.1.2 Merge/Diverge Operations

Merge/diverge operations are the result of off-ramp and on-ramp traffic leaving and/or getting onto the freeway and how the ramp traffic interacts with the mainline freeway traffic. Since all traffic on I-93 in the study area is entering or exiting in the rightmost lane, which is also where most heavy vehicles travel, this Lane 1 volume is critical to the determination of operations. The ramp spacing and order of operation (e.g. off-ramp followed by an on-ramp, as opposed to an off-ramp followed by another off-ramp) also plays a role in how and to what degree these movements impede mainline freeway traffic flow.

There are currently four merge (on-ramp) and diverge (off-ramp) arrangements in the Exit 4A study area in the northbound direction and a fifth in the southbound direction (the second SB on-ramp at Exit 4). The introduction of a new interchange between Exits 4 and 5 will add another merge and diverge in each direction. The differences between the northerly and southerly interchange alternatives and their relative proximity to Exits 4 and 5 will ultimately determine how these new ramps will affect mainline operations. Table 3 provides the analysis results for the merge/diverge operations along I-93 in the study area under 2015 AM and PM peak hour conditions.

### 6.1.3 Weaving Operations

Weaving operations occur on highway segments between on- and off-ramps where merging and diverging traffic conflict while completing their respective movements. This analysis is mostly governed by the distance between these ramps, the number of lanes available to make such a movement, the volumes making their respective merge and/or diverge movements, and the ability of these movements to occur independently without influencing each other. This is more of an issue in areas where there are closely spaced interchange ramps.

In the current condition, Exits 4 and 5 are more than two miles apart, so there is essentially no weaving that occurs between the ramps. With the introduction of Exit 4A to the I-93 network, weaving between the Exit 4 NB on-ramp and the Exit 4A NB off-ramp may need to be considered for the southerly interchange alternatives. However, the HCS Freeway Facilities calculations allow for an overlap of the 1500foot 'influence areas' between adjacent ramps, which was included in the analyses. At this point, it does not appear that a weaving section will be created between Exit 4A and Exit 5 because of the greater spacing between them.

### 7.0 Signalized Intersection Operations - 2015 Base Condition

The existing signal timing/phasing information gathered earlier, combined with the current lane use at each location along with the 2015 AM and PM peak hour volumes, was compiled into a data file in the SYNCHRO (Trafficware, 2016) signal analysis program, which emulates the procedures in Volume 3 (Interrupted Flow) of the Highway Capacity Manual 2000 (HCM) analysis procedures (TRB, 2000). Because of the phasing and timing limitations of the existing intersections, the HCM 2000 procedures were used for the signalized intersection analyses. The overall delay and LOS was determined by using the HCM module in SYNCHRO, while the queuing calculation results came directly from five runs of the Sim-Traffic module within SYNCHRO per NHDOT guidance (NHDOT, 2017a). The volume-to-capacity (v/c) ratios, average delays and LOS for the signalized intersections are shown in Table 4 below. The peak queues by approach are shown in Table 5 later in this report.

| Table 4 |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Summary of 2015 Signalized Intersection Capacity Analyses |  |  |  |  |  |  |

The HCM and SYNCHRO printouts are provided in Appendices G 1-3.
The results of these analyses show which movements at the various intersections exhibit some current capacity constraints (LOS E or worse). Some of these, such as at the Exit 4 ramp terminals, will be addressed by the ongoing I-93 widening project, while issues at other local intersections may need to be addressed in some form, either through added lanes and/or optimized signal timings, by the 2040 design year. These existing deficiencies are discussed briefly below:

- Exit 4 SB Off-Ramp

The turns from the off-ramp are the most constrained movements, with the higher-volume right turn from a single lane showing the most delay and queuing. A second right-turn lane is proposed as part of the ongoing improvements to Exit 4.

## - Exit 4 NB Ramps

The westbound thru traffic is under duress during the AM peak, while the eastbound left turn to the on-ramp is at LOS E in the PM peak. While the right turn from the off-ramp operates at a good LOS because it is not controlled by the signal, field observations show it is often impeded by either the eastbound traffic through the intersection and/or the downstream queuing of traffic on NH Route 102 east of the interchange.

## - NH Route 102/NH Route 28 (Crystal Avenue/Broadway/Birch Street)

This major crossroads in the heart of downtown Derry has several movements that exhibit substantial delays during AM and/or PM peak hours, and results in queuing along Broadway. The level of parking and pedestrian activity also affects overall traffic operations as the mix of local and through traffic results in significant congestion, even if not directly reflected in the overall capacity/LOS calculations.

Because the reduction in this through traffic in downtown Derry is one of the primary purposes for the proposed Exit 4 A project, it was necessary to find a more qualitative assessment of downtown congestion that may not be reflected in the capacity calculations. To do this, we looked at Google Maps snapshots during the course of typical weekday AM and PM peak hours (Google, 2018). These are based on real-time on-the-ground observations of travel times in the study area. The snapshots for AM and PM peak hours between Monday, January 22, 2018 and Friday, January 26, 2018 are provided in Appendix H. It should be noted that Exit 4 is currently under construction, although there should be minimal work going on during the winter when these snapshots were taken.
These figures show regular congestion at the NH Route 102/28 intersection as well as other key intersections in the study area during any given weekday peak
hour. Congestion in and around Exit 4 is oriented westbound in the AM peak and eastbound in the PM peak, and is shown to affect other segments along Broadway in both directions to varying degrees. Key intersections along the north-south corridors of NH Route 28 and NH Route 28 Bypass, such as at Ross' Corner, Tsienneto Road, and the traffic circle at NH Route 102, appear to exhibit regular levels of delay and congestion based on this sample of peak hour travel times.

## - Ross' Corner (NH Route 28/Tsienneto Road/Folsom Road)

This intersection leads to the major commercial corridor in north Derry as well as serving as a commuter route. Traffic currently uses the Ash Street Extension and Folsom Road as an alternative route to NH Route 102 to avoid the aforementioned downtown congestion. Several turning movements experience significant delays, even with recent improvements that provided a second SB leftturn lane onto Tsienneto Road. The proximity of the Pinkerton Street unsignalized intersection just east of this location also affects overall traffic flow in this area.

## - NH Route28/Ashleigh Drive

This intersection serves as the primary access drive to the new Wal-Mart supercenter as well as other commercial establishments on the east side of NH Route 28. The heavy turning movements into and out of this town road, combined with significant commuter volumes along the NH Route 28 corridor, result in less than desirable levels of delay for several movements, particularly in the PM peak, even though the overall LOS is at LOS C.

- NH Route 28 Bypass/Tsienneto Road

The Tsienneto Road corridor west of NH Route 28 Bypass as well as the lands adjacent to this intersection has seen a fair share of new development over the years, as well as increased use by east-west commuter traffic avoiding NH Route 102 and the downtown area. With only a single east-west lane through the intersection, calculated delays now exceed acceptable LOS thresholds for some movements during both peaks.

### 8.0 Unsignalized Intersection Operations

Similarly, the unsignalized intersections in the study area network were analyzed for the 2015 AM and PM peak hours using the standard 2010 HCM procedures. These results are provided in Table 6, with the printouts in Appendix I. It should be noted that the traffic circle at the intersection of NH Route 28 Bypass, NH Route 102, and East Derry Road was analyzed as a roundabout, since all turns at this location are right turns in the counterclockwise direction. The circle was evaluated using updated roundabout analysis procedures from HCM 6, published in 2016 (TRB, 2016), because it incorporates updated data from actual field operations of the growing number of roundabouts in the USA and, as such, should be more representative of local driver behavior.

As observed in the field and confirmed by the SYNCHRO analyses, left turns from the minor side streets experience significant delays due to the high volumes on the major streets, either on the State highway system or local streets such as Tsienneto Road. Of particular concern is the heavy left-turn volume exiting from Pinkerton Street onto Tsienneto Road in close proximity to the signalized intersection at Ross’ Corner. Special attention will be needed to address this condition under future No-Build and Build conditions.

The table also shows the peak design queue by approach for both the signalized and unsignalized intersections, based on the 2015 capacity analysis of base conditions. This will be an important component of evaluating the future 2040 Build condition layouts under the various alternatives.

| Table 5 <br> 2015 Signalized Intersection Capacity and Queuing Analys <br> Signalized Intersections |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Lane Groups | $95 \%$ <br> queue <br> (ft) | AM <br> v/c ratio | ak Hour <br> Average Delay | LOS | 95\% queue <br> (ft) | $\begin{gathered} \mathrm{PM} \\ \mathrm{v} / \mathrm{c} \\ \text { ratio } \end{gathered}$ | ak Hour <br> Average Delay | LOS |
| \#1 - Exit 4 SB Off-Ramp/NH Route 102 | EB Thru | 212 | 0.46 | 11.5 | B | 230 | 0.44 | 11.0 | B |
|  | WB Thru | 18 | 0.31 | 1.9 | A | 18 | 0.41 | 1.8 | A |
|  | SB LT | 251 | 0.64 | 39.5 | D | 317 | 0.69 | 50.4 | D |
|  | SB RT | 176 | 0.75 | 13.6 | B | 630 | 1.08 | 80.9 | F |
| \#2 - Exit 4 NB Off-Ramp/NH Route 102 | NB LT | 107 | 0.57 | 46.2 | D | 281 | 0.50 | 33.3 | C |
|  | NB RT | 0 | 0.15 | 0.2 | A | 0 | 0.41 | 0.8 | A |
|  | EB LT | 610 | 0.88 | 43.8 | D | 548 | 0.91 | 62.3 | E |
|  | EB Thru | 83 | 0.24 | 4.3 | A | 242 | 0.40 | 19.5 | B |
|  | WB Thru | 448 | 0.97 | 58.7 | E | 250 | 0.76 | 51.5 | D |
| \#3 - Exit 5 SB Off-Ramp/NH Route 28 | EB Thru | 212 | 0.68 | 32.7 | C | 197 | 0.56 | 27.8 | C |
|  | EB RT | 0 | 0.21 | 0.3 | A | 0 | 0.21 | 0.3 | A |
|  | WB LT | 211 | 0.81 | 40.0 | D | 151 | 0.62 | 45.3 | D |
|  | WB Thru | 59 | 0.43 | 7.0 | A | 52 | 0.28 | 4.8 | A |
|  | SB LT | 138 | 0.68 | 29.2 | C | 254 | 0.73 | 36.5 | D |
|  | SB RT | 148 | 0.78 | 28.7 | C | 63 | 0.45 | 6.2 | A |
| \#4 - Exit 5 NB Off-Ramp/NH Route 28 | EB LT | 251 | 0.86 | 55.0 | D | 223 | 0.72 | 48.4 | D |
|  | EB Thru | 5 | 0.44 | 2.2 | A | 308 | 0.53 | 12.7 | B |
|  | WB Thru | 189 | 0.56 | 26.1 | C | 192 | 0.37 | 27.4 | C |
|  | WB RT | 0 | 0.53 | 1.3 | A | 0 | 0.38 | 0.7 | A |
|  | NB LT | 233 | 0.87 | 49.4 | D | 180 | 0.75 | 44.1 | D |
|  | NB RT | 0 | 0.10 | 0.1 | A | 143 | 0.77 | 35.2 | D |
| \#6 - NH Route 102/Fordway | EB all | 247 | 0.12 | 17.7 | B | 591 | 1.00 | 47.1 | D |
|  | WB all | 368 | 0.94 | 26.4 | C | 306 | 0.81 | 26.8 | C |
|  | NB all | 304 | 0.72 | 51.7 | D | 215 | 0.84 | 36.6 | D |
|  | SB all | 22 | 0.86 | 12.4 | B | 90 | 0.18 | 15.9 | B |
| \#7 - NH Routes 102/28 | EB L | 148 | 0.83 | 83.0 | F | 155 | 0.70 | 55.8 | E |
|  | EB T/R | 170 | 0.42 | 20.1 | C | 393 | 0.73 | 34.2 | C |
|  | WB L | 47 | 0.28 | 40.6 | D | 119 | 0.68 | 69.5 | E |
|  | WB T/R | 385 | 0.88 | 42.7 | D | 272 | 0.67 | 35.1 | D |
|  | NB L | 101 | 0.79 | 90.6 | F | 80 | 0.43 | 42.5 | D |
|  | NB T/R | 274 | 0.85 | 48.3 | D | 316 | 0.86 | 51.3 | D |
|  | SB L | 121 | 0.86 | 103.4 | F | 174 | 0.79 | 67.9 | E |
|  | SB Thru | 188 | 0.61 | 33.9 | C | 346 | 0.77 | 43.3 | D |
|  | SB RT | 2 | 0.23 | 1.1 | A | 35 | 0.21 | 3.5 | A |


| Intersection | Existing Lane Use | Table 5 (Cont'd) <br> alized Intersections (cont.) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $95 \%$ <br> queue <br> (ft) | AM <br> v/c ratio | ak Hour <br> Average Delay | LOS | 95\% queue (ft) | PM <br> v/c ratio | ak Hour <br> Average Delay | LOS |
| \#11- Ross' Corner (Folsom/NH Route 28) | EB L | 191 | 0.16 | 88.0 | F | 324 | 0.89 | 78.7 | E |
|  | EB Thru | 169 | 0.27 | 45.1 | D | 310 | 0.73 | 49.0 | D |
|  | EB R | 0 | 0.25 | 0.0 | A | 0 | 0.17 | 0.7 | A |
|  | WB L | 157 | 0.70 | 66.1 | E | 273 | 1.14 | 165.5 | F |
|  | WB Thru | 323 | 0.21 | 80.3 | F | 241 | 0.75 | 60.7 | E |
|  | WB R | 108 | 0.26 | 8.0 | A | 190 | 0.52 | 16.4 | B |
|  | NB L | 35 | 0.90 | 40.5 | D | 134 | 0.58 | 66.6 | E |
|  | NB Thru | 90 | 0.63 | 25.5 | C | 198 | 0.43 | 40.0 | D |
|  | NB R | 0 | 0.01 | 1.2 | A | 0 | 0.27 | 1.1 | A |
|  | SB L | 131 | 0.74 | 42.0 | D | 248 | 0.76 | 49.7 | D |
|  | SB Thru | 72 | 0.95 | 19.5 | B | 419 | 0.64 | 35.6 | D |
|  | SB RT | 27 | 0.48 | 4.1 | A | 51 | 0.28 | 4.8 | A |
| \#13 -NH Route 28/Linlew Drive | EB L/T | 10 | 0.06 | 33.0 | C | 40 | 0.18 | 39.4 | D |
|  | EB R | 0 | 0.04 | 0.2 | A | 0 | 0.05 | 0.3 | A |
|  | WB L/T | 61 | 0.35 | 40.6 | D | 69 | 0.46 | 48.8 | D |
|  | WB R | 93 | 0.71 | 18.9 | B | 43 | 0.66 | 13.0 | B |
|  | NB L | 0 | 0.00 | 0.0 | A | 36 | 0.19 | 46.3 | D |
|  | NB T/R | 675 | 0.35 | 12.9 | B | 296 | 0.50 | 15.5 | B |
|  | SB L | 63 | $0.35$ | $42.8$ | $\mathrm{D}$ | 125 | $0.64$ | $37.4$ | D |
|  | SB T/R | 134 | 0.38 | 4.9 | A | 437 | 0.57 | 14.3 | B |
| \#14 - NH Route 28/Ashleigh Drive | EB L | 20 | 0.12 | 40.8 | D | 60 | 0.54 | 65.2 | E |
|  | EB T/R | 16 | 0.11 | 30.0 | C | 29 | 0.25 | 34.5 | C |
|  | WBL | 110 | 0.52 | 46.5 | D | 232 | 0.84 | 69.2 | E |
|  | WB L/T | 111 | 0.53 | 46.7 | D | 227 | 0.83 | 67.0 | E |
|  | WB R | 38 | 0.22 | 6.0 | A | 63 | 0.29 | 10.9 | B |
|  | NB L | 56 | 0.05 | 61.6 | D | 3 | 0.06 | 65.0 | E |
|  | NB T/R | 183 | 0.50 | 10.1 | B | 311 | 0.69 | 14.8 | B |
|  | SB L | 8 | $0.41$ | $42.9$ | E | 39 | 0.47 | 47.4 | D |
|  | SB T/R | 285 | 0.35 | 10.3 | B | 234 | 0.60 | 14.0 | B |
| \#18 - NH Route 28 Bypass/ Tsienneto Road | EB L | 126 | 0.88 | 77.5 | E | 278 | 0.86 | 54.0 | D |
|  | EB T/R | 114 | 0.49 | 24.2 | C | 394 | 0.69 | 30.0 | C |
|  | WB L | 82 | 0.50 | 41.9 | D | 36 | 0.15 | 35.1 | D |
|  | WB T/R | 309 | 0.95 | 59.4 | E | 248 | 0.86 | 58.0 | E |
|  | NB L | 119 | 0.70 | 57.5 | E | 97 | 0.53 | 44.2 | D |
|  | NB T/R | 193 | 0.48 | 26.8 | C | 307 | 0.69 | 37.0 | D |
|  | SB L | 36 | 0.18 | 35.8 | D | 80 | 0.44 | 42.4 | D |
|  | SB Thru | 171 | 0.63 | 35.7 | D | 149 | 0.39 | 29.4 | C |
|  | SB R | 71 | 0.41 | 7.9 | A | 30 | 0.20 | 2.3 | A |


| Table 6 <br> 2015 Unsignalized Intersection Capacity and Queuing Analyses |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | isting Lane Use | 95\% queue (ft) | AM <br> v/c ratio | k Hour <br> Average Delay | LOS | 95\% <br> queue <br> (ft) | PM <br> v/c ratio | k Hour <br> Average Delay | LOS |
| \#5-NH Route 102/Londonderry Road | EB L <br> WB L <br> NB all SB L/T SB R | $\begin{array}{r} 13 \\ 0 \\ 0 \\ 20 \\ 65 \end{array}$ | $\begin{aligned} & 0.142 \\ & 0.005 \\ & 0.008 \\ & 0.253 \\ & 0.505 \end{aligned}$ | $\begin{array}{r} 12.3 \\ 8.6 \\ 11.9 \\ 115.0 \\ 36.1 \end{array}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~A} \\ & \mathrm{~B} \\ & \mathrm{~F} \\ & \mathrm{E} \end{aligned}$ | $\begin{array}{r} 40 \\ 0 \\ 65 \\ 68 \\ 45 \end{array}$ | $\begin{aligned} & 0.354 \\ & 0.008 \\ & 1.078 \\ & 1.130 \\ & 0.395 \end{aligned}$ | $\begin{array}{r} 11.7 \\ 10.7 \\ * \\ * \\ 19.9 \end{array}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~B} \\ & \mathrm{~F} \\ & \mathrm{~F} \\ & \mathrm{C} \end{aligned}$ |
| \#8 - North High Street/Ash Street Extension | $\begin{gathered} \text { EB all } \\ \text { NB LT } \end{gathered}$ | $\begin{array}{r} 45 \\ 0 \end{array}$ | $\begin{aligned} & 0.383 \\ & 0.005 \end{aligned}$ | 15.4 8.2 | $\begin{aligned} & \mathrm{C} \\ & \mathrm{~A} \end{aligned}$ | $\begin{array}{r} 445 \\ 0 \end{array}$ | $\begin{aligned} & 1.152 \\ & 0.005 \end{aligned}$ | $\begin{array}{r} 123.5 \\ 8.4 \end{array}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{~A} \end{aligned}$ |
| \#9 - North High Street/Madden Road | $\begin{gathered} \text { EB all } \\ \text { NB LT } \end{gathered}$ | $\begin{aligned} & 8 \\ & 0 \end{aligned}$ | $\begin{aligned} & \hline 0.079 \\ & 0.000 \end{aligned}$ | $\begin{array}{r} 18.7 \\ 0.0 \end{array}$ | $\begin{aligned} & \hline \mathrm{C} \\ & \mathrm{~A} \end{aligned}$ | $\begin{array}{r} 10 \\ 0 \end{array}$ | $\begin{aligned} & 0.11 \\ & 0.00 \end{aligned}$ | $\begin{array}{r} \hline 27.2 \\ 0.0 \end{array}$ | $\begin{aligned} & \hline \mathrm{D} \\ & \mathrm{~A} \end{aligned}$ |
| \#10 - North High/Folsom/Franklin Streets | EB all <br> WB all <br> NB all <br> SB all | $\begin{array}{r} 3 \\ 3 \\ 15 \\ 8 \end{array}$ | $\begin{aligned} & 0.035 \\ & 0.025 \\ & 0.160 \\ & 0.096 \end{aligned}$ | $\begin{array}{r} 8.3 \\ 8.0 \\ 14.2 \\ 10.5 \end{array}$ | $\begin{aligned} & \text { A } \\ & \text { A } \\ & \text { B } \\ & \text { B } \end{aligned}$ | $\begin{array}{r} 3 \\ 3 \\ 30 \\ 50 \end{array}$ | $\begin{aligned} & 0.043 \\ & 0.038 \\ & 0.293 \\ & 0.424 \end{aligned}$ | $\begin{array}{r} 8.4 \\ 9.2 \\ 23.7 \\ 22.5 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~A} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ |
| \#12-Tsienneto Road/Pinkerton Street | $\begin{gathered} \text { WB L } \\ \text { WB L/T } \\ \text { NB L } \\ \text { NB R } \end{gathered}$ | $\begin{array}{r} 8 \\ 0 \\ 309 \\ 13 \end{array}$ | $\begin{aligned} & \hline 0.088 \\ & 0.000 \\ & 1.156 \\ & 0.154 \end{aligned}$ | $\begin{array}{r} \hline 8.5 \\ 0.0 \\ 154.3 \\ 11.8 \end{array}$ | $\begin{gathered} \mathrm{A} \\ \mathrm{~A} \\ \mathrm{~F} \\ \mathrm{~B} \end{gathered}$ | $\begin{array}{r} 13 \\ 0 \\ 340 \\ 28 \end{array}$ | $\begin{aligned} & \hline 0.138 \\ & 0.000 \\ & 1.424 \\ & 0.279 \end{aligned}$ | $\begin{array}{r} 9.3 \\ 0.7 \\ 282.3 \\ 15.0 \end{array}$ | $\begin{gathered} \hline \mathrm{A} \\ \mathrm{~A} \\ \mathrm{~F} \\ \mathrm{C} \end{gathered}$ |
| \#15-NH Route 28/Scobie Pond Road | $\begin{gathered} \text { EB L } \\ \text { SB all } \end{gathered}$ | $\begin{array}{r} 3 \\ 183 \end{array}$ | $\begin{aligned} & 0.022 \\ & 1.011 \end{aligned}$ | $\begin{array}{r} 9.5 \\ 143.2 \end{array}$ | $\begin{gathered} \mathrm{A} \\ \mathrm{~F} \end{gathered}$ | $\begin{array}{r} 5 \\ 318 \end{array}$ | $\begin{aligned} & 0.061 \\ & 2.116 \end{aligned}$ | $\begin{array}{r} 10.3 \\ * \end{array}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~F} \end{aligned}$ |
| \#16 - NH Route 102/NH Route 28 Bypass/East Derry Road (Traffic Circle-RT only) | $\begin{array}{r} \text { EDR WB } \\ 28 \text { Byp NB } \\ 28 \text { Byp SB } \\ 102 \mathrm{~EB} \\ 102 \mathrm{WB} \end{array}$ | $\begin{aligned} & 375 \\ & 175 \\ & 400 \\ & 475 \\ & 325 \end{aligned}$ | $\begin{aligned} & 1.031 \\ & 0.781 \\ & 1.058 \\ & 1.106 \\ & 1.026 \end{aligned}$ | $\begin{aligned} & 77.5 \\ & 29.5 \\ & 83.5 \\ & 96.6 \\ & 86.1 \end{aligned}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{D} \\ & \mathrm{~F} \\ & \mathrm{~F} \\ & \mathrm{~F} \end{aligned}$ | $\begin{aligned} & 450 \\ & 525 \\ & 750 \\ & 850 \\ & 100 \end{aligned}$ | $\begin{aligned} & 1.112 \\ & 1.268 \\ & 1.250 \\ & 1.456 \\ & 0.622 \end{aligned}$ | $\begin{array}{r} 103.3 \\ 169.4 \\ 146.4 \\ 240.0 \\ 24.6 \end{array}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{D} \\ & \mathrm{~F} \\ & \mathrm{~F} \\ & \mathrm{C} \end{aligned}$ |
| \#17 - NH Route 28Bypass/ <br> Pinkerton/Nesmith | EB L/T <br> EB R WB all NB all SB all | $\begin{array}{r} 125 \\ 40 \\ 245 \\ 30 \\ 0 \end{array}$ | $\begin{aligned} & \hline 3.388 \\ & 0.350 \\ & 1.371 \\ & 0.289 \\ & 0.014 \end{aligned}$ | $\begin{array}{r} \hline * \\ 13.6 \\ 296.3 \\ 9.5 \\ 8.5 \end{array}$ | $\begin{aligned} & \hline \mathrm{F} \\ & \mathrm{~B} \\ & \mathrm{~F} \\ & \mathrm{~A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{array}{r} 60 \\ 140 \\ 73 \\ 15 \\ 3 \end{array}$ | $\begin{aligned} & \hline 0.521 \\ & 0.692 \\ & 0.599 \\ & 0.175 \\ & 0.025 \end{aligned}$ | $\begin{array}{r} \hline 69.4 \\ 20.6 \\ 76.5 \\ 8.5 \\ 8.4 \end{array}$ | $\begin{aligned} & \hline \mathrm{F} \\ & \mathrm{C} \\ & \mathrm{~F} \\ & \mathrm{~A} \\ & \mathrm{~A} \end{aligned}$ |
| \#19-NH Route 102/Tsienneto Road | $\begin{array}{r} \text { EB L } \\ \text { SB L/R } \end{array}$ | $\begin{array}{r} 3 \\ 30 \end{array}$ | $\begin{aligned} & \hline 0.020 \\ & 0.287 \end{aligned}$ | $\begin{array}{r} 9.5 \\ 19.3 \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{C} \end{aligned}$ | $\begin{array}{r} 0 \\ 218 \end{array}$ | $\begin{aligned} & \hline 0.016 \\ & 0.869 \end{aligned}$ | $\begin{array}{r} 8.4 \\ 60.9 \end{array}$ | $\begin{gathered} \mathrm{A} \\ \mathrm{~F} \end{gathered}$ |

Note- Assumes 25 ft per queued vehicle

*     - calculated delay exceeds 300s


### 9.0 Summary of SNHPC Model Assignments - 2015, 2040

The SNHPC calibration of their regional traffic forecasting model was discussed with the Traffic Working Group (TWG) in October 2016. This calibration process was based on the least-mean squared comparison of the 2015 assignments (based on the various socioeconomic characteristics of each Traffic Analysis Zone (TAZ) used by the model to generate origins and destinations to be assigned to the network) to the calculated 2015 Average Annual Weekday Traffic (AAWDT) on the key links in the study area network that were derived from the extensive traffic counting program initiated at the start of this SDEIS project. This comparison was found to fall within the FHWA's acceptable margin of error for traffic modeling as summarized in Appendix D. As such, it was agreed by the TWG at this meeting that the model was in compliance with FHWA standards for model accuracy and could be used as a tool to reasonably project future volumes for this project.

It was further agreed by the TWG that the relative differences between the model AAWDT assignments for 2015 and 2040 would be applied to the calculated 2015 AAWDT volumes. AM and PM peak hour volumes were to be derived as a percentage of the AAWDT as determined in both the roadway and intersection turning movement count data. AAWDT assignments at individual intersections would be used to develop any adjustments to peak hour existing turning movements, based on both the increase/decrease in traffic volume as well as any changes in turning movement percentages of any particular movement. The derivation of these future intersection volumes was completed only after consensus was reached with the TWG on the reasonableness of the 2040 AAWDT traffic assignments for each alternative.

The future model includes known/programmed roadway improvements in the SNHPC's Regional Transportation Plan - 2015-2040 (SNHPC, 2017) that includes Exit 4A; however, this interchange was not included in any of the No-Build networks. While it was recognized that there may be locations where existing/projected capacity deficiencies may exist, only those projects either programmed in the State's Ten-Year Highway Plan (NHDOT, 2018) or the Regional Transportation Plan were included in the 2040 No-Build network.

The 2040 SNHPC model assignments were developed by including the population and employment projections for each community in the SNHPC model area, as outlined in the Lane Use Scenarios report (Louis Berger, 2017) and disaggregated to the TAZ level. This report also included alternative development scenarios without and with the proposed Exit 4A interchange, notably for the Woodmont Commons development on the east side of I-93, since the development of that parcel would be directly impacted by the location of the proposed interchange. In general, the Woodmont Commons-East development was assumed to reach its build-out potential under only the southerly interchange options (A and B), and would have a lesser development scenario under the 2040 No-Build C, D, and F alternatives.

It should also be noted that the Woodmont Commons traffic impact study for the full development project submitted to the Town of Londonderry (TEC, 2013) assumed that, because of the 'live-work-play' design intent of the proposed mixed-use development, a certain percentage of site-generated trips would remain 'internally captured' within the site itself and would not be assigned to the adjacent street network outside of the development. An adjustment factor of $23 \%$ was applied to the total site traffic generation for the various proposed land uses assumed in the Woodmont Commons traffic impact study to account for this estimated internal capture rate.

However, it should be noted that the methodologies used to develop trip generation, distribution and assignments for an individual traffic impact study versus a regional model are quite different. The model applies its trip distribution and assignment algorithms directly to the trip productions and attractions generated by each TAZ, based on their socioeconomic characteristics, which does not differentiate between trips that should or should not be assigned to other TAZs. In addition, the Woodmont Commons development is included as part of several TAZs, so correcting for only some trips from a particular TAZ and not others may appear to be arbitrary and jeopardize the validity of the model.

After consultation with the NHDOT Bureau of Traffic, it was agreed, as the initial step, all the model-generated traffic from all TAZs, including Woodmont Commons, was assigned to the SNHPC model network without regard to the internal capture rate assumptions noted in their site-specific traffic impact study. (NHDOT, 2017b) This should provide a conservatively worst-case estimate of traffic being assigned to the study area roadway network. Should the design intent of Woodmont Commons be realized and less traffic is actually generated as the project evolves, overall operations would be better than projected and the design life of any proposed improvements would be extended.

Individual spreadsheets were created for the key links in the network under each 2040 alternative for purposes of calculating the projected 2040 AAWDT and AM and PM peak hour volumes, based on the relative increase/decrease between 2015 and 2040 model assignments.

### 9.1 AAWDT Comparisons - 2040

Table 7 presents a summary of the projected 2040 AAWDT on key links in the study area roadway network, including the I-93 mainline and all interchange ramps. As noted above, these were derived by applying the growth rate between SNHPC's 2015 and 2040 model assignments to the calculated 2015 AAWDT derived from the updated traffic counting program created for this project. These assignments also provide projected volumes for newly created road segments, including the Exit 4A on- and off-ramps as well as the connector roadway between the new proposed interchange and the existing roadway network.
TABLE 7


### 9.1.1 No-Build Conditions

A review of the table indicates that there is a reduction in trips on north-south roadways such as NH Route 28 Bypass, NH Route 28 and Fordway under No-Build conditions. This appears to be as a result of the additional capacity provided by the widening of I-93 to four lanes each way which allows through traffic to use the interstate for these north-south trips as opposed to the local roadways through Derry. Mainline volumes on I-93 increase by between 64-68\% from 2015 and 2040, which is about a $2.5 \%$ annual growth rate. Volumes on the Exit 4 ramps increase between 95$125 \%$ from 2015 to 2040, while ramp volumes at Exit 5 only grow between 45-50\% during the same period. This would appear to indicate the influence of the Woodmont Commons development in Londonderry on both sides of the Interstate being accessed from either side of Exit 4, and is also reflected in volume increase on NH Route 102 west of the interchange. Local roads in the Woodmont area, such as Gilcreast Road and Ash Street, also experience marked increases in traffic volumes under 2040 NoBuild conditions.

### 9.1.2 Alternative A

Mainline volumes on I-93 show slightly higher growth rates under 2040 conditions with Exit 4A -Alternative A in place than in the No-Build condition. This is driven in part by Woodmont Commons because this development is assumed to reach its maximum potential with Alternative A in place, as opposed to either No-Build or most other Exit 4A options.

Exit 4 ramp volumes are affected to differing degrees with Alternative A in place. Growth rates for the NB on-ramp and SB off-ramp are about half what they are under the No-Build case, since this traffic is diverted to Exit 4A. The projected NB off-ramp volume of 17,385 vehicles per day (vpd), shows a $10 \%$ reduction over 2040 No-Build volumes. The development of Woodmont Commons to the west is reflected in the $10 \%$ increase in SB on-ramp volumes from the west side of the interchange, whereas the SB on-ramp volume from the east shows a $48 \%$ reduction in traffic that is now presumably using Exit 4A.

Exit 5 ramp volumes show greater increases on the NB off-ramp and SB on-ramp under Alternative A compared to the No-Build case. This would indicate increased interaction between Exit 4A and 5 to and from the north more than between Exits 4 and 4A, which is consistent with the findings in the previous DEIS for this project. (FHWA, 2007) The Exit 5 SB off-ramp actually shows a $43.5 \%$ reduction in traffic compared to No-Build, indicating that this traffic is likely continuing on the mainline down to Exit 4A. The NB on-ramp traffic volume is also about $20 \%$ lower than under No-Build conditions, indicating redistribution of some NB trips to Exit 4A and away from NH Route 28.

Exit 4A volumes range between 8,700-10,700 vehicles per day (vpd) on the NB offramp and SB on-ramp, and from 15,200 to $19,000 \mathrm{vpd}$ on the NB on-ramp and SB off-ramp, respectively. The two northerly-oriented ramps have the higher volumes, consistent with the increased interaction between the new interchange and Exit 5. The projected volume on the connector road east of the Alternative A interchange is $53,700 \mathrm{vpd}$.

The local roadways are also affected by the introduction of a new interchange to the regional network. Volumes on NH Route 102 just east of Exit 4 are about half of the projected 2040 No-Build condition, while volumes closer to the downtown area show reductions of around $19 \%$. Folsom Road shows significant increases, since it is now the primary connection between the new interchange and the local street network. Some of this increase continues easterly along the Tsienneto Road corridor ( +3000 vpd over No-Build) and NH Route 102 east at the Chester town line (+1000 vpd over No-Build).

### 9.1.3 Alternative B

Mainline volumes on I-93 under this scenario show similar growth rates as Alternative A as compared to 2040 No-Build conditions. This is consistent with the earlier DEIS when comparing southerly versus northerly interchange locations.

Exit 4 ramp volumes show some differences as compared to Alternative A. Projected volumes on the NB on-ramp and SB off-ramp are slightly higher under Alternative B than A, but still $17-19 \%$ less than what they are under the No-Build case. This may be because Alternative B provides a section of new roadway onto the Derry street network, which may attract more traffic. The NB off-ramp shows a $10 \%$ volume reduction under Alternative B than under No-Build, similar to Alternative A. This development of Woodmont Commons to the west is reflected in an $8 \%$ increase in SB on-ramp volumes from the west side of the interchange, whereas the SB on-ramp volume from the east shows about a $44 \%$ reduction in projected traffic, similar to Alternative A.

Exit 5 ramp volumes show smaller increases on the NB off-ramp and SB on-ramp than under Alternative A. This continues to indicate the increased interaction between Exit 4A and 5 to and from the north more than between Exits 4 and 4A, which is consistent with the previous DEIS for this project. The Exit 5 SB off-ramp actually shows a greater reduction in traffic under Alternative B than under A, and this is reflected in a similarly higher volume at the Exit 4A SB off-ramp as compared to Alternative A. The Exit 5 NB on-ramp traffic is also lower than under No-Build conditions or Alternative A, indicating redistribution of some NB trips to Exit 4A and away from NH Route 28. These results appear to show that this alternative supports more of a north-south trip pattern than the east-west pattern exhibited under Alternative A.

Exit 4A volumes with Alternative B range between 9,500-12,400 vpd on the NB offramp and SB on-ramp, and from 13,200 to 19,400 vpd on the NB on-ramp and SB off-ramp, respectively. The SB on- and off-ramp volumes are higher than under Alternative A, but the NB on-ramp traffic is slightly lower than under Alternative A. The projected connector road volume east of the Alternative B interchange are about $54,500 \mathrm{vpd}$, and decrease to 16,200 vpd east of NH Route 28 along the Ashleigh Drive alignment.

The projected volumes on the local roadways under Alternative B have similar but generally slightly lower volumes than Alternative A. Volumes on NH Route 102 just east of Exit 4 are about $48 \%$ of the projected 2040 No-Build condition, while volumes closer to the downtown area show reductions around $19 \%$. Folsom and Tsienneto Roads do not see the same increases as under Alternative A, since the new main connection road goes north of this area to intersect with Franklin Street Extension and Ashleigh Drive on the new alignment. The existing Tsienneto Road corridor sees minimal change since Alternative B creates a new roadway for the eastwest traffic that currently uses this roadway to access the Interstate, but traffic volumes at the east end of the study area are higher than under Alternative A.

### 9.1.4 Alternative C

Mainline volumes on I-93 south of Exit 5 under this scenario show slightly higher growth rates than the southerly interchange alternatives (A and B) when compared to 2040 No-Build conditions. Projected volumes north of Exit 5 are consistent across all interchange alternatives, being slightly higher than No-Build.

Exit 4 ramp volumes under this alternative are slightly lower than the southerly interchange options, notably on the NB on-ramp and SB off-ramp, but higher for the SB on-ramp from the east than either Alternative A or B. This is likely indicative of the increased distance of the northerly interchange from the NH Route 102 corridor and the expectation of less effectiveness in reducing east-west traffic through the downtown area.

Impacts on Exit 5 ramp volumes show larger reductions in both the NB on-ramp and SB off-ramp volumes than the southerly interchange options. This makes sense, given the greater proximity of Alternatives C (and D) to Exit 5, which further emphasizes the increased interaction between Exit 4A and 5 to and from the north more than between Exits 4 and 4A, which is consistent with the previous DEIS for this project.

Exit 4A ramp volumes for trips to/from the south with Alternative C are noticeably lower than with the southerly interchange options, ranging between $2,800-5,000 \mathrm{vpd}$ on the NB off-ramp and SB on-ramp. Trips on the NB on-ramp are similar to Alternative B but are lower on the SB off-ramp, respectively. The projected connector road volume east of the C interchange is less than under A or B (about $38,500 \mathrm{vpd}$ ), and decrease to 13,900 vpd west of NH Route 28 along the Ashleigh Drive alignment.

The projected volumes on the local roadways under Alternative C have similar but slightly larger volume reductions than Alternatives A or B. Volumes on NH Route 102 just east of Exit 4 are slightly lower than 2040 No-Build volumes but slightly higher than 2015 base conditions. Volumes further east on NH Route 102 show slightly larger reductions than under A or B . With the main connection road going north to NH Route 28 near the town line, volumes on this section of NH Route 28 more than double than under existing conditions. The existing Tsienneto Road corridor sees similar volume levels as Alternative B since C follows the new roadway to serve this east-west traffic demand.

### 9.1.5 Alternative D

Mainline volumes on I-93 under this scenario show similar growth rates as Alternative C as compared to 2040 No-Build conditions. This is consistent with the earlier DEIS where comparing southerly versus northerly interchange locations. Exits 4 and 5 ramp volumes under this option are also quite similar to Alternative C.

Exit 4A volumes with Alternative D are similar to Alternative C - the NB off-ramp and SB on-ramp volumes are lower than Alternative C but the SB off-ramp traffic is slightly higher. The projected connector road volume east of the Alternative D interchange is about $36,700 \mathrm{vpd}$.

The projected volumes on the local roadways under Alternative D have similarly but generally slightly lower reductions than Alternatives A or B. Volumes on NH Route 102 just east of Exit 4 are about the same as under 2015 base conditions, even if slightly lower than 2040 No-Build volumes. Volumes further east on NH Route 102 show smaller traffic reductions than any of the other interchange options. With the main connection road going north to NH Route 28 near the town line, volumes along this part of the NH Route 28 corridor more than double over existing conditions. The existing Tsienneto Road corridor also sees marked growth over existing volumes with this option since it follows the present roadway for east-west traffic.

### 9.1.6 Alternative F

Alternative F is essentially the Transportation Systems Management (TSM) option, which from the traffic model's perspective is essentially a third lane along NH Route 102 to provide some additional capacity at intersections east of Exit 4 into downtown Derry.

Mainline volumes on I-93 under this scenario show similar growth rates compared to 2040 No-Build conditions and lower than with an interchange alternative. This is consistent with the lower growth scenario as compared to those with a new interchange. Exits 4 and 5 ramp volumes under this option are also quite similar to 2040 No-Build conditions. With the provision of some additional capacity along the existing NH Route 102 corridor easterly into downtown Derry, traffic volumes are
higher than under No-Build conditions or with any of the interchange alternatives, so it does not meet the Purpose and Need for the project.

Figures 8 through 12 graphically show these volume comparisons by alternative for key areas of interest as part of this study: the Exit 4 ramps, Exit 5 ramps, Exit 4A ramps, points along the NH Route 102 corridor, and other local streets of interest, respectively.

### 9.2 Composition of Through Traffic in Downtown Derry

While the volume reductions may not be as profound on the surface as one might expect, it is the composition of the trips in the downtown area that are of interest, since one of the Purposes and Needs of the project is to reduce through traffic in downtown Derry that had neither an origin nor destination there. Existing travel patterns suggest that a good deal of existing traffic is already finding alternative routes to avoid the downtown area.

To test the sensitivity of the hypothesis of a reduction in 'through' traffic as a result of a new interchange, a link on NH Route 102 just west of the main downtown area, which is the location east of Griffin Street near the Beaver Brook bridge, was chosen as a representative location of downtown traffic. The SNHPC model can generate trip tables that will provide the origin and destination zone for trips on any link in the network in either direction. This traffic pattern was evaluated by comparing the number of trips from zones and external stations from the east and northeast that are currently assigned to that link under existing (2015) base, 2040 No-Build and 2040 -Alternative A conditions, which was the Preferred Alternative in the previous DEIS for this project, that might be diverted to another route/path under any Build scenario.

A series of TAZs from the SNHPC traffic model area to the east and northeast were aggregated to see how many trips remained on this link under the different scenarios, as shown in Figures 13 and 14. The ones of primary interest were noted as follows:

- North Derry - TAZs 121-124, 126, 127
- East Derry - TAZs 128-130, 145-147, 221, 225
- Chester - TAZs 148-155
- Raymond/Deerfield/Candia - TAZs 156-191
- External Stations east and northeast - Stations 308-324

Table 8 shows a summary of the assigned trips to this link in each direction as well as combined under the three scenarios. In summary, the table shows that, in general, the trips to and from these zones to the east that now pass through the downtown area are lower with an interchange alternative (in this case, Alternative A) in place than under the 2040 No-Build scenario. However, since the overall link volume is reduced as well, these trips make up a slightly higher percentage of the total trips on that link than under NoBuild conditions. This appears logical, because this link is likely the shortest path from these easterly zones to destinations in downtown Derry. Nevertheless, this analysis appears to show that an interchange alternative will reduce the amount of through traffic in downtown Derry for trips to and from the east and northeast.

TABLE 8
SELECT LINK ANALYSIS NH ROUTE 102, EAST OF GRIFFIN ROAD, DERRY, NH

| Eastbound (To) | N Derry | E Derry | Chester | Raymond/Candia/ Deerfield | N/NE/SE <br> External <br> Stations |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Traffic Zones | $\begin{gathered} \text { 121-124. } \\ 126,127 \end{gathered}$ | $\begin{aligned} & 128-130 \\ & 145-147 \\ & 221,225 \\ & \hline \end{aligned}$ | 148-155 | 156-191 | 308-324 | Target zone total | Increase over 2015 Base | Total trips on link | $\%$ of total to target zones |
| 2015 Base | 1194 | 642 | 162 | 293 | 1209 | 3500 |  | 8,806 | 39.7\% |
| $\%$ total on link | 13.6\% | 7.3\% | 1.8\% | 3.3\% | 13.7\% |  |  |  |  |
| 2040 No-Build | 1332 | 1056 | 130 | 78 | 1282 | 3878 | 1.1\% | 9,642 | 40.2\% |
| \% total on link | 13.8\% | 11.0\% | 1.3\% | 0.8\% | 13.3\% |  |  |  |  |
| 2040 Alt A | 571 | 1235 | 236 | 146 | 1845 | 4033 | 1.2\% | 9,108 | 44.3\% |
| \% total on link | 6.3\% | 13.6\% | 2.6\% | 1.6\% | 20.3\% |  |  |  |  |
| Westbound (From) | N Derry | E Derry | Chester | Raymond/Candia/ Deerfield | N/NE/SE <br> External <br> Stations |  |  |  |  |
| Traffic Zones | $\begin{gathered} 121-124 . \\ 126,127 \end{gathered}$ | $\begin{aligned} & 128-130, \\ & 145-147, \\ & 221,225 \\ & \hline \end{aligned}$ | 148-155 | 156-191 | 308-324 | Target zone total | Increase over 2015 Base | Total trips on link | $\%$ of total to target zones |
| 2015 Base | 1177 | 814 | 114 | 192 | 760 | 3057 |  | 9,191 | 33.3\% |
| \% total on link | 12.8\% | 8.9\% | 1.2\% | 2.1\% | 8.3\% |  |  |  |  |
| 2040 No-Build | 1663 | 1465 | 64 | 37 | 773 | 4002 | 1.1\% | 11,168 | 35.8\% |
| \% total on link | 14.9\% | 13.1\% | 0.6\% | 0.3\% | 6.9\% |  |  |  |  |
| 2040 Alt A | 307 | 1097 | 156 | 113 | 1073 | 2746 | 0.8\% | 7,776 | 35.3\% |
| \% total on link | 3.9\% | 14.1\% | 2.0\% | 1.5\% | 13.8\% |  |  |  |  |
| Both Directions | N Derry | E Derry | Chester | Raymond/Candia/ Deerfield | N/NE/SE <br> External Stations |  |  |  |  |
| Traffic Zones | $\begin{gathered} 121-124 . \\ 126,127 \end{gathered}$ | $\begin{aligned} & 128-130, \\ & 145-147, \\ & 221,225 \end{aligned}$ | 148-155 | 156-191 | 308-324 | Target zone total | Increase over 2015 Base | Total trips on link | \% of total <br> to target <br> zones |
| 2015 Base | 2371 | 1456 | 276 | 485 | 1969 | 6557 |  | 18,002 | 36.4\% |
| \% total on link | 13.2\% | 8.1\% | 1.5\% | 2.7\% | 10.9\% |  |  |  |  |
| 2040 No-Build | 2995 | 2521 | 194 | 115 | 2055 | 7880 | 2.3\% | 20,810 | 37.9\% |
| \% total on link | 14.4\% | 12.1\% | 0.9\% | 0.6\% | 9.9\% |  |  |  |  |
| 2040 Alt A | 878 | 2332 | 392 | 259 | 2918 | 6779 | 1.9\% | 16,885 | 40.1\% |
| \% total on link | 5.2\% | 13.8\% | 2.3\% | 1.5\% | 17.3\% |  |  |  |  |

### 9.3 Comparison to I-93 SEIS 2030 Mainline Projections

An additional comparison was made to the projected 2030 mainline volumes on I-93 as shown in the SEIS for the I-93 project (NHDOT, 2009). This document utilized the statewide traffic model that was available at the time, and also included the proposed Exit 4A Preferred Alternative as part of the network.

However, there are some major differences between the two scenarios. First, there are two different design years: the I-93 SEIS went out only to 2030 while this Exit 4A SDEIS extends out to 2040 , so there are ten more years of overall growth that contributes additional traffic onto the network. Secondly, the I-93 SEIS did not account for the full Woodmont Commons development scenario included in the Exit 4A project for the Preferred Alternative, which adds a substantial number of trips to the area in and around Exit 4 and the proposed Exit 4A. Given these factors, it is expected that design hourly volumes would be higher under the 2040 case.

Table 9 shows excerpts from Tables 4-12 and 4-13 from the 2009 I-93 SEIS, which includes the projected ADT and DDHV for 2020 and 2030 from that document. The current table includes a projection of these volumes to 2040 using the same growth rates, including Exit 4A which was included in the I-93 SEIS Build condition, and the projected AAWDT and DDHV from the latest SNHPC modeling to the 2040 design year, and a comparison between the two modelling efforts.

These comparisons show that the more recent SNHPC AAWDT traffic projections are consistent with the growth trend line from the I-93 SEIS if it were extended to the same 2040 design year within less than $4 \%$. Similarly, the differences calculated DDHV extended to 2040 are within $3 \%$ when using the same methodology. The last two points on the graphs compare the 2040 projections for both the I-93 numbers and the latest SNHPC projections. Therefore, it would appear that the two modelling efforts are reasonably close to each other when extending the original I-93 design horizon out to 2040.

The original I-93 SEIS also noted that the congested flow capacity for I-93 would be $1,800 \mathrm{vph}$ per lane, which would be $7,200 \mathrm{vph}$ for the projected four-lane Interstate project. Should this volume be exceeded, the volumes would have to be adjusted to account for the effect of peak spreading that would likely occur into the adjacent hours before and after this demand was projected. At first glance, it appears that this scenario may also occur between Exits 4A and 5 and north of Exit 5 when using the SNHPC 2040 model projections, using the same DDHV calculation assumptions as in the I-93 SEIS. However, a more detailed review of the projected 2040 mainline volumes, which are discussed below, indicates that this $7,200 \mathrm{vph}$ threshold will not likely be reached under any Exit 4A scenario.

TABLE 9

## COMPARISON OF I-93 SEIS AND EXIT 4A SDEIS TRAFFIC PROJECTIONS 2020, 2030 AND 2040 DESIGN YEARS, INCLUDING EXIT 4A

## Average Annual Weekday Traffic (AAWDT) Projections

| I-93 Segment | I-93 SEIS |  |  |  | SNHPC 2040 <br> Model Projections <br> Alternative A | \% Difference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2020 | 2030 | Growth | Projected |  |  |
|  | Build | Build | Rate/Year | To 2040 |  |  |
| Exit 3 to Exit 4 | 94,800 | 109,000 | 1.014 | 125,330 | 120,860 | -3.6\% |
| Exit 4 to Exit 4A | 88,200 | 101,500 | 1.014 | 116,810 | 118,015 | 1.0\% |
| Exit 4A to Exit 5 | 100,600 | 116,100 | 1.014 | 133,990 | 132,734 | -0.9\% |
| North of Exit 5 | 97,600 | 113,100 | 1.015 | 131,060 | 128,466 | -2.0\% |



Notes:
DDHV calculated as $9.4 \%$ of ADT with a 60/40 directional split, consistent with I-93 SEIS, using Scenario 2 (OEP Projections)

Source: NHDOT, Supplemental Environmental Impact Statement and Reevaluation/Section4(f)
Evaluation, August 2009, Tables 4-12 and 4-13

TABLE 9 (Cont'd)
COMPARISON OF I-93 SEIS AND EXIT 4A SDEIS TRAFFIC PROJECTIONS 2020, 2030 AND 2040 DESIGN YEARS, INCLUDING EXIT 4A

Directional Design Hourly Volume (DDHV) Projections

|  | I-93 SEIS |  |  |  | SNHPC 2040 |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| I-93 Segment | Build | Build | Growth | Projected | Calculated DDHV |  |
|  |  |  |  | Coar | To 2040 | Alternative A |$\quad$ \% Difference



Notes:
DDHV calculated as $9.4 \%$ of ADT with a 60/40 directional split, consistent with I-93 SEIS, using Scenario 2 (OEP Projections)

Source: NHDOT, Supplemental Environmental Impact Statement and Reevaluation/Section4(f)
Evaluation, August 2009, Tables 4-12 and 4-13

### 10.0 Derivation of 2040 Volumes for Analysis Purposes

Now that the projected 2040 AAWDT volumes have been provided by the SNHPC model and appear to be reasonable, these need to be reduced to AM and PM peak volumes for analysis purposes. Since the SNHPC model provides only daily volumes, these must be reduced to peak hours on both the I-93 mainline and interchange ramp terminals as well as at the various study area intersections that may be directly or indirectly affected by any alternative. Different procedures were used to develop these volumes to be used for analysis purposes.

As noted earlier, the full development potential of Woodmont Commons was assigned to the study area traffic model network as a worse-case scenario, but if much of the sitegenerated traffic is captured internally to the site - as is the design intent of this mixeduse development - operations would be better than projected and the design life of any roadway and intersection improvements would be extended.

### 10.1 Mainline Interstate Volumes

A different procedure was used to generate the 2040 No-Build interstate networks as was done for deriving the 2015 base network for calibration. The projected 2040 AAWDT was calculated based on the projected growth (positive or negative) reflected in the model assignments on that segment between 2015 and 2040, then this growth rate was applied to the adjusted 2015 AAWDT. Then, the 2040 projected AM and PM peak hour volumes were derived based on the percentage that the existing (2015) AM and/or PM peak hour volume was as a percentage of the adjusted 2015 AAWDT, since these percentages should not change substantially over time. These peak hour percentages generally fell in the range of $6-9 \%$ of AAWDT. Tables J-1 through J-6 in Appendix J show summary tables of the projected 2040 peak hour volumes for each alternative on the key links on the interstate and local roadway networks.

As in the 2015 base case, the most logical starting point for developing the balanced interstate networks is south of Exit 4, where NHDOT permanent recorder data should provide more reliability. The various interchange ramp volumes were then taken directly from the appropriate tables in Appendix J, and the mainline volumes were balanced through the network to the point north of Exit 5. This process was followed to develop 2040 AM and PM peak hour volumes along the Interstate for each alternative, which are shown graphically in Figures 15 through 26.

### 10.2 Local Intersection Volumes

A more detailed procedure was needed to derive peak hour intersection volumes for each alternative from the regional traffic model to be used for design purposes. Since the SNHPC model only provides daily volumes, a relationship needs to be established between the peak hour volumes from the actual turning movement count at any intersection and the model output that can be made available. The SNHPC model can provide daily volumes between any two nodes through one central node that would
simulate movements at an intersection. As such, information was requested from SNHPC for the daily model assignments for each study area intersection for each alternative to assist in developing turning movements at each location. Then a procedure was developed to estimate intersection turning movements at each study area location based on the existing turning movement volumes for both the AM and PM peak hours and how the total and individual turn volumes change as a result of the reassignment of traffic under any scenario. This process had to be usable regardless of alternative or the magnitude of change in traffic assignments for any movement at a specific intersection from one alternative to another. The procedure is discussed in greater detail in the memorandum dated September 29, 2017, which is attached in Appendix K. The memo was reviewed and approved by the NHDOT before the procedure was applied to the rest of the alternatives (NHDOT, 2017c).

The resulting AM and PM peak hour volumes for each study area intersection for each of the 2040 alternatives are provided in Figures 27 through 38.

### 11.0 Analysis of Interstate Operations

As in the existing case, the Freeway Facilities procedure from the 2010 HCM and replicated in the HCS was used to evaluate the mainline interstate operations under all 2040 conditions. A free flow speed of 70 mph and a Peak Hour Factor of 0.94 were agreed upon by NHDOT (NHDOT, 2017d) to be used in the HCM analysis. With the introduction of a northerly or southerly interchanges, certain design parameters consistent with the I-93 layout were agreed upon with the NHDOT to ensure that the appropriate distances would be used in the analyses. A conceptual layout for the southerly interchange for Alternatives A and B had already been provided in the 2007 DEIS as well as part of the I-93 design between Exits 4 and 5, and was used to determine ramps spacing for analysis purposes. The previous conceptual layout for the northerly interchange for Alternatives C and D from the 2007 DEIS was used as the starting point for this study.

The HCM procedure accounts for a 1,500 foot 'influence area' in the ramp merge or diverge areas. With the southerly interchange, there is overlap between the influence areas of the Exit 4 NB on-ramp and the Exit 4A NB off-ramp, as well as the Exit 4A SB on-ramp and the Exit 4 SB off-ramp. As such, the HCS analysis software allows for this overlap to be considered, and is reflected in the results.

The Freeway Facilities criteria in the HCS were provided in Appendix E when the 2015 operations were discussed for the existing two-lane facility. The 2040 results for the proposed four-lane facility are summarized in Table 10 with the HCM printouts provided in Appendix L. By definition, if the demand/ capacity ( $\mathrm{d} / \mathrm{c}$ ) ratio is greater than 1.00 , ramp merge/diverge or mainline operations will be constrained, either by traffic unable to merge onto the interstate and subsequently affecting 'topside' operations at the ramp terminals, or by the off-ramp being unable to process the demand for exiting traffic, which may affect mainline traffic free flow speeds.

The 2040 cases where $\mathrm{d} / \mathrm{c}$ ratios are 0.98 or greater, indicating potential capacity constraints to I-93 operations with a single-lane ramp, are noted below:

- Alternative A - Exit 4A SB off-ramp diverge - AM peak
- Alternative B - Exit 4A SB off-ramp diverge - AM peak
- Alternative B - Exit 4 NB on-ramp merge - AM peak
- Alternative B - Exit 4 SB off-ramp diverge - PM peak
- Alternative F - Exit 4 NB on-ramp merge - AM and PM peaks
- Alternative F - Exit 4 SB off-ramp diverge - PM peak

These results appear to reflect the increased demands from the higher development scenarios from the Woodmont Commons development under Alternatives A and B, as well as the projected limitations at the Exit 4 interchange with Alternative F in place, even with a lesser development scenario for Woodmont Commons.

If the projected Exit 4 NB on-ramp volumes reach levels where the merge with the mainline I-93 is affected as shown, it would likely result in backups of traffic back to the ramp terminal itself, affecting the topside intersections along NH Route 102. Both the Exit 4 and Exit 4A SB off-ramp diverge constraints could be ameliorated by providing a two-lane off-ramp to service the projected traffic should actual volumes meet projections in the future.

However, given the aforementioned discussion about the possible realization of the Woodmont Commons internal capture rate and the subsequent reduction in traffic assignments onto the study area network, a sensitivity analysis was conducted at the Exit 4A SB off-ramp to determine what kind of volume reduction would be needed to provide an acceptable LOS for a single-lane off-ramp at this location. If the projected off-ramp AM peak volume was reduced by only 200 vph , this ramp would function at a LOS D with a demand/capacity ratio of 0.94 , which would be acceptable. Therefore, should the full impact of the traffic projections from Woodmont Commons or the overall study area development scenario not be realized, the ramps that are projected to be capacityconstrained may operate better than these analyses would indicate.



### 12.0 Estimated Contribution of Woodmont Commons Traffic to Interstate Ramp Volumes

During the review of the traffic projections, the NHDOT inquired as to the potential impact that traffic from the Woodmont Commons development may have on the Exit 4 ramps under the various alternatives, since the southerly interchange alternatives (A and B) assume a higher intensity of development that under all other alternatives, including the No-Build.

As noted earlier, the 2040 projections from the SNHPC regional traffic model do not account for the same level of 'internally captured' trips within the development itself in the traffic assignments used for the Exit 4A project, as opposed to the site-specific traffic study prepared for the Woodmont project that assumed as much as a $23 \%$ internal captured trip rate in their projections and traffic assignments (TEC, 2013). Nevertheless, the model assignments should be able to present an 'order of magnitude' assessment of the relative contribution of traffic to the Exit 4 and 4A ramps from the three traffic analysis zones that Woodmont Commons would eventually occupy.

To accomplish this, SNHPC was tasked with providing 'select link' assignments to the Exit 4 and 4A ramps for trips from the three Woodmont Common zones (Zone 277 to the west, and Zones 69 and 375 to the east) under different scenarios: 2015 No-Build; 2040 No-Build; and 2040 Build with either Alternative A (southern interchange) and Alternative C (northern interchange). This information was summarized in a technical memo provided to the NHDOT for their review and concurrence (CLD, 2018), which is attached in Appendix M.

The results show that under the 2015 No-Build case, the three Woodmont zones only account for about $13 \%$ of the total traffic volume on all Exit 4 ramps, almost exclusively from the existing development in Zone 277 on the west side of I-93 in the Garden Lane area. Under the 2040 No-Build condition, the total volumes on the Exit 4 ramps would more than double, even with a lesser Woodmont development scenario, and these three zones now comprise almost $27 \%$ of this total Exit 4 ramp traffic and almost $40 \%$ of the projected increase in traffic.

With Exit 4A in place under Alternative A, which also assumes the most intense Woodmont development scenario, traffic assignments from the three subject zones account for $36 \%$ of the total Exit 4 ramp volume, most of which comes from Zone 277 on the west side. At Exit 4A, the two easterly Woodmont zones also account for $36 \%$ of total Exit 4A ramp traffic with no traffic assigned to these ramps from the west side.

With Alternative C in place, which assumes the same development scenario for Woodmont as in the 2040 No-Build case, the total traffic on the Exit 4 ramps is roughly the same as under Alternative A, but the Woodmont contribution is a slightly lower percentage ( $32 \%$ ) of the total. At Exit 4A, Woodmont traffic would comprise only about $1 \%$ of the total ramp assignments, given that it is further removed from the traffic zones in question.

This analysis is only intended to show the relative potential contribution of Woodmont Commons traffic to both Exits 4 and 4A based on the full assignment of this traffic to the network as reflected in the SNHPC regional traffic model. As the Woodmont Commons development progresses and traffic is added to the adjacent road network, this situation should be monitored to determine how the actual additional traffic impacts affect overall traffic operations. Should the magnitude of the 'internal capture' trip rate be closer to what the TEC study anticipated, operations on the ramps, their intersections with the local road system, and the overall Interstate system would be better than by using the more conservative SNHPC model projections.

### 13.0 Exit 4A and Connecting Roadways

The Exit 4A interchange is currently proposed as a diamond configuration with access only to and from the east. As such, it creates two new ramp terminal intersections that will be provided with sufficient lanes to operate at an acceptable LOS. The connector road to the existing roadway network was assumed to be a four-lane limited access arterial roadway between the interchange and NH Route 28 to the east, with future breaks in access reserved for the proposed Woodmont Commons-East parcel based on their future development layout. New intersections would be created under all Build alternatives and existing intersections that would be affected by each of the respective layouts would need to be upgraded, which will be discussed in the next section.

The following is a listing of new intersections created by the connector roadway under the various interchange alternatives:

- Alternative A - Connector Road with North High Street.
- Alternative B - Connector Road with Franklin Street Extension, NH Route 28 Bypass, and relocated Tsienneto Road. In addition, the existing intersection with Ashleigh Drive will be reconfigured.
- Alternative C-Connector Road with NH Route 28 near the Londonderry town line, as well as NH Route 28 Bypass and relocated Tsienneto Road.
- Alternative D - Connector Road with NH Route 28 near Londonderry town line.


### 14.0 Analysis of Local Intersection Operations

Only those known programmed projects in the SNHPC 2040 Long-Range Transportation Plan (SNHPC, 2017) were included as foreseeable projects in the traffic modeling for this study. However, it is also assumed that ongoing State and Town traffic maintenance projects, such as signal retiming and optimization, will occur during the duration of the design horizon. Therefore, any intersection analyses assumes the optimization of signal timing and phasing at a specific location as a base condition, with any additional lane improvements evaluated as an impact associated with a specific alternative.

In addition, the Woodmont Commons development has also developed conceptual plans along the NH Route 102 corridor, as well as other intersections in Londonderry and Derry, to accommodate their projected traffic as that project moves forward (TEC, 2013). The NHDOT has agreed that these projects should be considered as part of the 2040

No-Build condition (NHDOT, 2016f). While most of these future improvements on NH Route 102 are west of Exit 4, including the Garden Lane and Gilcreast Road intersections, there are other improvements in the Exit 4A study area east of I-93 that will be considered as part of this No-Build condition for analysis purposes. These include:

- \# 5 - NH Route 102/Londonderry Road intersection - signalization and lane additions, including a second east-west through lane on NH Route 102.
- \# 8- North High Street/Ash Street Extension - providing a four-way stop controlled intersection, as well as separate left- and right-turn lanes exiting Ash Street, and adding an exclusive SB right-turn lane from North High Street onto Ash Street Extension.

It also should be noted that not all of the study area intersections are directly affected by the Exit 4A alternatives, even though the redistribution of traffic will have an indirect effect. Only those intersections that a specific alternative passes through were considered for any additional improvements as part of the project to maintain an acceptable LOS D or better for the overall intersection as well as on any individual approach. Analyses were conducted for all of the study area intersections, either with or without any required improvements.

It was also assumed that signalization would be required at many of the existing unsignalized locations where an alternative passes through it or where new intersections were being created at major State or local roadways. No formal signal warrants study was performed, but engineering judgment was applied to treat each of these locations the same if they were part of the layout of an alternative. Conversely, if the alternative did not go through that location, the existing traffic control was assumed to remain in place, regardless of operational efficiency, since these locations have not yet been programmed for further improvements.

## 15. Signalized Intersections

A summary table for the comparison of lane use and operations at each existing or proposed signalized intersection is provided in Table 11. No additional improvements to the lane use at the Exits 4 and 5 ramp terminals were investigated as part of any Build alternative, since these are being reconstructed as part of the ongoing I-93 project. The results are provided using the HCM 2000 procedures, since these procedures can address many non-standard timing and phasing parameters that later versions of the HCM cannot, as well as to be consistent with the Interstate Justification Report being conducted separately. (Louis Berger, 2018). The actual HCM and Synchro printouts for all the 2040 alternatives are provided in Appendices N through S.

| Intersection | 2040 Alternative | Table 11 <br> 0 Capacity Analyses by Alternative <br> $\underline{\text { Signalized Intersections }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  |  | PM Peak Hour |  |  | Comments/ <br> Lane Use Revisions |
|  |  | $\begin{gathered} \mathrm{v} / \mathrm{c} \\ \text { ratio } \end{gathered}$ | Average Delay | LOS | v/c ratio | Average Delay | LOS |  |
| \#1-Exit 4 SB Off Ramp/NH 102 | No-Build | 1.08 | 44.5 | D | 1.22 | 106.4 | f | Current lane use per I93 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project |
|  | Alternative A | 0.92 | 25.9 | C | 1.09 | 50.9 | D |  |
|  | Alternative B | 0.93 | 26.8 | C | 1.09 | 53.9 | D |  |
|  | Alternative C | 1.00 | 36.1 | D | 1.09 | 57.2 | E |  |
|  | Alternative D | 0.99 | 35.1 | D | 1.11 | 59.6 | E |  |
|  | Alternative F | 1.09 | 51.0 | D | 1.14 | 61.5 | E |  |
| \#2 - Exit 4 NB Off Ramp/NH 102 | No-Build | 1.10 | 61.4 | E | 1.12 | 92.8 | F | Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project |
|  | Alternative A | 1.04 | 71.2 | E | 1.11 | 115.1 | F |  |
|  | Alternative B | 0.99 | 54.8 | D | 1.06 | 88.0 | F |  |
|  | Alternative C | 1.02 | 62.1 | E | 1.05 | 82.0 | F |  |
|  | Alternative D | 1.04 | 67.3 | E | 1.06 | 81.8 | F |  |
|  | Alternative F | 1.06 | 57.5 | E | 1.15 | 91.8 | F |  |
| $\begin{aligned} & \text { \#3 - Exit } 5 \text { SB Off } \\ & \text { Ramp/NH } 28 \end{aligned}$ | No-Build | 1.17 | 77.0 | E | 0.90 | 31.2 | C | Current lane use per I93 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per I93 project Current lane use per 193 project |
|  | Alternative A | 1.06 | 49.3 | D | 0.83 | 20.1 | C |  |
|  | Alternative B | 0.86 | 28.0 | C | 0.70 | 16.9 | B |  |
|  | Alternative C | 0.83 | 22.9 | C | 0.62 | 15.0 | B |  |
|  | Alternative D | 0.82 | 23.3 | C | 0.61 | 15.2 | B |  |
|  | Alternative F | 1.10 | 62.1 | E | 0.87 | 27.8 | C |  |
| \#4 - Exit 5 NB Off Ramp/NH 28 | No-Build | 1.10 | 51.7 | D | 1.04 | 37.7 | D | Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project Current lane use per 193 project |
|  | Alternative A | 1.11 | 63.0 | E | 0.99 | 39.2 | D |  |
|  | Alternative B | 1.03 | 50.2 | D | 0.93 | 33.9 | C |  |
|  | Alternative C | 1.02 | 49.9 | D | 0.87 | 27.7 | C |  |
|  | Alternative D | 1.02 | 50.5 | D | 0.89 | 32.6 | C |  |
|  | Alternative F | 1.07 | 44.0 | D | 0.99 | 35.1 | D |  |
| \#5 - NH Rte 102/Londonderry Rd/ St. Charles Street | No-Build | 0.85 | 17.7 | B | 1.16 | 67.5 | E | Add 2nd E-W lane per Woodmont concept Add 2nd E-W lane per Woodmont concept Add 2nd E-W lane per Woodmont concept Add 2nd E-W lane per Woodmont concept Add 2nd E-W lane per Woodmont concept Add 2nd E-W lane per Woodmont concept |
|  | Alternative A | 0.52 | 11.4 | B | 0.58 | 14.8 | B |  |
|  | Alternative B | 0.48 | 7.2 | A | 0.54 | 14.2 | B |  |
|  | Alternative C | 0.52 | 8.2 | A | 0.53 | 13.1 | B |  |
|  | Alternative D | 0.56 | 8.3 | A | 0.65 | 16.3 | B |  |
|  | Alternative F | 0.75 | 12.3 | B | 0.87 | 27.9 | C |  |
| \#6 - NH Rte 102/Fordway/Madden Hill Road | No-Build | 0.92 | 30.8 | C | 1.04 | 47.3 | D | Current lane use <br> Current lane use <br> Current lane use <br> Current lane use <br> Current lane use <br> Add NB LT, EB RT lanes |
|  | Alternative A | 0.79 | 23.4 | C | 0.99 | 42,5 | D |  |
|  | Alternative B | 0.80 | 23.0 | C | 0.91 | 29.1 | C |  |
|  | Alternative C | 0.78 | 22.3 | C | 0.92 | 30.0 | C |  |
|  | Alternative D | 0.81 | 23.2 | C | 0.94 | 30.2 | C |  |
|  | Alternative F | 0.93 | 28.7 | C | 0.96 | 29.9 | C |  |
| \#7-NH Rtes 102/28 | No-Build | 0.88 | 47.4 | D | 0.79 | 37.5 | D | Current lane use <br> Current lane use <br> Current lane use <br> Current lane use <br> Current lane use <br> Add NB LT, WB Th, EB RT lanes |
|  | Alternative A | 0.89 | 55.3 | E | 0.84 | 47.9 | D |  |
|  | Alternative B | 0.87 | 44.1 | D | 0.80 | 40.5 | D |  |
|  | Alternative C | 0.77 | 35.0 | C | 0.84 | 40.2 | D |  |
|  | Alternative D | 0.89 | 48.1 | D | 0.86 | 46.2 | D |  |
|  | Alternative F | 0.63 | 28.6 | C | 0.83 | 34.0 | C |  |


| Table 11 (Cont'd) <br> Summary of 2040 Capacity Analyses by Alternative <br> Signalized Intersections |  |  |  |  |  |  |  | Comments/ <br> Lane Use Revisions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | 2040 Alternative | AM Peak Hour |  |  | PM Peak Hour |  |  |  |
|  |  | $\begin{gathered} \mathrm{v} / \mathrm{c} \\ \text { ratio } \end{gathered}$ | Average Delay | LOS | $\begin{gathered} \mathrm{v} / \mathrm{c} \\ \text { ratio } \end{gathered}$ | Average Delay | LOS |  |
| \#9A - Connector Rd/N High $\mathbf{S t}$ | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | 0.59 | $\begin{aligned} & \hline \mathrm{n} / \mathrm{a} / \\ & 25.0 \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \end{aligned}$ | C | 0.95 | n/a/ <br> 37.5 <br> $\mathrm{n} / \mathrm{a} /$ <br> $\mathrm{n} / \mathrm{a} /$ <br> n/a/ <br> n/a/ | D | Does not exist <br> Prop lane use: EB - T,T,R; WB-L,T,T; <br> NB- L,L,R lanes <br> Does not exist <br> Does not exist <br> Does not exist <br> Does not exist |
| \#10-N <br> High/Folsom/Franklin Sts. | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | 0.65 | $\begin{aligned} & \mathrm{n} / \mathrm{a} / \\ & 17.9 \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \end{aligned}$ | B | 0.92 | $\begin{aligned} & \mathrm{n} / \mathrm{a} / \\ & 32.2 \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \end{aligned}$ | C | Would remain unsignalized <br> EB - L,T,T,TR; WB-L,T,TR; SB- LT,R; <br> NB- L,TR lanes <br> Would remain unsignalized <br> Would remain unsignalized <br> Would remain unsignalized <br> Would remain unsignalized |
| \#11- Ross' Corner (Folsom/NH 28) | No-Build Alternative A | $\begin{aligned} & \hline 0.72 \\ & 0.56 \end{aligned}$ | $\begin{aligned} & \hline 91.3 \\ & 22.3 \end{aligned}$ | $\begin{aligned} & \mathrm{F} \\ & \mathrm{C} \end{aligned}$ | $\begin{aligned} & \hline 0.80 \\ & 0.79 \end{aligned}$ | $\begin{aligned} & 56.4 \\ & 32.9 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{C} \end{aligned}$ | Current lane use <br> Add 2nd EB LT and Th lanes; add 2nd WB Th lane |
|  | Alternative B <br> Alternative C <br> Alternative D | $\begin{aligned} & 0.49 \\ & 0.73 \\ & 0.73 \end{aligned}$ | $\begin{aligned} & 28.4 \\ & 32.5 \\ & 27.0 \end{aligned}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | $\begin{aligned} & 0.66 \\ & 0.83 \\ & 0.80 \end{aligned}$ | $\begin{aligned} & 38.3 \\ & 46.1 \\ & 35.2 \end{aligned}$ | $\begin{aligned} & \mathrm{D} \\ & \mathrm{D} \\ & \mathrm{D} \end{aligned}$ | Current lane use <br> Current lane use <br> Add 2nd EB LT lane; add 2nd WB RT lane |
|  | Alternative F | 0.61 | 32.6 | C | 0.72 | 42.7 | D | Current lane use |
| \#12 - Tsienneto Rd/Pinkerton St | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | $\begin{aligned} & 0.61 \\ & 0.69 \end{aligned}$ | $\begin{gathered} \hline \mathrm{n} / \mathrm{a} / \\ 13.7 \\ \mathrm{n} / \mathrm{a} / \\ \mathrm{n} / \mathrm{a} / \\ 20.1 \\ \mathrm{n} / \mathrm{a} / \end{gathered}$ | B | $\begin{aligned} & 0.65 \\ & 0.64 \end{aligned}$ | $\begin{gathered} \hline \mathrm{n} / \mathrm{a} / \\ 12.5 \\ \mathrm{n} / \mathrm{a} / \\ \mathrm{n} / \mathrm{a} / \\ 24.2 \\ \mathrm{n} / \mathrm{a} / \end{gathered}$ | B | Would remain unsignalized <br> Signalized and coord with Ross' Corner <br> Would remain unsignalized <br> Would remain unsignalized <br> Signalized and coord with Ross' Corner <br> Would remain unsignalized |
| \#13-NH 28/Linlew Dr | No-Build | 0.41 | 18.9 | B | 0.48 | 17.2 | B | Current lane use |
|  | Alternative A | $0.19$ | $11.7$ | B | 0.46 | $25.0$ | C | Current lane use |
|  | Alternative B | $0.36$ | $6.3$ | A | $0.49$ | $13.8$ | B | Current lane use |
|  | Alternative C | 0.39 | $5.2$ | A | 0.49 | $12.9$ | B | Current lane use |
|  | Alternative D | 0.56 | 14.9 | B | 0.78 | $20.4$ | C | Current lane use |
|  | Alternative F | 0.28 | 11.3 | B | 0.40 |  | B | Current lane use |
| \#14-NH 28/Ashleigh Dr <br> \#22-B/C Connector/NH 28 | No-Build | 0.43 | 17.3 | B | 0.59 | 24.8 | C | Current lane use |
|  | Alternative A |  | 17.0 | B | 0.48 | 21.7 | C | Current lane use |
|  | Alternative B | 0.73 | 26.8 | C | 0.83 | 35.6 | D | Revised Lane Use: EB- L,T,R; WB- <br> L,L,T,TR; NB-L,T,T,R,R; SB-L,T,T,R |


| Table 11 (Cont'd) <br> Summary of 2040 Capacity Analyses by Alternative <br> Signalized Intersections |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AM Peak Hour |  |  | PM Peak Hour |  |  | Comments/ <br> Lane Use Revisions |
| Intersection | 2040 Alternative | $\begin{gathered} \mathrm{v} / \mathrm{c} \\ \text { ratio } \end{gathered}$ | Average Delay | LOS | $\begin{aligned} & \mathrm{v} / \mathrm{c} \\ & \text { ratio } \end{aligned}$ | Average Delay | LOS |  |
| \#22-B/C Connector/NH 28 | Alternative C <br> Alternative D <br> Alternative F | $\begin{aligned} & \hline 0.71 \\ & 0.58 \\ & 0.38 \end{aligned}$ | $\begin{aligned} & \hline 22.0 \\ & 21.0 \\ & 16.9 \end{aligned}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{~B} \end{aligned}$ | $\begin{aligned} & \hline 0.84 \\ & 0.84 \\ & 0.55 \end{aligned}$ | 29.7 34.8 26.2 | C C C | Revised Lane Use: EB- L,L,T,TR; WBL,T,TR; NB-L,TR; SB-LT,R <br> Add WB RT lane to current lane use Current lane use |
| $\begin{aligned} & \text { \#18 - NH Byp 28/Tsienneto } \\ & \text { Rd } \end{aligned}$ | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | 0.69 0.64 0.54 0.58 0.56 0.74 | $\begin{aligned} & \hline 58.1 \\ & 33.6 \\ & 32.4 \\ & 23.9 \\ & 25.2 \\ & 32.4 \end{aligned}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | $\begin{aligned} & \hline 0.90 \\ & 0.80 \\ & 0.59 \\ & 0.79 \\ & 0.60 \\ & 0.87 \end{aligned}$ | $\begin{gathered} \hline 112.0 \\ 23.8 \\ 33.0 \\ 28.4 \\ 22.9 \\ 34.8 \end{gathered}$ | $\begin{aligned} & \hline \mathrm{F} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | Current lane use <br> Add 2nd EB/WB Th lanes <br> Current lane use <br> Current lane use <br> Add 2nd EB/WB Th lanes <br> Current lane use |
| $\begin{aligned} & \text { \#19 - NH 102/Tsienneto Rd, } \\ & \text { coord w/ } \\ & \text { \#26 - NH 102/North Shore } \\ & \text { Rd } \end{aligned}$ | $\begin{gathered} \text { No-Build * } \\ \text { Alternative A } \\ \text { Alternative B } \\ \text { Alternative C } \\ \text { Alternative D } \\ \text { Alternative F* } \end{gathered}$ | 0.53 0.62 0.60 0.60 0.63 0.30 | $\begin{aligned} & 24.9 \\ & 13.2 \\ & 11.0 \\ & 12.7 \\ & 12.1 \\ & 24.3 \end{aligned}$ | $\begin{aligned} & \mathrm{C} \\ & \text { B } \\ & \text { B } \\ & \text { B } \\ & \text { B } \\ & \text { C } \end{aligned}$ | $\begin{aligned} & 1.53 \\ & 0.76 \\ & 0.61 \\ & 0.60 \\ & 0.65 \\ & 1.46 \end{aligned}$ | $\begin{gathered} 247.7 \\ 19.6 \\ 9.9 \\ 9.0 \\ 6.9 \\ 247.5 \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ \mathrm{D} \\ \mathrm{~A} \\ \mathrm{~A} \\ \mathrm{~A} \\ \mathrm{~F} \end{gathered}$ | LOS as unsignalized <br> Add EB LT, WB RT lanes at signal Add EB LT, WB RT lanes at signal Add EB LT, WB RT lanes at signal Add EB LT, WB RT lanes at signal LOS as unsignalized |
| \#20 - Exit 4A SB off ramp/Connector Rd | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | $\begin{aligned} & 0.97 \\ & 1.04 \\ & 0.73 \\ & 0.70 \end{aligned}$ | $\begin{gathered} \hline \mathrm{n} / \mathrm{a} / \\ 41.2 \\ 52.3 \\ 20.1 \\ 19.2 \\ \mathrm{n} / \mathrm{a} / \end{gathered}$ | D D C B | $\begin{aligned} & 0.88 \\ & 0.94 \\ & 0.65 \\ & 0.63 \end{aligned}$ | $\begin{gathered} \hline \mathrm{n} / \mathrm{a} / \\ 28.9 \\ 34.6 \\ 18.3 \\ 18.2 \\ \mathrm{n} / \mathrm{a} / \end{gathered}$ | C C B B | Does not exist <br> 2 SB LT lanes from off-ramp, 2 WB LT lanes to on-ramp <br> 2 SB LT lanes from off-ramp, 2 WB LT lanes to on-ramp <br> 2 SB LT lanes from off-ramp, 2 WB LT lanes to on-ramp <br> 2 SB LT lanes from off-ramp, 2 WB LT lanes to on-ramp <br> Does not exist |
| \#21-Exit 4A NB off ramp/Connector Rd | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | $\begin{aligned} & 0.93 \\ & 0.97 \\ & 0.65 \\ & 0.59 \end{aligned}$ | $\begin{gathered} \hline \mathrm{n} / \mathrm{a} / \\ 20.4 \\ 27.5 \\ 7.9 \\ 5.7 \\ \mathrm{n} / \mathrm{a} / \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{~A} \\ & \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 0.84 \\ & 0.88 \\ & 0.58 \\ & 0.53 \end{aligned}$ | $\mathrm{n} / \mathrm{a} /$ 16.1 15.8 7.1 5.1 $\mathrm{n} / \mathrm{a} /$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~B} \\ & \mathrm{~A} \\ & \mathrm{~A} \end{aligned}$ | Does not exist <br> EB - T,T; WB T,T,R,R; NB- LR,R <br> EB - T,T; WB T,T,R,R; NB- LR,R <br> EB - T,T; WB T,T,R,R; NB- LR,R <br> EB - T,T; WB T,T,R,R; NB- LR,R <br> Does not exist |
| \#23-B/C Connector Road/NH Bypass 28 | No-Build Alternative A Alternative B Alternative C Alternative D Alternative F | $\begin{aligned} & 0.25 \\ & 0.37 \end{aligned}$ | $\begin{aligned} & \hline \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & 17.0 \\ & 18.5 \\ & \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \end{aligned}$ | B | 0.32 0.46 | $\begin{aligned} & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \\ & 16.9 \\ & 20.4 \\ & \mathrm{n} / \mathrm{a} / \\ & \mathrm{n} / \mathrm{a} / \end{aligned}$ | B | Does not exist <br> Does not exist <br> Prop lane use: EB- L,T,TR; WB- L,T,TR; NB- <br> L,TR; SB-L,T,R <br> Prop lane use: EB- L,TR; WB- L,TR; NB- <br> L,TR; SB-L,T,R <br> Does not exist <br> Does not exist |


| Intersection | Table 11 (Cont'd) <br> Summary of 2040 Capacity Analyses by Alternative <br> Signalized Intersections |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2040 Alternative | AM Peak Hour |  |  | PM Peak Hour |  |  | Comments/ <br> Lane Use Revisions |
|  |  | v/c <br> ratio | Average Delay | LOS | v/c <br> ratio | Average Delay | LOS |  |
| \#25-C/D Connector | No-Build |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ |  | Does not exist |
| Road/NH 28 | Alternative A |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ |  | Does not exist |
|  | Alternative B |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ |  | Does not exist |
|  | Alternative C | 0.81 | 10.6 | B | 0.79 | 12.2 | B | Prop lane use: EB- L,T,T; WB- T TR, SB- L,R |
|  | Alternative D | 0.96 | 13.7 | B | 0.87 | 14.1 | B | Prop lane use: EB- L,T,T; WB- T TR, SB- L,R |
|  | Alternative F |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ |  | Does not exist |

## \#1 - Exit 4 SB off-ramp at NH Route 102

The results show that this ramp terminal as presently proposed will still experience capacity constraints into the 2040 design horizon. All 4A Build interchange alternatives appear to function better than No-Build, with Alternatives A and B doing better than the northerly or no interchange alternatives, even though they both have a higher potential development scenario for Woodmont Commons than the others. The heavy SB right turn onto NH Route 102 from the ramp, even with two lanes, combined with heavy WB flow from the NB ramps located to the east, contribute to the decline in LOS. The single left turn lane from the off-ramp also appears insufficient to handle the peak hour demands.

## \#2 - Exit 4 NB ramps at NH Route 102

The results show that this ramp terminal as presently proposed will also experience capacity constraints into the 2040 design horizon. All 4A Build interchange alternatives improve 2040 AM peak hour operations, with Alternatives C and D doing slightly better than Alternatives A and B in the PM peak. The heavy EB left-turn onto the on-ramp, even with two lanes, is the dominant volume at this location, as well as the NB left turn from the off-ramp. Alternatives C and D appear to operate at a slightly better LOS, but the Woodmont Commons development scenario is also less intense in these cases than under Alternatives A and B. Alternative F fares worse than any of the alternatives as proposed.

## \#3 - Exit 5 SB ramps at NH Route 28

The results show that this ramp terminal as presently proposed will still experience some capacity constraints into the 2040 design horizon. All 4A Build interchange alternatives provide better operations than the No-Build condition. The single WB left turn and SB right-turn lanes appear to be the constraints to better operations across all alternatives. Alternatives C and D appear to function better than No-Build or the southerly or no interchange alternatives, likely because of their proximity to this interchange and the increased likelihood of diverting some of the traffic demand, as opposed to the other alternatives.

## \#4 - Exit 5 NB ramps at NH Route 28

The results show that this ramp terminal as presently proposed will also experience capacity constraints into the 2040 design horizon. All 4A Build interchange alternatives provide slightly better operations than under No-Build conditions. The heavy EB left-turn demand onto the on-ramp in a single lane, as well as the single-lane NB left turn from the off-ramp, are the critical movements at this intersection. Alternatives C and D appear to operate at a slightly better LOS than Alternatives A and B, again because of their proximity to this interchange and increased likelihood of diverting some of the traffic demand. Alternative F fares worse than any of the alternatives as proposed.

## \#5 - NH Route 102/Londonderry Road/St. Charles Street

With the addition of a second east-west through lane on NH Route 102 as part of the proposed Woodmont Commons improvements, this intersection would operate at acceptable LOS under all alternatives. Alternative F would operate slightly worse than the other alternatives, because of projected increased traffic on NH Route 102, but would still be at an acceptable LOS.

## \#6 - NH Route 102/Fordway/ Madden Hill Road

This existing intersection would operate at acceptable LOS under all alternatives except Alternative F. Alternative A appears to draw more traffic to the Madden Hill Road approach that opposes the heavy Fordway volumes on the same permissive phase (where both approaches have a concurrent green light and must wait for gaps in opposing traffic to proceed), so it operates slightly worse than the other interchange alternatives, particularly in the 2040 PM peak. Alternative F would necessitate provision of lane separation out of Fordway as well as an exclusive EB right-turn lane to maintain an acceptable LOS.

## \#7 - NH Routes 102/28

Based solely on the capacity calculations, this existing intersection would operate at acceptable LOS under all alternatives except Alternative F. As noted earlier, there are many other unquantifiable factors in the downtown area, such as pedestrian activity and friction from side street and on-street parking maneuvers, that contribute to reduced traffic speeds and the general diversion/avoidance of the area by through traffic to other routes such as Ash Street Extension, North High Street, Folsom Road, and Tsienneto Road.

The traffic model indicates that Alternative A appears to draw more traffic to the eastern part of downtown that then makes a right turn to NH Route 28 in the direction of Exit 4A and the Woodmont Commons development. In reality, much of this traffic may divert to the traffic circle to the east and use the Pinkerton/Tsienneto corridor to complete such a trip. Other Build alternatives show similar operational/LOS characteristics than under No-Build conditions. With additional traffic through the downtown area and no interchange option, Alternative F would necessitate provision of a second NB left-turn lane, an EB exclusive right-turn lane, and a second WB thru lane to maintain an acceptable LOS in the 2040 design horizon.

## \#9A - Alternative A Connector Road/North High Street

This new intersection is created by the Alternative A connector road with the local street network. The existing intersection of North High Street with Madden Road would be relocated off the new connector road as a minor roadway serving the small number of residences there. It is envisioned that this new intersection would need to be signalized and widened to provide acceptable operations, given the projected traffic volumes. The Connector Road eastbound approach would consist of two thru lanes and an exclusive right-turn lane to North High Street. The Connector Road westbound approach would consist of an exclusive left-turn lane and two thru lanes. The North High Street northbound approach would
consist of two left-turn lanes and a right-turn lane. Given the projected volumes and this lane use, this intersection would operate at a LOS D in the 2040 PM peak hour.
\#10 - Alternative A Connector Road/Franklin Street/Franklin Street Extension This existing intersection is presently unsignalized and operates at a poor LOS for the north/south side street approaches, which experience difficulty entering the main traffic flow during peak periods. With the increase in development activity nearby, this condition would be exacerbated into the future to the point where there may need to be consideration of additional improvements to provide acceptable operations, even with other interchange alternatives beyond Alternative A.

With the Alternative A connector road in place, this intersection will require significant widening and signalization to provide sufficient lanes to handle the project volumes as a direct result of Exit 4A. The east/west approaches would have at least two thru lanes (the projections suggest a third lane may be needed for the eastbound approach) with exclusive left-turn lanes. The north/south approaches would have two lanes with an exclusive lane oriented to the west to handle the projected traffic. This configuration would operate at a LOS C in the 2040 PM peak hour.

## \#11 - Ross' Corner (NH Route 28/Folsom Road/Tsienneto Road)

This intersection was upgraded several years ago to provide a second southbound left-turn lane from NH Route 28 onto Tsienneto Road to serve the predominant southbound-to-eastbound travel demand between I-93 and Derry and points to the east. With the projected growth to 2040, the existing lane geometry will no longer be sufficient to meet the expected traffic demands.

With an Exit 4A interchange in place, and with the Alternative A connector road in particular, the existing north-south traffic orientation now becomes an eastwest flow. As such, improvements to handle the increase east-west travel demand will be required. With Alternative A, a second EB left-turn lane and second EB thru lane will be needed, as well as a second WB thru lane, to provide an acceptable LOS. Alternatives B and C are on a new east-west alignment north of this intersection so no changes to the existing lane use are required. With Alternative D, the interchange is north of this intersection, so movements oriented in that direction will need to be augmented. This means the addition of a second EB left-turn lane and second WB right-turn lane at this location. Alternative F maintains the existing traffic distribution, and the existing lane use can accommodate the projected traffic volumes.

## \#12 - Tsienneto Road/Pinkerton Street (Alternatives A and D only)

This intersection is in close proximity ( 300 feet $+/-$ ) from the Ross' Corner signal, but is not currently signalized. As such, left-turn exits experience lengthy delays while waiting for a gap in the Tsienneto Road traffic flow. The eastbound right-
turn movement has been separated from the main traffic stream by a channelizing island to help exiting traffic, but the opposing traffic flow limits the number of available gaps for exiting traffic. At some point in the future, regardless of this project, this intersection may need to be signalized and coordinated with the Ross' Corner signal, but there are no defined plans to do that at this time. Therefore, except for those alternatives that directly impact this intersection, namely Alternatives A and D, the intersection is assumed to remain unsignalized and is expected to operate at a poor LOS for the minor street approach from Pinkerton Street.

For Alternatives A and D, a second lane for thru traffic would be provided in both the eastbound and westbound directions, as well as an exclusive westbound leftturn lane into Pinkerton Street. With this geometry and coordinated phasing with Ross' Corner as a cluster intersection, this location would operate at an acceptable LOS C or better in the 2040 design year.

## \#13 - NH Route 28/Linlew Drive

No changes to the existing lane use at this intersection are required to accommodate traffic volumes under any of the proposed alternatives.

## \#14/22 - NH Route 28/Ashleigh Drive/Alternative B-C Connector Road

This intersection would see significant changes depending on which alternative would be in place. For Alternatives B and C, the proposed connector road would create a new east-west roadway that would require reconfiguration of lanes to accommodate the new distribution of traffic for either a southerly or northerly interchange. Under Alternative B, the new roadway would need two thru lanes in the east-west direction, as well as double-turn lanes to and from NH Route 28 to the south, along with other lane use changes. With Alternative C, a double SB left-turn lane into Ashleigh Drive would be needed to serve traffic from the new interchange to the north and the connector road, among other lane use changes. An acceptable LOS C or better can be provided for all alternatives with the appropriate revisions to the lane use.

## \#18 - NH Route 28 Bypass/Tsienneto Road

The 2040 No-Build analysis shows that the existing intersection would operate at or over capacity during both peak hours, so some improvements would appear to be needed at some point in the future. Alternatives B and C reduce east-west traffic through this intersection, so the existing lane use can provide an acceptable LOS D or better in 2040. Alternatives A and D will require the addition of a second east-west thru lane to accommodate the increased east-west traffic at an acceptable LOS.
\#19/26- NH Route 102/Tsienneto Road/North Shore Road (Alternatives A-D) A review of the existing traffic counts at the North Shore Road and English Range Road intersections indicate that existing 2015 left-turn volumes currently satisfy turn-lane warrants at both locations. As such, any improvements at the Tsienneto

Road/NH Route 102 intersection associated with any of the alternatives should take this into consideration in the design.

Because existing PM peak analyses already indicate a poor LOS for exiting traffic, combined with the projected increase in left-turn volumes exiting Tsienneto Road, it has been assumed that this location will need to be signalized as part of any interchange alternative. Because of the proximity of North Shore Road, that intersection would be incorporated into the signalized intersection, similar to Ross' Corner and Pinkerton Street. An exclusive right-turn lane would be provided for NH Route 102 WB traffic entering Tsienneto Road, as well as a WB left-turn lane into North Shore Road. This left-turn lane would also be carried easterly towards the English Range Road intersection for continuity, where an EB left turn lane would be provided. There would still only be a single lane exiting Tsienneto Road, despite the higher volumes, because of the complexity of accommodating a double left-turn lane onto NH Route 102 and then tapering back to a single lane with North Shore Road being so close.

With signalization of the intersection as proposed, an acceptable LOS C or better can be provided for all interchange alternatives in the 2040 design horizon.

## \#20/21 - Exit 4A SB and NB Ramp Terminals (Alternatives A-D)

With either a northerly or southerly interchange, it is envisioned that both ramp terminals would be signalized as part of the diamond configuration. The SB offramp would have two lanes exiting the ramp, while there would be two lanes provided for the left turn onto the SB on-ramp. This ramp would be close to capacity in the 2040 AM peak hour, assuming full realization of the traffic projections on the SB off-ramp.

At the NB ramps, there would be two east-west thru lanes with a single EB leftturn lane and double WB right-turn lanes onto the NB on-ramp. On the off-ramp, there would be a shared left/right lane and an exclusive right-turn lane, since there is no access to the west. An acceptable LOS D or better can be provided at this ramp terminal under all interchange alternatives.

## \#23 - NH Route 28 Bypass/B-C Connector Road (Alternatives B and C)

This new intersection is created by the connector road roughly along the alignment of the existing Ashleigh Drive. With Alternative B, two east-west thru lanes need to be provided so that an acceptable LOS C can be achieved. Only one east-west thru lane is required with Alternative C because of less overall traffic volume through the intersection.

## \#25-C-D Connector Road/NH Route 28 (Alternatives C-D)

This new intersection is created by the connector road from the northerly interchange where it would intersect with the existing two-lane section of NH Route 28 just north of the Derry/Londonderry town line. NH Route 28 southbound would become the minor approach to the intersection and would have
separate left- and right-turn lanes. The EB approach would have an exclusive left lane and two thru lanes, while the WB approach would have a thru lane and a shared thru/right lane. This configuration would provide a LOS B during the 2040 peak hours.

## 16. Unsignalized Intersections

A summary table showing a comparison of operations at each existing or proposed unsignalized intersection is provided in Table 12. In most cases, the existing or projected deficiencies for the minor street approaches are exacerbated, except where traffic diversions may reduce the volume of traffic on the major approach that would conflict with traffic turning from the minor street approach(es).

It is not envisioned that any of these intersections would warrant signals, except those that are directly impacted by a specific alternative, such as Tsienneto Road/Pinkerton Street or NH Route 102/Tsienneto Road/North Shore Road. Delays at the North High Street /Ash Street Extension and the North High Street/Folsom Road/Franklin Streets locations are excessive and should be monitored as the Woodmont Commons development progresses to determine if and when signal warrants may be satisfied.

| Table 12 <br> Summary of 2040 Capacity Analyses by Alternative <br> Unsignalized Intersections |  |  |  |  |  |  |  | Comments/ <br> Lane Use Revisions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection |  | AM Peak Hour |  |  | PM Peak Hour |  |  |  |
|  | $2040$ <br> Alternative | v/c ratio | Average Delay | LOS | v/c ratio | Average Delay | LOS |  |
| $\begin{aligned} & \hline \text { \#8 - N High St/Ash St Ext } \\ & \text { (Critical Movement - EB LT) } \end{aligned}$ | No-Build | 1.04 | 78.0 | F | 3.04 | >300 | F |  |
|  | Alternative A | 0.53 | 17.4 | C | 1.47 | 228.8 | F |  |
|  | Alternative B | 0.42 | 14.3 | B | 0.96 | 56.5 | F |  |
|  | Alternative C | 0.76 | 29.3 | D | 1.09 | 90.6 | F |  |
|  | Alternative D | 0.74 | 25.7 | D | 1.70 | >300 | F |  |
|  | Alternative F | 0.74 | 27.1 | D | 1.79 | >300 | F |  |
| \#10-N High/Folsom/Franklin Sts. (Critical Movement varies between NB and SB) | No-Build | 0.20 | 21.8 | C | 0.55 | 82.0 | F | NB all is critical |
|  | Alternative A |  | n /a/ |  |  | $\mathrm{n} / \mathrm{a} /$ |  | Signalized |
|  | Alternative B | 0.94 | 96.5 | F | 3.00+ | >300* | F | NB all is critical |
|  | Alternative C | 1.35 | 219.6 | F | 3.31 | >300* | F | SB all is critical |
|  | Alternative D | 0.22 | 10.9 | B | 1.21 | 160.2 | F |  |
|  | Alternative F | 0.36 | 31.7 | D | 2.31 | >300 | F | NB critical in AM, SB critical in PM |
| \#12 -Tsienneto Rd/Pinkerton St (Critical Movement - NW LT) | No-Build <br> Alternative A | 0.25 | $\begin{aligned} & 16.1 \\ & \mathrm{n} / \mathrm{a} / \end{aligned}$ | C |  | $\begin{gathered} 84.0 \\ \mathrm{n} / \mathrm{a} / \end{gathered}$ | F | Signalized |
|  | Alternative B | 0.89 | 80.0 | F | 1.00 | 126.4 | F |  |
|  | Alternative C | 2.04 | >300* | F | 2.54 | >300* | F |  |
|  | Alternative D |  | n/a/ |  |  | n/a/ |  | Signalized |
|  | Alternative F | 0.65 | 66.1 | F | 4.10 | >300 | F |  |
| \#15-NH 28/Scobie Pond Rd (Critical Movement - SB all) | No-Build | 1.01 | 144.7 | F | 0.58 | 32.2 | D |  |
|  | Alternative A | 0.18 | 14.4 | B | 0.19 | 16.4 | C |  |
|  | Alternative B | 0.18 | 13.3 | B | 0.23 | 16.5 | C |  |
|  | Alternative C | 0.67 | >300* | F | 4.44 | >300* | F |  |
|  | Alternative D | 1.34 | >300* | F | 6.67 | 4259.8* | F |  |
|  | Alternative F | 0.31 | 27.4 | D | 0.47 | 51.0 | F |  |
| \#16 - NH 102/NH Byp 28/E Derry Rd <br> (Traffic Circle-RT only) <br> (HCM 2010) <br> (Critical Movement - E Derry Rd) | No-Build | 0.87 | 31.9 | D | 1.26 | 151.2 | F |  |
|  | Alternative A | 1.11 | 94.0 | F | 0.92 | 41.9 | E |  |
|  | Alternative B | 0.77 | 21.4 | C | 0.68 | 16.4 | C |  |
|  | Alternative C | 0.73 | 18.8 | C | 0.78 | 21.7 | C |  |
|  | Alternative D | 0.84 | 28.3 | D | 0.89 | 33.6 | D |  |
|  | Alternative F | 0.91 | 40.1 | E | 1.21 | 128.7 | F |  |
| \#17-NH Byp 28/Pinkerton/Nesmith <br> (HCM 2010) <br> (Critical Movement - WB all) | No-Build | - | \% | F | . | - | F | Left turns from Nesmith |
|  | Alternative A | 1.01 | 138.9 | F | 0.52 | 55.3 | F |  |
|  | Alternative B | 1.13 | 188.1 | F | 0.53 | 57.3 | F |  |
|  | Alternative C | 0.96 | 127.6 | F | 0.41 | 41.7 | E |  |
|  | Alternative D | 1.35 | 280.7 | F | 0.63 | 78.3 | F |  |
|  | Alternative F | 0.45 | 26.2 | D | 0.46 | 49.1 | E |  |
| \#24-B/C Connector Rd/Tsienneto Road (Critical Movement - NB LT) | No-Build |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ | - | Does not exist |
|  | Alternative A |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ | - | Does not exist |
|  | Alternative B | 0.09 | 38.9 | E | 0.00 | 0.0 | A |  |
|  | Alternative C | 0.00 | 0.0 | A | 0.00 | 0.0 | A |  |
|  | Alternative D |  | $\mathrm{n} / \mathrm{a} /$ |  |  | $\mathrm{n} / \mathrm{a} /$ | - | Does not exist |
|  | Alternative F |  |  |  |  |  |  | Does not exist |


| Table 12 (Cont'd) <br> Summary of 2040 Capacity Analyses by Alternative <br> Unsignalized Intersections |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | 2040 Alternative | AM Peak Hour |  |  | PM Peak Hour |  |  | Comments/ Lane Use Revisions |
|  |  | v/c ratio | Average Delay | LOS | v/c ratio | Average Delay | LOS |  |
| \#27-NH 102/English Range Road (Critical Movement - SEB all) | No-Build |  | n/a/ |  |  | n/a/ | - |  |
|  | Alternative A | 0.17 | 20.8 | C | 0.16 | 28.4 | D |  |
|  | Alternative B | 0.23 | 24.5 | C | 0.22 | 26.1 | D |  |
|  | Alternative C | 0.17 | 20.8 | C | 0.23 | 42.1 | E |  |
|  | Alternative D | 0.17 | 21.0 | C | 0.18 | 32.8 | D |  |
|  | Alternative F | 0.17 | 20.8 | C | 0.16 | 28.4 | D |  |

## 17. Findings and Conclusions

The results of the traffic modeling for the Project indicates that the provision of a new interchange on I-93 will provide varying levels of traffic relief to NH Route 102 east of Exit 4 and into the downtown Derry area by the 2040 design year, as shown in Table 7.

Examples on key links include:

- NH Route 102 east of Exit 4: In the 2040 No-Build case, there is projected to be $41,725 \mathrm{vpd}$ on this segment. Alternative A provides the most relief on this segment ( $-51.5 \%$ ) to a volume of 20,240 vpd, which is the same magnitude as the 2015 base volume. Alternative B shows a $48 \%$ reduction, while Alternatives C and D show lesser reductions. Alternative F shows a slight increase in projected traffic than any interchange alternative.
- NH Route 102 east of Griffin Street (downtown): Alternatives A, B and C show similar reductions, on the order of $19-21 \%$, or $3000-4000$ vpd, over 2040 NoBuild conditions. Alternative D shows a lesser reduction, but still lower volume than the 2015 base. Alternative F projects higher volumes than any interchange alternative and would be higher than either the 2015 or 2040 No-Build case.
- Volumes on the Exit 4 ramps are lower under most interchange alternatives, with Alternative A providing the most overall relief over No-Build conditions, even under the highest potential development scenario for the Woodmont Commons development.
- Volumes on the Exit 5 ramps see the highest traffic reductions under Alternatives C and D (northerly interchange) than under a southerly interchange scenario.

Mainline freeway facilities operational analyses indicates that the four-lane I-93 mainline will function at an acceptable LOS C or better under all scenarios, with a couple of exceptions where two-lane on- or off-ramps may be needed to accommodate all projected volumes. A sensitivity analyses of the Exit 4A SB off-ramp indicated that a 200 -vph reduction in the assigned traffic would allow this ramp to function as a single lane offramp if these traffic projections are not fully realized.

The Exit 4 ramps would have slightly higher volumes under either Alternatives A or B, but this is more reflective of the higher potential development scenario assumed for the Woodmont Commons development than for Alternatives C, D or F, which use the same scenario as the No-Build condition. As noted earlier, should the $23 \%$ internal capture rate for Woodmont Commons trips be realized in some form, the number of trips assigned to the study area network may be reduced accordingly, which should result in better traffic operations than the worse-case scenario assumed in this study.

The level of intersection improvements needed to accommodate the alternative and connector road corridors vary greatly depending on alternative. In general, all intersections can provide an acceptable LOS under any alternative with appropriate lane use and signalization/coordination as required. The traffic circle at NH Route 102/NH Route 28 Bypass will continue to function at a poor LOS regardless of alternative.

In summary, from a purely traffic standpoint, Alternatives A appears to best satisfy the Purpose and Need for the Project by providing the greatest reductions in NH Route 102 traffic through downtown Derry than the other alternatives evaluated. Volumes on NH Route 102 just east of Exit 4 would be roughly half of 2040 No-Build levels and similar to existing (2015) conditions. Alternative B provides some relief as well, but primarily serves a north-south trip pattern as opposed to the east-west pattern needed to reduce traffic on NH 102 in downtown Derry. Alternatives C and D would provide some, but not as much, relief to the NH Route 102 corridor, because of the increased distance between these northerly interchange alternatives and the NH Route 102 corridor.

Other natural and cultural resource impact criteria will be used to provide the final assessment of the Preferred Alternative, but the previous finding of Alternative A as the Preferred Alternative from a traffic standpoint is supported by the updated analyses contained herein.

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Figure 3 - I-93 Exit 4A Supplemental Draft EIS - Zones 1-6 Locus Map


Figure 4-2015 No-Build AM Peak Hour Base Volumes - Locations 1-4


Figure 5-2015 No-Build PM Peak Hour Base Volumes - Locations 1-4



FIGURE 8 - VOLUME COMPARISONS - EXIT 4 RAMPS





FIGURE 9 - VOLUME COMPARISONS - EXIT 5 RAMPS





FIGURE 10- VOLUME COMPARISONS - EXIT 4A RAMPS


Exit 4A SB Off-Ramp


Exit 4A NB On-Ramp


Exit 4A SB-On-Ramp


FIGURE 11 - VOLUME COMPARISONS - NH ROUTE 102 CORRIDOR





FIGURE 12- VOLUME COMPARISONS- OTHER LOCAL STREETS



Tsienneto Rd, West of NH 102






Figure 15-2040 No-Build AM Peak Hour Base Volumes - Locations 1-4




Figure 18-2040 Alternative A PM Peak Hour Base Volumes - Locations 1-4 and 20-21








Figure 25-2040 Alternative F AM Peak Hour Base Volumes - Locations 1-4


Figure 26-2040 Alternative F PM Peak Hour Base Volumes - Locations 1-4






Figure 31-2040 Alternative B AM Peak Hour Base Volumes - Locations 5-19, 22-24, and 26-27


Figure 32-2040 Alternative B PM Peak Hour Base Volumes - Locations 5-19, 22-24, and 26-27



Figure 34-2040 Alternative C PM Peak Hour Base Volumes - Locations 5-19 and 22-27




Figure 37-2040 Alternative F AM Peak Hour Base Volumes - Locations 5-19 and 26-27


Figure 38-2040 Alternative F PM Peak Hour Base Volumes - Locations 5-19 and 26-27

## APPENDIX A: TRAFFIC COUNT DATA

## NHDOT PERMANENT RECORDER COUNTS－ 1935 OF EXIT 4 －MAY 2016

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| 5723 | ${ }_{6}$ | A | rm | 15 | ，${ }^{1}$ | 24 | 120］ | －1 | M | 昭 | ts | $18 \pm$ | xu1 | chit | raid | 2 | 20． | 3120 | 1 | $1 \times$ | ， | sed | yed | 12 | Bx |
| 53 | 3， | C | 圽 | 16 | 4 | 31 | 14 | $\cdots$ | \％sis | 1 H | 102 | 4 | 1920 | m | 2459 | $\cdots$ | 2180 | 3s | 11919 | N | win | 11.2 | 功 2 | S 4 | ： |
| $\pm 15$ | 3 | 2 | 3 | 12 | nos | 201 | IT＝ | 182． | 13＞1 | 128 | 1532 | 204 | 去城 | 24 | 2919 | 132 | \％ | 楽 | ： 21 | 去： | Lesi | 14 | \％ | st | $\cdots$ |
| ${ }^{3}$ 5 5 | 43： | A99 | 1 |  | $\pi$ | 2 | ＇6 | 2010 | 1980 | 1 | 1.202 | \％ | 02 | Ts | nes | 1 mP | 301 | H\％ | ＋ | Y 4 | 139 | 2 tug | 14 | tsit | stis |
| \％ 138 |  |  |  |  |  | \％ 4 |  | N20 | nse | $16+1$ | 139 | CESE， | 2 | en | 3\％ | 42 | 193 | 坔， | 50 c | cist | 125 | 120 | 12. | $0 \times$ | ceses |
| 5 It |  | N2 | Lex |  | 成 | 3 ${ }^{2}$ | Ex2 | Msi | 0 | ？ | ＋$\times$ \％ | （the |  | 3th | 3 | 3rn | 2019 | 3ter | 暒 | pise |  | 1\％n | T／is | 4 | R15\％ |
|  |  |  |  |  | \％ |  | 20， | Sx | N | Sel | 12． | 2 LE | 2teri | ${ }^{2} \times$ | smil | 3elt | 231 | 2xec | 잔 | Rep． | 12910 | 1 | 18 遂 | sel | 11930 |



| mis or ${ }^{\text {a }}$ | Hi | $\mathrm{Hz}^{2}$ | H | H2 | 든 | 緼 | 41） | 78 AM | H ${ }^{\text {S }}$ | \＄19 | 34： | H22 | His | H12 | bis | ＋136 | mi | 5.5 Pm | 1：9 | $\mathrm{H}_{2} \mathrm{~s}$ | H21 | H2］ | H73 | H24 | sxtodi |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 F | $\pm 1$ | 3 s | 1 m | 1.1 | － | \％ 7 | 515 | 家 | Hext | 13 | 500 | 4 | N：S | 5 | 129 | ast | nim | As／ | 2， | 10， | 3n9 | 篤 | w | 20．4 | － |
| $\leq 121$ | 37 | 213 | 12 | S | $1{ }^{\text {a }}$ | sm | 201 | $\mathrm{H}^{2}$ | 隹角 |  | Hes． | 3 m | 10 | r3＞ | cta | 2Feco | 208 | \％ | 安速 | ver | Ste | 03 | $\pm$ | 4 | Rater |
| － 19 | 4 | ne： | 4 | 1 18， | 边 | S | 3 | E15 | 125 | 1 12 | 21m | ［19 | mid | sor | \％ | \％ | Anc | N40 | $20 \%$ | 38. | 5 5 | $4{ }^{4}$ | $\cdots$ | ， | W， |
| $\leq 21$ | n | s | $1 \times 1$ | 採 | 14 | 2 l | $\leq 15$ | 0 | و15 | 1848 | mi | S | $4 \times 1$ | N：－ | 区䢕 | 219 | \％ 46 | fist | 10x | 0 | 㫛 | \＃13 | 591 | L11 | 3， |
| $5 \geqslant$ | 18 | 23 | 1 | 11 | H1 | 组 | $\pm$ | ra | 318） | 200： | 115 | 21 | $3{ }^{3}$ |  | n－ | Siv | z：37 | 23i | 㫛 | \％ | S22 | Et | 妆 | 5 | 3 |
| $5{ }_{5}{ }^{5}$ ， | 战 | S | 12 | 1 F | 2 | Dis | 9 | $1 \%$ | 1ee | ［stelf | N | 家 | 4 A | 2m． | 2xt | 23 | 20x | \％ | 12 m | Sme | ＋19 | S14 | 23 | 2 | 29. |
| \％\％， | xins | $\underline{4}$ | n | $1 \times$ | 3 | $\operatorname{tes}^{1}$ | 4，3 | 12 | 1bes． | \％ | 211 | 143 | 212 | 2 SO | 分耍 | m | 为 | \＄409 | 170 | ， | 58 | 133 | 5 S ！ | $\pm$ | 5 |
| 5 18， | ， 1 | ， | 些 | 1 | 会 | sed | \％ | 18 | 13 | Sss | 7\％ | क 4 12 |  | \％ | 32］ |  | 2：1 | 2 m | $3 \times 1$ | ［4］ | 129 | 12 t | m | 2 | \％ |
| 5 2， | 2 | －0， | \％ | 1 | 4 | 4 | E | ： | \％ | 3 y ： | 201 | yect | （1） | \％ | 104 | 1 TH | 2 | 20＊ | 5 Ec | 4 | 3 | $1290{ }^{1}$ | get | 22 | $1!9$ |
| $\leq$ \％ | 3 t | \％ | \％${ }^{\text {che }}$ | H | $\because$ | \％ | 5 | $2 \times$ | 1 2 | 139 | \％ | ＋12 | 1131 | 心1 | 4 | 3 y | 2020 | 4 ta | ：$* \times 1$ | － $4 \times 1$ | 1 H | S | tit | $0 \cdot 1$ | 1 ssex |
| 5 bis | rss | 吹 | sisf | S | 1 m | 321 | 38. | 1 | ： | 3 S | 11nt | \％ | 1813 | Erra | ar | ， | \％ | 3\％ | 231 | 4 | ｜im | 1H： | E2： | $\underline{5}$ | may mine |
| 547 | 134 | 11 | 1） | $\ldots$ | x | 245 | 100 | 3x1 | נ | ［4］ | $1 \times 2$ | 13 l | 12， | W | Pay | 盛 | 1090 | A | Sas | 5 | 3：2 | mid | 29 | ICS | 1208 |
| 538 | 12 | 115 | 2 2 | A | ts： | 去 5 ¢ | $\cdots$ 碞 | 12xt | गtig | ser | $19 \%$ | 120 | 12 | 18.1 | \％rei | m | 15920 | 3431 | 5 | － | 53 | 2，$=1$ | 311 | 2 | Lind |
| $5{ }_{5}{ }_{5}{ }^{5}$ | ， $\mathrm{H}_{2}$ | 13 | 1 | x | \＃ | $2 \times 1$ | 31. | यuia | 1111 | 2 m | 15＊ | ［2］${ }^{\text {a }}$ | 14 | 14 | Wh | 14 | \％ | यer | 320 | 152 | 时 | 19 | 3 － | $1{ }^{18}$ | 30es |
| $5: 3$ | St | ${ }_{163}$ | \％ | 20，f | \％ | w | 3：31 | sas | 3 Jg 9 | 25 | 3 mm | 178） | Lsi | 17 col | 48 | \％ 1 | \％ 4 | 4 | $\mathrm{rax}^{3}$ | 14 | \＄ | 0 | 4 | 2\％ | were |
| 53 | 5 | 1 | \％ | 4 | \％ | 26s | 148 | 160： | 3198 | im | H1 | 12 a | 19 | 164 | 120， | \％ | 2tes | 121 | 2 1 | 1001 | 217 | W | 6 3 | smi | Hese |
| 5 5 | ， 6 | 12 | 域 | 12 | ${ }^{4}$ | $1{ }^{21}$ | $3 \geqslant 3$ | 19 | 18989 | 141 | $\pm$ | 1 | 137 | ref | 13，${ }^{\text {a }}$ ， | － | M1si | 䢒 | 1251 | 19 | EEL | ［2］ | 3 | 3 | 15 |
| 5 |  |  |  |  | $\pm$ | $6{ }^{6}$ | 22， | Prs | 12 | 4x | 1s00 | $x \leq 1$ | 18 － | 129 | 2129 | $0 \rightarrow 1$ | 1 l | $4{ }^{4}$ | $1 / 40$ | 140 | 54 | \％ | 2 m | 3 | jer |
| $5{ }_{5}^{5}$ | ${ }^{\text {Hex }}$ | 19 | 1 | m | ${ }^{2}$ | 3 mac | 5 | 边 | ， 21 | 明 | min | nse |  | 12 s | 1920 | A12 | （2a） | S2 |  | $1{ }^{1}+8$ | 18 | 5 | Eir | 3 | 2 |
|  | 㫛 | 18， | 碞 | 2s， | Ext | 6 6 | 3its | 11／4 | $2{ }^{2}$ |  | 迷 | 35x｜ | 1\％ | 17 |  | cast | 2ne |  | $1 / 4$ | 1 mol | wer | ET | ， 3 | 3 | 3ner |
|  | 18 | sis | 12 | $\triangle$ | 5 | $3{ }^{3}$ | 5：5 | 36 | 32es | 34 | ：3 | ，m | 9， | 19 | $\underline{10+1}$ |  | 20er | 乒 | 10 crs | ret | 3 m | Q： | \％ | ， | 品 |
| $5 \%$ | 13 T | $\underline{3}$ | 13 | cs | 0 | 掦 | 2ma | sex | $2{ }^{4}$ | 249 | $\pm$ | 15：2 | 4 | 08 | \％ | 20¢ | 24－1 | 251 | iies | S | W | 5 ${ }^{2}$ | 58 | 3 | sis |
| $5 \%$ | 20 | 29 | 1 | \％ | 书 | \％ | \％ | 1＊4 | 3 31 | at | －821 | 29， | Lex | ， $\mathrm{Sa}_{5}$ | 2 l | 2309 | ise | ist | 2 | Sem | ？al | \＃： 4 | Se： | Hes | 9 |
| $\begin{array}{llll}5 & 14 & 5 \\ 4 & 71 & 5 \\ 4\end{array}$ | \％ | reil | 19 | 3 | 0 | 3 | 3112 | － | sce， | i | 1.45 |  | 5 | sir | 319 |  | 2 cos | 采 | 等 | cin | 42 | rsid | ＝1 | 3） | 3wn |
|  | ． |  | \％ | ＊ | th | A\％ | 210， | 50940， | 18219 | N | cas | 1291 | Stas | 201 | Hed | 2 m | 23 | 394 | Sis | 2r1 | ， | 31 | 18 | dr） | Hese |
| 5 ， 5 |  | ： | 景 |  | 盛 | An | 1123 | 3040 | 2 mit | 0 | 1407 | 190｜ | 183： | 4 |  | 2 Sc | A | $\cdots$ | 1 | H20 | 104 | Eses | Erct | 迷 | \％ext |
| $5 \mathrm{E}=$ | Ss： | 4 | m | \％1 | 二小 | A10 | \％ | 120 | 10t | 2108 | 20 | mel | $1 \times 0$ | \％ | ${ }_{\text {cose }}$ | ， | 2018 | 211 | 迷 | ist | 129 | 108 | ¢ $\times 1$ | 2난 | xomit |
| 3 ＊3 5 | Heg | 13 | 1－1． | 29 | tis | 201］ | 2 | 2n： | 3：4， | 181 | 212 | ET0 | Cosi | \％ Cl | cs： | 491 | del | me？ |  | tis） | sis | w | is | 54 | tath |
| 522 E | $n$ | 1 | M | 4 | 穴 | 31 | 3 | 318 | 8 m | Sis | 230 | 1935 | 13 | ab | 7n | 3 m | Lest | \％ | 174 | 13： | $1 \times 4$ | uct | St | a | 8 8 \％ |
| $* 2$ | A | \％ | －ss． | ，is | Ext | 43F | 盛 | 3 Sa | 381 | \＄01 | $\underline{n c c}$ | 3591 | 394 | ＋ | 20， | zesi | zei | 201 | अस | 139：3 | 1 | － 1 | 53 | \＄ | $\pm \pm$ |

STATE OF NEN HAMPSHIRE, DEPARTMENT OF TRANSPORTATION - BEREAL OF TRAFFIC
IN COOPERATION WITH US DEPAETHENT OF TRANSDORTATON FEDERAS HGAWAY AOMANSTRATION
AUTOAATIC TRAFFIC RECORDER DATA FOR THE AONTH OF MAY 2016


## 81269107 LONDONDERRY-I-93 NE OFF RAMP EXIT 4

| E |  | $12 \mathrm{Am} \mathrm{B}^{3}$ | 1 AiM | 2 A A | 3 mm | 4 AM | 5 Abs | 6 AM | 7 A ${ }^{\text {a }}$ | 8 A M | 5 A | 10 Am | 19 AM | 柆 P阿 | $1{ }^{1} \mathrm{PG}$ | ) 7 Pr | 3 PR | $\triangle \mathrm{PM}$ | 5 PR | 6PM | 7 M | B PM | ¢ PM | 10 PM | $1)^{1} \mathrm{Pht}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E | 1 | ¢ | 337 | 54 | 35 | 26 | 25 | 97 | 1091 | 232 | 339 | 480] | 5 5 ) | 767 | $7{ }^{7} 5$ | 631 | 676 | 760] | 672 | 6531 | 509 | 405 | 272] | 348 | 323 | 8 B 71 |
| 3 | 3 | rof | 45 | 44 | 3 B | 45 | 17 | 7421 | 472 | 467 | 423. | 4 CE | 47 F | 492 | 334 | 815 |  | 13305 | 1478 | 1056 | 615 | 460 | 3241 | 210 | 175 | 11288 |
| 4 | 4 | 31. | 59 | 49 | 34 | 41 | 106 | 269 | 44.2 | 475 | 391 | 453 | 552 | 559 | 573 | 63? | 7,0 | 5201 | 1778 | 1040 | 672 | 480 | 3e7 | EYC | 594, | 4133 |
| 5 | 5 | 122 | 52 | 50 | 43 | 54 | 90 | 236 | 435 | 496 | 4 ES | 454 | 398 | 569 | 419 | 915 | $\underset{1}{1076}$ | +1929 | 1828 | 1824 | 725 | 474 | 359 | 244 | 1B6 | 1718: |
| E | 6 | 122 | 21 | 465 | 41 | 03 | 109 | 254 | 491 | 45 | 405 | 459 | 562 | 587 | 667 | 901 | +1060 | 1793 | 1708 | 9:3 | 653 | 431 | 392 | 354 | 299 | 1:1433 |
| 7 | 7. | 1501 | 17] | 693 | 42 | 31 | 61 | 138 | 235 | 451 | 644 | 593 | 6 d | 754 | 515 | 857 | 791 | 795 | EES | 627 | 521 | 4 Et | 369 | 291 | 246 \} | 19518 |

STATE OF NEW HANPSHIRE, DEPARTMENT OE TRANSPORTATION ~ BUREAL OF TRAFFIC
EN COOPERATION WATHUS DEPARTMENT OF TYANSFORTATION FEDERAL HGHWAY ADMNSTRATOR
LONDONDERYMATIC TRAFFFC RECORDER DATA FOR THE MONTH OF MAY 2015
 LONDONDERRY-1-93 NB ON RAMP EXIT 4
; ${ }^{\mathrm{E}}$;
5 - 3


| 5 | 5 | 5 |
| :--- | :--- | :--- |

$=7$
Sum Anet ANDF

| 22af | 185 | 2Ant | 3 AM | 4 AM | 5 A ${ }^{\text {a }}$ | E AlM | 7 AM | BAEs | 9 Ap | 10 A A 5 | fif Am | 12PM | - Ps | 3 PM | 3 P P | 4 P \% | 5pm | ¢ $\mathrm{P}_{\text {P }}$ | 7 Pm | 日 $\mathrm{P}^{\text {M }}$ | P PM | to pm | 11 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 72 | 5 | 35 | 301 | 25 5 | 59 | 977 | 194 | 2741 | 438 | 603 | Ex | 657 | 59 | 639 | 5 S | 3 36 | 4391 | 42 | 377 | 303 | 233 | \% 13 | 7. | 7478 |
| 17 | 30 | 3 | 36 | 83 | 224 | 693 | 1091 | 855 | 610 | 559 | 542 | 5 S 3 | 595 | 6 CO | E30) |  | 729 | 69 | 4 21 | 305 | 2231 | 432 | 88 |  |
| 42 | 76 | 19 | 42 | 75 | 235 | 298 | 2175 | B77 | 5is | 56.5 | 655 | 619 | 617 | 692 | 79 | 782 | 773 | 572 | 43 E | 329 | 2 C | 145 | 74 | 76976 |
| 30 | 26 | 31 | 35 | Fe, | 238 | 69 | EGE | 865 | 69\% | 593 | 618 | 759 | 654 | 753 | 871 | 938i | 895 | 633 | 433 | 332 | 252 | 167 | 85 | 11732 |
| 49 | 37 | 40 | 42 | 62 | 237 | E69, | : 643 | 839 | 650 | 615 | 625 | 783 | 688 | 856 | 545 | 876. | 859 | 627 | 455 | 377 | 256 | 223 | +34 |  |
| B0, | 54 | 43 | 40 | 42 | 6? | 2001 | 341 | 50 | 509 | E41 | 733 | 373 | 740 , | 715 | 7\% | 6.41 | 5551 | 502 | 413 | 338 | 373 | 225 | ¢53! | 9392 |

STATE OF NEW HAMPSTHRE，DEPARTMENT OF TRANSPORTATION－RUREAIU OF TRAFFIC
N COOPERATION WITH U．S．DEPARTMENT OF TRANSPORTATIGN FEDERAL HGHWAY ADAIINISTRATION AJTONATC TRAFFIC RECORDER DATA FOR THE MONTH OF MAY 2016


|  |  |  | 12 AM | 1 AM | 2 Am | 3 Aln | 4 Asi | 5 A | \％And | 7 AMS | BAM | 924 | İAM | $11 / \mathrm{AM}$ | 12 FM | 号啉 | 2 P | 3 P1 | 4 PKS | 5 P相 | 6 PM | 7 P 礝 | 界 | 昌积 |  | 81p | ， |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $s$ | 8 | \％ | 12 | 6 | 4， | 20 | 30 | $6{ }^{6}$ | 65 | 197 | 318 | 424 | 5231 | 52 s | 63 ¢ | E戔电： | 554 | 63 2 | 559 | ${ }^{4} 5$ | 456 | 340 | 3 Cl | TR 7 | 139 | 6］ | 153 |
| 5 | 3 | 3 | 72 | 45 | 27 | 41 | 193 | 2 c | 531 | 76 | 784 | 519 | 56 | 522 | 543 | E93 | 674 | B22 | $9!3$ | 545 | 629 | 452 | 347 | 258, | 1431 | 107 | 1078 |
| 5 | 4 | 4 | 58 | $3+$ | 2 C | 46 | 134 | 275 | 544 | 774 | 170 | 5371 | 545 | 59 | 615 | 57 | 659 | $8 \times 1$ | $62:$ | c53 | 647 | 4.3 | 3151 | 25. | 155 | 8 E | 19472 |
| 5 | 5 | 5 | 63 | 23 | 26 | 37 | 184 | 270 | 522 | 7453 | 751 | 545 | 372 | 577 | 5 m | 677 | 658 | E．3 | 857 | 54 | 53 ， | 432 | 340 | 320 | 202 | 110 | 19391 |
| 5 | 6 | 5 | 76 | 53 | 45 | 3 E | 112 | 263 | $51!$ f | 717 | 734 | 353 | 59 | 693 | Ex5 | 694 | 724） | 896 | 950 | 456 | 674， | 502 | 357 | 256 | 246 | 155 | 1140 |
| 5 | 7 | 7 | 95 | 59 | 43 | 27 | 54. | 92 | 174 | 346 | 444 | 322， | 528 | 627 | 607 |  | E73 | 和3 | 613 ： | 636 | 52 | 455 | 32 | 28 | 22 |  |  |

STATE OF NEW HA APSHARE GEPARTMENE OF TRANSPORTATION－日UREAU OF TRAFFIC
IN COOPERATION WITH US．DEPARTWENT OF TPANSPORTATION FEDERAS HIGHWAY ADNNISTRATION
ONDONDERRYOMATIC TRAFFIC RECORDER DAYA FOR THE WONTH OF MAY 2OIG

| ＊ | $\square$ | － | 81269 |  | ONDO | DER |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \％ | $\stackrel{*}{*}$ | ${ }_{*}^{*}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | E |  | 12 Ans | 1A3 | 2 婑 |  | 4 A 析 | － 5 Ant | 5 Alf | 7 Am | 8 A ${ }^{\text {a }}$ | 9 Am | to Am | If A A | İ－ | 1 Pm | 2 Fut | 3 P | 4 PM | 5 P ¢ | 6 P8 | 7 PM | $5 \mathrm{~F} \mathrm{H}_{1}$ | 9 PM | 10 PRA | \％9 | otat |
| 5 | $\delta$ | 1 | 39 | 8 | 12 | 19 | $1{ }^{\text {5 }}$ | 53 | 73 | 13 | $1{ }^{2} 2$ | 23 | 366 | 384 | 334 | 378 | 315 | 290］ | 234 | 25 | 23 S | 214 | 126 | ＋0， | 44 | 29 | S 514 |
| 5 | 3 | 3 | 8 | 19 | 17 | 39 | 127 | 438 | 646 | 687 | 587 | 330 | 252 | 259 | 208 | 284 | 2.81 | 294 | 266 | 386 | 209 | 142 | 96 | 79 | 4 | 18 | 5387 |
| 5 | 4 | 4 | 10. | 11 | 25 | 34 | 1441 | 459 | 597 | 69 | 546 | $3 \% \mathrm{~F}$ | 253 | 295 | 265 | 225 | 313 | 290 | 301 | 340 | 212 | 141 | 112 | 30， | 63 | 24 | 5835 |
| 5 | 5 | 5 | 18. | 15 | 18 | 25 | 141 | 419 | 609 | 677 | 615 | 358 | 369 | 261 | 2741 | 292 | 228 | 313 | 293 | 298 | 220 | 155 | 133 | 83 | $0 \cdot 3$ | 13 | 5574 |
| 5 | 6 | も | d | 15 ！ | 25 | 4.5 | 130 | 422 | 532 | 637 | 54 | 452 | 3i1． | 325 | 2 as | 278 | 305 | 314. | 30. | 319 | 255 | 182 | 5 | E2 | ： 561 | 20. | 5959 |
| 5 | 7 | 7 | 2 C | $1{ }^{\text {¢ }}$ | 12 | 17 | 42 | 59 | 131 | 195 | 2 EB | 349 | 358 | 437 | 430 | 34 Et | 379 | 383 | 318］ | 2201 | ${ }^{245}$ | 153. | 154 | 321 | 55 | 70 | 4915 |
| Sum | AWD |  | 44 | 67 | 89 | 141 | 542 | 1729 | 2384 | 2691 | 2266 | 1527 | 1155 | 1140 | 1116 | 1080 | 1.194 | \＄220 | ＊168 | 1243 | 926 | 50 | 439 | 361 | 249 | 89 | 23450 |
|  | A ${ }^{\text {a }}$ |  | 11 | 17 | 22 | 35 | 136 | 432 | 596 | 673 | 587 | 382 | 289 | 285 | 279 | 270 | 299 | 305 | 292 | 311 | 232 | 150 | 110 | 90 | 62 | 22 | 5865 |

STATE OF NEW HANESHIRE, DEFARTINENT OF TRANSPORTATION -BUREAU DF TRAFFIC


| * | 0 | 0 | B9 269 |  | NDO | DER |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| - | ${ }^{4}$ | ${ }^{4}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | E |  | 12 A | 1 AR | 2 Ak | 3 AM | 4 AM | 5 A 3 | 6 Ax | 7 새수 | 4 A¢ ${ }^{\text {a }}$ | ¢ $\mathrm{ck}^{\text {a }}$ | 10 Abs | 11.40 | 12 P4* | 1 PM | 2 FM | 3 pM | 4 P閏 | 5 PL | G FH | 7 PM | BPM | 9PM | 40pM | it |  |
| $\underline{5}$ | $s$ | 1 | 37 | 29 | 7 | P1 | 22 | 56 | 83 | Q ${ }^{\text {a }}$ | 173 | 2 ${ }^{\text {a }}$ | 383 | 369 | 3 C 产 | 331 | 323 | 299 | 283 | 2941 | 220 | 232 | 1561 | \%21] | T13 | 4 | 4367 |
| 5 | 3 | 3 | 3 | 3 | 22 | 52 | 196 | 529 | 552 | 534 | 395 | 3 F | 229 | $35 \overline{1}$ | 184 | 269 | 246 | 243 | 212 | 228 | 16 | 12 E | +0, | 94 | 81 | 22 | 5022 |
| 5 | 4 | 4 | 17 | 22 | 32 | 52 | 250 | 514. | 568 | 563 | 414 | 280 | 244 | 2 LC | $246 ;$ | 245 | 249 | 264 | 265 | 245 | 150 | 152 | 210 , | 68 | 80 | 29 | 5243 |
| 5 | 5 | 5 | 21 | 21 | 27 | 4 C | ; ${ }^{\text {P }}$ | 519 | $\dot{5} \leqslant 8$ | 527 | 413 | 302 | 192 | 271 | 300 | 247 | 293 | 274 | 253 | 231 | 176 | 135 | 319 | 115 | 75 | 47 | 5343 |
| 5 | \% | 6 | 19 | 49 | 35 | 50 | 32 | 484 | 527 | 524 | 418 | 283 | 237 | 245 | [43: | 2 F ¢ | 268 | 28 | 265 | 268 | 260 | $1{ }^{19}$ | 140 | 15 | 125 | 55 | 5452 |
| 5 | 7 | 7 | 19 | P6 | 22 | 21 | 52 | 335 | 150 | 210 | 266 | 273 | 293 | 397 | 352 | 3 TH | 343 | 3:5] | 349 | 295 | 335 | 29. | 2221 | 120 | 107 | 701 | 5136 |
| Sumb | AND |  | 76 | 76 | 122 | 202 | 777 | 2030 | 2195 | 2146 | 1641 | 1474 | 902 | 978 | 967 | 965 | 1059 | 1041 | 998 | 977 | 763 | 573 | 471 | 408 | 35 | ¢ 54 | 27500 |
|  | AWD |  | $\because .19$ | 19 | 34 | 51 | 194 | \$08 | 5.49 | 537 | 410 | 294 | 226 | 245 | 242 | 241 | 265 | 260 | 250 | 244 | 191 | 143 | 118 | 102 | 91 | 39 | 5265 |

SFATE OF NEW HANAPSHIRE, DEPARTMENT OF ERANSPORTATION - BUREALI OF TRAFFIC


 excl $5 / 30$ - Holiday

STATE OF NEW HAMPSHERE，DEPARTMEET OF TRANSPORTATION－BUREAU OF TRAFFIC
IN COOPERATION WITH U．S DERARTMENT OF TRANSPORTATIONFEDERAL HIGHWAY ADKINISTRATION

## AUTOMATIC TRAFFIC RECORDER DATA FOR THE WONSH OF MAY 2016

## ＊B B 269102 ZONDONDERRY－1－93 NB ON RAMP EXIT 5

|  |  |  | 12 Am | 1 AM | 2 AM | 3 ABM | 4 A 2 ¢ | 5 A ${ }^{\text {a }}$ | 古的解 | 7 AM | 明的 | 9ats | to Ant | if AM | 12 Pm | 1 PM | 2 FM | 3 FNA | 4 PM | 5 PM | 6 Pa | 7 FM | 日 PM | 9 P | to P3 | 11 pg | 迷 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | \＆ | $\ddagger$ | 75 | 31 | 27 | ${ }_{57} 7$ | 26 | 53 | 85 | 5431 | 2561 | 417 | 451 | 530 | 526｜ | 525 | 541 | 445 | 463 ！ | $3)^{3}$ | 359 | 329 | 254 | 158 | 136 | 53 | 63 |
| $s$ | 2＊ | 3 | 5 | 45 | 30 | 17 | 21 | 69 | 515 | \＄BE｜ | 237 | 356 | 455 | 4.55 | 967 | 446 | 475 | 425 | 355 | $33{ }^{3}$ | 267 | 239 | 216 | 152 | 120 | 58 | 56 |
| 5 | 30 | 2 | 3 ${ }^{\text {e }}$ | 28 | 23 | 23. | 5 | 56 | 323 | 139 | i82 | 293： | 364 | 451 | 4.47 | 426 | 415 | 3 d 5 | 365 | 325 | 387 | 246 | 241 | 153 | 906 | 78 | 52 |
| 5 | 3 | 3 | 61 | 34 | 26 | 56 | 79 | 诃 7 | 5513 | 1061 | $7{ }^{7}$ | 592 | 447 | 46 | 4 E 9 | 597 | 675 | 825 | 850 | 657 | 555. | $3{ }^{3} 1$ | 2 E | 192 | 133 | 71 | 4019 |
| 5 | 24 | 3 | 坆 | 36 | 32 | 75 | H9 | 227 | 515 | 1602 | 336 | 513 | $4{ }^{4} 2$ | 518 | 458 | $4{ }^{49}$ | 715 | 806 | 84］ | 732 | 544 | 423 | 305 | 205 | 73 | 95 | 1212 |
| 5 | It | 3 | 42 | 21. | 25 | 54 | 75 | 233 | 624 | 1907 | E32 | 506 | 557 | $5 \div 5$ | 513 | 481. | 79 | 823 | 399 | 755 | 525 | 453 | 305 | 225 | 159 | E6 | 194 |
| 5 | ， | 4 | 85 | 35 | 51. | 46 | 70. | 218 | b13 | 986 | 323 | 520 | 511 | 477 | 535 | 528 | 692 | 378 | 82 C | 744 | 438 | $3{ }^{3} 4$ | 293 | 174 | 144 | 75 | 101 |
| 5 | 25 | H | 185 | 69 | 45 | 63 | 80 | 246 | 633 | 955 | 336 | 559 | 478 | 547 | 534 | 553， | 7．6） | 8639 | 823 | 821． | 635 | 436 | 352 | 250 | 36 | 96 | 185 |
| 5 | \％ | 5 | 93. | 30 | 25 | 47 | 昭 | 1939 | 395 | 99ir | ． 65 | 574 | 59 | 526 | 585 | 529 | 322 | 919 | 859 | $8: 9$ | 5261 | $46^{4}$ | 284 | 231 | 7 3 | 95 | ETE |
| 5 | $2 \overline{2}$ | 5 | 115 | Q ${ }^{\text {a }}$ | 33 | 5 5 | 5 Sc | 247 | 6i24 | 30：3 | B84， | 6：5 | 550 | 576 | 511 | 517 | 738 | E76 | 720 | $84 i$ | 568 | $45 E$ | 362 | 235 | 213 | 317 | 116 |
| 5 | \％ | E | 12 | （6） | 39 | 63 | S01 | 220 | 600 | 539 | 602） | 595 | 5ag | 591 | 635 | 629 | 733 | 931 | 6. | 8231 | 613 | 505 | 339 | 241 | 226 | ＋35 |  |
| 5 | 27 | $\underline{6}$ | TO｜ | 55 | 35 | 5？ | 16 | 242 | 575 | 938 | 7G7 | 532 | 594 | 810． | 650 | 51 | 760 | 25， 2 | 697 | 674 | 59 | 454 | 324. | 392 | 207 | 140 | 110 |
| 5 | 7 | ． | 11： | 42 | 32 | 37 | 45 | g2： | 197 | 350 | 443 | 515 | 578 | E341 | 594 | 613 | 647 | 527 | 523 | 502 | 437 | 374 | 30： | 230 | 190 | 126 | ： 12 |
| 5 | 28 | 7 | 89 | $4{ }^{\text {a }}$ | 32 | 57 | 46 | Q4 | 135， | 356 | 462 | 53， | 559 | 493 | 542 | 4 CE | 586 | 5941 | 478 | 431 | 350 | 319！ | 268 | 2071 | 15，哏 | 199］ | 72 |




STATE OF NEW HAMPSHIRE，DEPARTMENT OF TRANSPORTATBN－BUREAU OF TRAFFIC W COOPERATION WITHILS DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMNISTRATON

| ${ }^{4}$ | 0 | 0 | 81269 |  | ONDO | DER | Y－1．93 |  | RA | EX: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | $\underset{\sim}{A}$ | $\stackrel{*}{*}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| N |  |  | 12 AM | $1 A^{\text {a }}$ | 2 Am | 3 Am | 4 AM | 5 Am | 6 AM | 7 AH | 8 AB | 9 ¢ M | 10 裪 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ${ }_{2}$ | E | 1 | no | 63 | 53 | 303 | 3 | 39 | 67 | 151 | 2 F |  | $4{ }^{4} 7$ |  |  | 1， | 2 P\％ | 3ph | 4 Pan | 5 Pm | Lpat | 7 P\％A | BPM | 9 PH | 14P號 | 12 Pk |  |
|  |  |  |  |  |  |  |  |  |  |  |  | 3.2 | 447 | 559 | 5 FE ， | 562 | 356 | 5.27 | 472 | $45^{2} 2$ | 367 | 346 | 269 | 昭 | ：31 | 61 | 6572 |
| \％ | 29 | 1 | 97 | $6 ?$ | 35 | $2{ }^{2}$ | 18. | 25 | 109 | 152 | 219， | 293 | 345 | 4 C ［ | 427 | 444 | 449 | 420 | 422 | 46 | 369 | 304 | 242 | 236 | ：50 | 112 | 5776 |
| 5 | 30 | 2 | 35 | 35 | 33 | 10. | 29 | 40 | 72. | 129 | 152 | 223 | 315 | 415 | 455 | 441 | 697 | 472 | 419 | 369 | 342 | 340 | 874 | 22 | 16： | 75 | 55.56 |
| 5 | 3 | 3 | $4 ?$ | 37 | 34 | 47 | 143 | 321 | 739 | 737 | 623 | 450 | 334 | 433 | 444 | 513 | 61 | 720 | 905 | 943 | 58. | 456 | 329 | 2751 | 15 C | 103 | 10134 |
| 5 | 24 | 3 | 47. | 35 | 33 | 4 | 157 | 301 | E69 | 647 | 902 | 465 | 44 S | 512 | 493 | 447 | 564 | isc， | SSE | 96 | $5{ }^{5} 4$ | 4.95 | 344 | 28 | 14.31 | 121 | 10280 |
| $\stackrel{3}{3}$ | $3 i$ | 3 | 5 5 | 2 F | 23 | 40 | 1900 | 295 | 741 | 82t | 706 | 5011 | 472 | 693 | 547 | 542 | 677 | 92\％ | 593 | 962． | 544 | 444 | 327 | 291 | 19. | 178 | 10251 |
| $\pm$ | 4 | 4 | 56 | 45 | 27 | 42 | 146 | 326 | 7 Ca | ？ 96 | S39 | 448 ， | 316 | $44^{4}$ | 496 | 516 | 5kE | 70 ¢ | 1927 | 1093 | 708 | 378 | 337 | 276 | 147 | 99 | 10554 |
| 5 | $2{ }^{\text {2 }}$ | 4 | 711 | 31 | 33. | 41 | 171 | 323 | 736 | 754 | 61 | 483 | 448 | 530 | 527 | 571 | 6,2 | $8{ }^{\text {cin }}$ | 923 | 977 | 614 | 437 | 433 | 351 | 16. | 126 | 70250 |
| 5 | ง | $\stackrel{5}{4}$ | 72 | 38 | 35 | 41 | 153 | 305 | 590 | 866 | 414 ！ | 252 | \＄57 | 499 | 526 | 520 | 634 | 7 Sk | 977 | 6 60 | 653 | 434 | 359 | 324 | 1解 | 139 | 10707 |
| 5 | 28 | 5 | 113 | Et | 34 | 51. | ：42 | 313 | 697 | 791 | 674 | 484 | 472 | 535 | 523 | 53 E | 639 | 837 | R19 | 973 | 020 | 485 | 374 | 347 | 227 | 156 | 1006 |
| 5 | E | $\sigma$ | 75 | 59 | 44 | 45 | 173 | 273 | 714 | 163 | 649 | 500 | 455 | 512 | $5 \mathrm{EL4}$ | 502 | 54. | E71 | G40 | 93 | 51 b | $4{ }^{6} 5$ | 356 | 329 | 216 | 569 | 51035 |
| 5 | 27 | 6 | E： | 42 | 29 | 53 | $\pm 2$ | 25 ． | 707 | 369 | 601 | 514： | 469 | 539 | 577 | 581 | E69 | a3？ | 222 | ${ }^{1} 15$ | 482 | 432 | ，3， 36 | 297 | 223 | 5 | 3514 |
| 5 | 7 | 7 | 11 | 64， | 37 | 35 | 3 3 | 100 | 167 | 311 | 395 | 446 | 488 | 523 | 54 | 561 | $6{ }^{2} 20$ ， | 621. | 598 | 547 | 435 | 335 | 307 | 297 | 197 | ！59］ | 7010 |
| 5 | 28 | \} | 710 | 61 | 53 | 42 | 23） | 60 | 777 | 275 | 39 | 4281 | 425 | 453 | 48 | 4 E 9 | 453 | 43 T | 436 | 456 | 323 | 348 | 369 | 319 | 237 | 159 | ¢092 |



exci 5－24
6246

STATE OF NEW HABFSHIRE，DEPARTMENT OF TRANSPORTATION－EUREAU OF TRAFFIC
IN COOPERATION WTH US．DEPART解ENT OF TRANSPORTATON FEDERAE HIGHWAY ADMBWSTRATION
AUTOMATIC TRAEFIC RECORDER DATA FOR THE MONTH OF MAY 2016
LONDONOERRY－I－93 SB ON RAMP EXIT 5
$\begin{array}{lll}0 & \mathrm{E} & \mathrm{B} \\ \mathrm{B} & \mathrm{A} & \mathrm{A} \\ \mathrm{F} & \mathrm{Y}\end{array}$
$\begin{array}{ll}29 & 1 \\ 29 & 1 \\ 29 & 1\end{array}$
39
$\begin{array}{llll}5 & 35 & 2 \\ 5 & 3 & 3\end{array}$ 3
3

| AM | A A | A明 | 3 A ${ }^{4}$ | 4 AK | 5Al | GAM | 7 AB | B A 4 | 9 A A ${ }_{\text {d }}$ | 15 AK | 118 AR | $12 \mathrm{PF} \times$ | \＃PRs | 2 PM | 3 ¢ ${ }^{\text {d }}$ | 4 Pat | $5 \mathrm{P} \times 1$ | E PM | 7 PM | BP釉 | 9 PM | 10 PM | 11 P |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 351 | 25 | 18 | 16. | 19 | 459 | 82 | 134 | 170 | 212 | 256 | 297 | 38 | $3{ }^{3}$ | 275 | 251 | 2 c 5 | 214 | ＋${ }_{\text {B }}^{\text {c }}$ | 135 | 184 | 54 | 541 | 2 B | 3534 |
| 3 3t | 2 S | 11 | 21 | 23 | 43. | 56 | 192 | 447 | 192 | 253 | 27 ， | 2 E 5 | 253 | 246 | 206 | 137 | 213 | 464 | 129 | 19 | 63 | 65 | 43 | 3270 |
| 3 y | 15 | 13 | 2］ | 35 | 5 | 63 | E0 | 325 | 151 | 184 | 249 | 24.5 | 212 | 211 | 205 | 18. | 570 | 192 | 146 | 139 | 78 | 43 | 28 | 2863 |
| 54 | 27 | 39 | 65 | 175 | 390 | 520 | 4 cos | 453 | 375 | 273 | 275 | 313. | 293 | 341 | 437 | 385 | 393 | 289 | 167 | ！29 | 95 | 65 | 47 | 6114 |
| 51 | 44 | 35 | 61 ！ | 214 | 396 | 521 | 532 | 331 | 331 | 277 | 271 | 316 | 265 | 327 | 393 | 435 | 474 | 121 | 1992 | 931 | E2 | 59 | 4 a | 6 6 25 |
| 38 | 18 | 27 | 59 | 185 | 400 | 566 | 523 | 46 | 377 | 327 | 323 | 236 | 312 | 3 E 4 | 426 | 462 | 472 | 22e | 139 | i33 | E6 | 94 | ${ }^{1} 1$ | 6350 |
| 53 | 32 | 3 ？ | 65 | 187 | 423 | $5: 8$ | 515 | 456 | 549 | 324. | 275 | 296 | अ4 | 327 | 402 | 3¢8 | 449 | 273 | 185 | 326 | 95 | 65 | 5 | 619 ${ }^{6}$ |
| 54 | 23 | 33 | 65 ： | 153 | 476 | 527. | 549 | $4{ }^{4}$ | 36 준 | 249 | 270 | 290 | 275 | 320 | 465 | 423 | 4311 | 254 | \％27 | 34 | 95 | 67 | $5{ }^{5}$ | 6356 |
| 52 | 34 | 42 | 45 | 136 | 435 | 538 | 482 | 418 | 412． | 317 | 310 | 313 | 282 | 324 | 425： | $4{ }^{4} 2$ | 415 | 251 | 173 | 176 | 102 | 8. | 45 | 629 |
| 69 | 31 | 34 ） | 54 | 129 | 413 | 598 | 520 | 476 | 363 | 311 | 352 | 3 g | 289 | 297 | 458 | 474 | 455 | 281 | 393 | 139 | 720 | 72 | 65 | 6353 |
| 57 | 26 | 42 | 42. | 1.5 | 375 | 479 | 424 | 455 | 3 B 4 | 301 | 2891 | 353 | 308 | 403 | 4 SE | 451 | 4：1 | 299 | 276 | 140 | 119 | 75 | 57 | 6439 |
| 47 | 34 | 53 | 6 | 133. | 36 | 454 | 544 | 43 | 356 | 337 | 326 | 332 | 316 | 3 F 4 | 403 | 343 | 355 | 200 | $15^{3}$ | 136 | 102 | 77. | E 4 | ETV1） |
| 49 | 15 | 15 | 29） | 48 | ：19 | 128 | 209 | 259 | 373 | 288 | 322 | 307 | 314 | 363 | 295 | 319 | 262 | 管高 | 180 | 134 | 500 | 163 | Es | 6391 |
| 45 | 37 | 33. | 29 | 4 | 2 | 136 | 192 | 273 ： | 2， 5 | 286 | 249 | 242 | 243. | 254 | 222 | 2 T 4. | 125 | 47 | 165 | 143 | 192 | 73 | 57 | 3709 |
| 4 c | 33. | 31 | 631 | 18. | 492 | 55s | 561. | 469 | 330 |  | 274 | 272 | 268 | 30 al | 399 | 359 | 469， | 252 | 152 | ：641 | 60） | 7 c ［ | 42 |  |



DERRY
CRYSTAL AVE SO OF TSIENNETO RD STATE COLNT

438 Dubuque Street, Manchester, NH 03102
Tel: 603-669-4664 Fax.603-669-4350
Web: www.snhpc.org


DERRY FOLSOMRD NEST OF NH 28 STATE COUNT


DERRY
PINKERTON ST
EAST OF TSIENNETORD
STATE COUNT

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Latitude: $0^{\prime} 0.0000$ Undefined


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| Start | Mon | Tue | Wed | Thu | Ffi | Average | Sat | Sun | Week |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | 02-May-16 | 03-May-16 | 04-May-16 | 05-May-16. | 06-May-16 | Day | 07-May-16 | 08-May-16 | Average |
| 12:00 AM |  |  | 31 | 35 | 47 | - 38 | - 85 | . 85 | 5711 |
| -0100 | * | * | 26 | \% 25 | 24 | 25 | 37 | $\cdots 32$ | \% 29 |
| 02:00 |  | * | 27 | 27 | 20 | 25 | 35 | 29 | 281 |
| 03:00 | * |  | 37 | 42 | 40 | 40 | 28 | 15 | 32 |
| 04:00 |  |  | 127 | 119 | 109 | 118 | 51 | 29 | 87 1318 |
| \% 0500 |  |  | 309 | 320 | 308 | 312 | 112 | 56 | $221 \sim$ |
| 06000 |  | * | 938 | 959 | 909 | -935 | 301 | 132 | 648 , प |
| 07:00 |  |  | 1097 | 1159 | 1084 | 1113 | 561 | 353 | 851 < , , ${ }^{\text {a }}$ |
| 08:00 |  | - | 1021 | 1102 | 1042 | 1055 | 788 | 461 | 883 प, щ |
| 09:00 |  |  | 873 | 931 | 946 | 917 | 929 | 676 | 871 - |
| 10:00 |  |  | 985 | 950 | 995 | 977 | 1106 | 822 | 972 , < $\quad \cdots \times \cdots$ |
| 1100 |  | 1034 | 1001 | 1131 | 1202 | 1092 | 1286 | 879 | 1089 , , , , |
| 12:00 PM |  | 1087 | 1110 | 1101 | 1248 | 1136 | 1047 | 983 | 1096 , < , |
| 0100 |  | 1085 | 1083 | 1010 | 1309 | 1122 | 1142 | 745 | 1062 , , , , , , |
| 02:00 |  | 1446 | 1410 | 1505 | 1496 | 1464 | 3134 | 821 | 1302, , , < |
| 03:00 |  | 1441 | , 1382 | 1363 | 1495 | 1420 | 977 | 806 | $1244 \times 1$ |
| 04:00 |  | 1457 | 1540 | 1476 | 1523 | 1499 | 1005 | 741 | 1290 - , < |
| 05:00 |  | 1395 | 1355 | 1346 | 1415 | 1378 | 886 | 784 | 1197 - |
| 0600 |  | 1050 | 885 | 934 | 998 | 957 | 767 | 640 | $879 \square \square$ |
| 07:00 |  | 594 | 618 | 666 | 720 | 650 | 572 | 515 | 614 प |
| 08:00 |  | 467 | 393 | 429 | 526 | 454 | 466 | 361 | 440 , 4 |
| $09: 00$ |  | 247 | 236 | \% 277 | 417 | 294 | 352 | 218 | 291 \# |
| 10:00 | * | 119 | 119 | 166 | 306 | 178 | 241 | 153 | 184 |
| 1100 |  | 80 | 89 | 95 | 128 | 98 | 126 | \% 47 | 94. |
| Day Total | 0 | 11502 | 16692 | 17108 | 18307 | 17307 | 14034 | 10383 | 15461 |
| \% Avg. WkDay | 0.0\% | $65.5 \%$ | 95.4\% | 99.2\% | 105.8\% |  |  |  |  |
| \% Avg. |  |  |  |  |  |  |  |  |  |
| Week | 0.0\% | 74.4\% | 108.0\% | 119.0\% | 118.4\% | 115.9\% | 00.8\% | 67.2\% |  |
| AMPeak | - | 11.00 | 07:00 | 07:00 | 11:00 | 07:00 | 11:00 | $11: 00$ | 1100 |
| Vol. | - | 1034 | 1097 | 1159 | 1202 | 1113 | 1288 | 879 | 1089 |
| PM Peak | - . | 16:00 | 16:60 | 14:00 | 16:00 | 1600 | $13: 00$ | 12:00 | 14:00 |
| Vol. | - | 1457 | 1540 | 1505 | 1523 | 1499 | 1142 | 983 | 1302 |

438 Dubuque Street, Manchester, NH 03102
Tel: 603-669-4664 Fax:603-660-4350
Web: www.snhpc.org

Latitude: 0 ' 0.0000 Undefined


DERRY
NO. MAIN ST
NO OF ACADEMY OR
STATE COUNT

438 Dubuque Street Manchester, NH 03102
Te: 603-669-4664 Fax-603-669-4350
Web: www.snłpc.org
Site Code: 82119052 Staten ID:


DERRY
NO. MAIN ST
NO OF TSIENNETORD
STATE COUNT

438 Dubuque Street Manchester NH 03102
Tel: 603-659-4664 Fax:603-669-4350
Web: www.snhpc.org


Southern New Hampshire Planning Commission

DERRY
SO. MAN ST SO OF THORTON ST STATE COUNT


DERRY
TSENNETORD
WEST OF CHESTERRD
STATE COUNT

438 Dubuque Street, Manchester, N: 03102
Tel: 603-669-4664 Fax:603-669-4350
Web: www.snhpc.org


LONDERRY
NH 1C2 (NASHUARD)
(9) DERRY TJ

STAATE COUNT

438 Duburue Street, Manchester, NH 03602
Tel 603-669-4664 Fax:603-669-4350
WeD: www.snhpc.org

Latitude: 0' 0.0000 Undefined


LONDONDERRY NH 28 (ROCKINGHAM RD) @ DERRY TIL STATE COUNT


## Southern New Hampshire Planning Commission <br> 438 Dubuque Street, Manchester, NH 03102

ONDONDERRY GILCREST RD NO OF NH 102 STATE COUNT

Tel: 603-669-4664 Fax:603-669-4350
Web: WWw.snhpc.org
Site Code: 82269082
Station 1 B:

Latitsde: $0^{\prime} 0.0000$ Undefined


82119071 DERRY- NH 102 (EAST BROADWAY) WEST OF ABBOT ST

. 19071 DER



STATE OF NEW HANPSHIRE, DEPARTMENT OF TRANSPORTATION - BUREAU OF TRAFFIC
IN COOPERATION WITH U.S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION
AUTOMAICC TRAFFIC RECORDER DATA FOR THE MONTH OF APRIL 2014

## 8211901 DERRY- NH 102 (BROADWAY) EAST OF GRIFFIN ST

A

TYPE STATLON YEAR MONTH
62 119011 $\quad 2014$ ATil

| NO | AVERAGE |
| ---: | ---: |
| DAYS | SUNDAY |
| 6 | 12162 |

AVERAGE
WEEKDAY
I7752

PEAK HOUR VOLLMES:
AVERAGE AM: AVERAGE MDDAY: AVERAGE PR:

| Sunday | 665 | 121年 | 883 | AM-EAM TO 10 AM |
| :---: | :---: | :---: | :---: | :---: |
| WEEKDAY | 1054 | 118 | 1224 | MODAY - 10 AM TO 2 PM |
| SATUROAY | 1073 | 3359 | 1302 | PM-2PM TOBPM |

AUTOMATIC TRAFFIC RECORDER DATA FOR THE MONTH OF APRIL 2014

## 82119091 DERRY. FORDWAY ST OVER BEAVER BROOK

12 AM 1 AM 2 AM 3 AM 4 AM 5 AM 6 A
AII 2 AM JAM AM SAM 7 AM 8
AM 10 AM 11

| 1 | 31 | 37 | 22 | 10 | 12 | 17 | 38 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 37 | 18 | 13 | 12 | 45 | 112 | 283 |
| 4 | 28 | 12 | 14 | 13 | 49 | 98 | 228 |
| 5 | 32 | 8 | 14 | 13 | 51 | 117 | 258 |
| 6 | 37 | 19 | 13 | 7 | 33 | 116 | 253 |
| 7 | 48 | 35 | 12 | 14 | 19 | 37 | 94 |

TYPE STATION YEAR MONTH
NO.
$82 \quad 11$ B691 $2014 \quad$ Acili its PEAK HOLR VOLLWES:

| AVERAGE AVERAGE |  |
| :---: | :---: |
| SENDAY WEEKDAY |  |
| 3703 | 5856 |


| AVERAGE | AVERAGE | COMPUTED | PERCENT | PERCENT |
| :---: | :---: | :---: | :---: | :---: |
| SATURDAY | DARY | VOL HAE | GAN | LOSS |
| G3O: | 5628 | $16 B B 54$ |  |  |

AVERAGE AVS: AVERAGE MDDAY: AVERAGE PM

|  | AVERAGE AM: | AVERAGE MDDAY: | AVERAGE PA: |  |
| :---: | :---: | :---: | :---: | :---: |
| SUNDAY | 215 | 335 | 295 | AM-6AMTO 10 AM |
| MEEKDAY | 410 | : 372 | 481 | MDDDA - 10 AM TO 2 FM |
| SATURDAY | 492 | 570 | 589 | PM-2PMTOEPM |

AUTOMATIC TRAFFIC RECORDER DATA FOR THE MONTH OF APRIL 2014 DERRY-FRANKLIN ST EXT NORTH OF FOLSOM RD



## 62269054 LONDONDERRY- NH 28 (ROCKINGHAM RD) EAST OF PERKINS RD

## A



| 20 | 7 |
| :--- | :--- |
| 16 | 4 |
| 17 | 5 |
| 18 | 6 |
| 19 | 7 |


|  | 77 | 44 ; | 58 | 65 | 98 | $143{ }^{\prime}$ | 281 | 57 | 63 | B: | 975 | 695 | 10 | 99 | 931 | 1054 |  | 853 | 769 | 576 | 392 | 249 | 151 | 285 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 163 | 96 | 116. | 114 | 233 | 683 | 1009 | 1361 | 1432 | 1071 | 958 | 1031 | 1005 | 1072 | 1004 | 145 | 593 | 60 | 1139 | 818 | 729 | 46 | 334 | 223 | 19780 |
| 171 | 105 | 98 | 118 | 257 | 64 | 10 | 1409 | 1491 | 1197 | 1004: | 1022: | 110 | 113 | 119 | 150 | 62 | 175 | 125 | 909 | 75 | 527 |  | 240 | 20789 |
| 206 | 132 | 103 | 117 | 196 | 564 | 1003 | 1289 | 137 | 1141 | 1060 | 1006 | 114 | 1147 | 145 | 18 | 17 | 172 | 131 | +1090 | 723 | 493 | 452 | 339 |  |
| 257 | 13 | 101 | 104 | 177 | 202 | 277 | 435 | 598 | 751 | 02 | 051 | 07 | 9 | 105 | 97 | 933. | 790 | 686 |  | 494 |  |  |  |  |


| NO. AVERAGE | AVERAGE | A |  |
| ---: | ---: | ---: | ---: |
| DAYS | SUNDAY | WEEKDAY | SA |
| 5 | 12854 | $2 D G 67$ |  |


| AVERAGE | AVERAGE | COMEDUTED |
| :---: | :---: | :---: |
| SATLRDAY | DAFLY | VOLUME |
| $\$ 3464$ | $\because 18729$ | $5 B O 605$ | PEAK HOUR VOUUNES:


| SUNDAY | 63t | 1014 | 1054 | AM-EAMTO 10 AM |
| :---: | :---: | :---: | :---: | :---: |
| WEEKDAY | $\therefore 1406$ | 1118 | 1797 | MIDDAY - 10 AM TO 2 FM |
| SATURDAY | 751 | 1978 | 1056 | PM-2 PA TO8P的 | AVERAGE AM: AVERAGE MIDDAY: AVERAGE PM:

STATE OF NEW HAMPSHIRE, DEPARTMENT OF TRANSPORTATION - BUREAU OF TRAFFIC
IN COOPERATION WITHU.S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION
AUTOMATIC TRAFFIC RECORDER DATAFOR THE MONTH OF JUNE 2015

| $M$ | $D$ |
| :---: | :---: |
| $O$ | $A$ |
| $N$ | 1 |
|  | $E$ |
| 6 | 28 |
| 6 | 24 |
| 6 | 25 |
| 6 | 26 |
| 6 | 27 |

## B2 119070 DERRY- NH 28 (CRYSTAL AVE) SOUTH OF ROLLINS $\$ T$

A $\stackrel{y}{4}$


| 6 | 28 | 1 | 435 | 69 | 39 | 2 |  | 52 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | +17 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 28 24 | 4 | 118 | 69 | 36 | 24 | 318 | 52 | $\underline{405}$ | 249 | . 313 | 804 | 693 | 97 | 932 | $\frac{952}{1028}$ | 875. | 8611 | B0B | 789 | 741 | 678 | 456 | 342 | 217 | 101. | 10827 |
| 6 | 25 | 5 | 117 | 54 | 38 | 29 | 74 | 181 | 392 | 642 | 823. | 816 | 862 | 1068 | 1110 | 1071 | 1079 | 3050: | 1094 | 1130 | 966 | E54: | 773 | 572 | 394 | 205 | 394 |
| 6 | 26 | 6 | 119 | 59 | 39. | 28 | 75 | 194 | 370 | 620 | 727 | 829 | 867 | 1036. | 1125 | 3144: | 1127 | 108t | 1139 | 1230 | 1137 | p5 | 77 | 69 | 436: | 297 | 1610 |
| 6 | 27 | 7 | 178 | 60 | 55 | 41 | 56 | 190 | 207 | 402 | 574: | 842 | 1051 | 1061 | 1128 | 1054 | 1018 | 1003 | 882 | 894 | 815 | 759 | 618 | 529 | 331 | 163 | 1386 |


| TYPE STATION | YEAR | MONTH |
| ---: | ---: | :---: |
| 82 | 19070 | 2015 |


| NO | AVERAGE |
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| SLAYSAY | SLI |
| 5 | 10927 |


| AVERAGE | AVERAGE | AVERAGE | COMPUTED | PERCENT | PERCENT |
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| WEFKOAY | SATURDAY | DAILY | VOLLME | GAJN | 1055 |
| 55568 | \#36i | 14708 | 6412 |  |  | PEAK HOUR VOL UMES:

SUNDAY
WEEKDAY
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556
815

| 952 | 875 |
| :--- | ---: |
| 1096 | 7174 |
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$A M-G A N T O 10 A N$ MODAY - 10 AM TO 2 PM PM-2P制TO日PM

STATE OF NEW HAMPSHIRE, DEPARTMENT OF TRANSPORTATION - BUREAU OF TRAFFIC IN COOPERATION WITH U.S. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION

AUTOMATIC TRAFFIC RECORDER DATA FOR THE MONTH OF APRIL 2014
82119059 DERRY- ASH ST AT LONDONDERRY TL
$\begin{array}{lll}\mathrm{O} & \mathrm{A} & \mathrm{A} \\ \mathrm{N} & \mathrm{T} & \mathrm{Y}\end{array}$


| 20 | 1 | 25 | 16. | 7. | 10 | 11 | 39 ' | 51 | 102. | 154 | 224 | 292 | 32 | 404 | 284 | 228 | 235 | $205^{\prime}$ | 274 | 249 | 207 | 139 | 68 | 43 | 23 | 60 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 3 | 12 | 5 | 8 | 5 | 39 | 100 | 306: | 405: | 382 | 331 | 354 | 411 | 488 . | 477 | 454: | 551 | 665 | 608: | 461 | 314 | 203 | 107 | 54 | 43 | 6723 |
| 16 | 4 | 45 | 14. | 9 | 4 | 29 | 106 | 281 : | 386 | 357 | 369 | 404 | 471 | 453 | 428 | 496 , | 603 | 619. | 678 | 561: | 366 | 218 | 108 | 64 | 34 | 710 |
| 17 | 5 | 18 | 11 | 9 | 8 | 34 | 125 | 327 | 419 | 424 | 345 | 408 | 456 | 548. | 483 | 576; | 613 | 768 | 753 | 556 | 382 | 254 | 182 | 71 | 60 | 783 |
| 18 | 6 | 21. | 17 | 6 | 6 | 31 | 98. | 255. | 380 | 419 | 427 | 438 | 568 | 559; | 512 | 651 | 724 | 777 | 707 | 574 | 419 | 257 | 196 | 94 | 67 | 8203 |
| 19 | 7 | 24 | 14 | 13 | 9 | 17 | 40 | 89 | 226 | 345 | 457 | 563 | 636 | 662 | 599 | 629 | 613 | 516 | 468 | 449 | 290 | 259 | 146 | 95 | 53 | 721 |

TYPE STATION YEAR MONTH NO.
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224
410
457

| 404 | 271 |
| :--- | :--- |
| 622 | 722 |
| 662 | 629 |

AM- GAM TO 10 AM MDOAY - 10 AMTOR PM PM-2 PMTOBPM

## AUTOMATIC TRAFFIC RECORDER DATA FOR THE MONTH OF JUNE 2015



STATE OF NEW HAMPSHIRE, DEPARTMENT OF TRANSPORTATION - BUREAU OF TRAFFIC
IN COOPERATION WIHUS. DEPARTMENT OF TRANSPORTATION FEDERAL HIGHWAY ADMINISTRATION
AUTOMATIC TRAFFIC RECORDER DATA FOR THE MONTH OF SEPTEMBER 2015


STATE OF NEW HAMPSHIRE, DEPARTMENT OF TRANSPORTATION - BUREAU OF TRAFFIC

## H D D 82269048 LONDONDERRY-NH 102 (NASHUA RD) EAST OF HAMPTON DR

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No.
DAYS
TYPE STATION VEAR MONTH

DAYS
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2015 July
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SUMDAY

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PEAK HOUR VOLLMES:

|  | AVERAGE AM: | AVERAGE MDDAY: | AVEPAGE PN: |  |
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| Stivody | * |  | $\cdots$ | $\therefore A M-6 A M T O L D A$ |
| WEEKDAY | 2478 | 2349 | 2842 | $\therefore$ MIDPAY - 10 AMTO 2 PM |
| SATURDAY | - | $\cdots$ | \% | PM-2PWTO\&PN |



|  | ws |  | \% |  | 動 |  |  |
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|  | RT | Tis | Rip | Et | T* | LT. | 3etal |
| 700.8is | 518 | 83 | E83 | . 337 | .585 | 527 | 2738 |
| 735.715 | 520 | 603 | 209 | 207 | 534 | 562 | 2825 |
| 730.839 | 455 | 8 | 210 | <39 | \$68 | 5 EL | 2850 |
| 745-845 | 309 | 855 | 217 | 235 | 577 | 535 | 8 |
| brenge | 348 | 84 | 20\% | -23) | 573 | 515 | 2705 |


| Southbound |  |  |  |  |  |  |  |  |
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| Hree Perlos | Ciass. | $\dagger$ | 0 | 17 | 1 | 0 | \# | 0 |
| Peak 1 | diehts | 0 | 353 | 461 | Site | (i) | 129\% | 137 |
| Specilied Perisiz | 3 | ** | 92 x | ¢\% | $5 z^{2}$ | sin | \% | 5s |
|  | Oher wehsser | 0 | $3{ }^{\text {a }}$ | 13 | zí | p | 34 | A |
| cretastreat | s | 5 | \% |  | 2 C | $\Leftrightarrow$ | \% | sis |
|  | Total | - | 20, ${ }^{2}$ | 455 | 89 | - | :2st | 778 |
|  | :FH\% | . | 09 | 3.6\% | be2 | e | 697 | 6.9 |
| ymotes |  | on | Sth |  |  |  | $\cdots$ | 7 T |
|  |  | * |  | NE | 等 |  |  |  |
|  |  | ${ }_{5} 1$ | Ti | RT | T | TH | 1 l | Tata |
|  | 400-500 | 363 | : 6.22 | 533 | $5{ }^{5}$ | 375 | 597 | 3230 |
|  | 15-515 | 357 | 597 | 543 | 524 | 74.3 | 520 | 3584 |
|  | 30-530 | . 357 | - 35 | 53 B | 532 | EGI | 525 | $33^{3} 8$ |
|  | 4.45-545 | css | - 348 | 55B | 535 | 835 | 535 | 3359 |
|  | 50.659 | 314 | 515 | 591 | 575 | :523 | 503 | 332 |




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|  | fi | ET | F | 7 | Totė！ |
| 700－650 | 532 | 219 | 517 | 832 | Te |
| 715 cis | \＄35 | 76 | 559 | 846 | 275 |
| $730-835$ | 504 | 246 | 885 | 849 | 7 CBE |
| 345－k45 | 503 | \％ 87 | 696 | 815 | 2134 |
| 8tossa | 510 | 2 z ¢ | 610 | 794 | 2180 |



|  | RT． | 13 | Et | TH | 15. | Jotal |
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| 480503 | 56e | 847 | 1013 | Eis | \％ | 2834 |
| 415－515 | 597 | 263 | 973 | 493 | 0 | 2828 |
| 433－53\％ | 627 | 260 | ． 39 | 1051 | 0 | $2{ }^{2} 13$ |
| 445．595 | 203 | 36 | $\underline{0} 17$ | 1052 | 0 | zes2 |
| $500-600$ | 655 | 307 | $\underline{E S}_{11}$ | 1695 | 0 | $\mathrm{T}^{1} 89$ |


|  |  |  | Southbound（Ekit 4 5s offl |  |  |  |  | Westhaund［NX 102$\}$ |  |  | Eastbaind［ni 102 ） |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tene Periad | Elass． | \％ | 1 | U | 1 | 0 | 8 | 1 | U | 1 | 0 | 7 | 1 | H | 1 | 0 | Total |
| Peak I | i ight | 6邺 | 286 | e | 9\％ | $\dot{1}$ | 0 | sel | 0 | צ07 | 1325 | 1035 | 1 | 0 | 3 cc | 1570 | 200］ |
| Spatitel feras | $\stackrel{+}{*}$ | cs | Ss | cis | 5 | 感 | 0 | \％ | \％ | sp | sis | ss\％ | ms | m | 5 | 580 | － |
|  | He？Yerks | 14 | 14 | 0 | 2غ | d | 0 | 3 | $\theta$ | 10 | 27 | 敕 | 5 | \％ | 13 | 24 | 51 |
| Con tesu feek | 3 | \％ | \％ | 3 | 38 | 的 | ra | 1x | 5 | a | － | ＊ | Re |  | ： | 2 | － |
| 4．45．PAM－5．4．5 f | Tutal | CB3 | 3018 | $\theta$ | 983 | － | $\square$ | 517 | $\therefore 0$ | S17 | 1357 | 1052 | ： |  | 1052 | 18.50 | 2952 |
|  | FHi | （19） | 09： | C | E．s？ | 9 | 0 | 0.39 | 0 | 6．E9 | （b） | His2 | 1 | 4 |  | 0．8 | ． 0.59 |
|  | tresors\％ |  |  |  | 5］ | cos |  |  |  | 1：\％ | $\pm 4$ |  |  |  | 35\％ | Sex |  |











| Amesazt |  | Somat |  | Tater | Fupera |  | 家 | $\begin{aligned} & \text { an } \\ & \hline 10 \end{aligned}$ |  |  | \&ises |  <br>  |
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| Nomh | Critu: 3icationicnar <br>  |  | $4 \pm$ | 8 | 123 | 4 | 113 | 15356 | 75 |  | 3488 | 76 |
| Stued: |  | 108 | 325 | 35 | 63 | 335 | sst | 23E5 |  |  |  | 「15 |
| Fest | A) Leves, wrimz | \% | 3593 | 1059 | 3 s | 420 | 36 | 1355 |  |  | 3ه8\% | 7 7\% |
| Wes: |  | 1 ib | 313 | 235 | $55!$ | 58 | 1153 | 15152 |  |  | 5 seis | x) |
|  |  | : 12 | 1.3) | 3274 | 102 | $3 \mathrm{~F} \times 2$ | +ax |  |  |  |  |  |



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## 8 Loration: North High St af Ash St Ext



Fraiect：Init 4a SDEFS
location：：High 5 tat Mactden Rd

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| :--- | :--- | :--- |
| Annsp | $2014-32015$ | 1.025 |
|  | $2016-3015$ | 0.975 |

Seasoral：
morsection Turning Movement Counts

|  |  | AMP Pak | PM Peak |
| :---: | :---: | :---: | :---: |
| May－16 | Adj Farder | 0.96 | 0.98 |


|  | 2016－Raw |  |  | 201E－AADT |  |  |  | 2015－AAD |  |  |  | 12015－AADT－Rounded |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { AM Peak: } \\ & \{730-830\} \\ & \hline \end{aligned}$ | Fu Feak \｛500－600） | $\begin{gathered} \text { AM Feak } \\ 1730-8301 \end{gathered}$ | Approact Jotals | $\begin{aligned} & \text { PNE Peak } \\ & 5500-650 \mathrm{O} \end{aligned}$ | Appioart Totals | $\begin{gathered} \text { AM Peak } \\ {[745-845]} \end{gathered}$ | Approath Totats | $\begin{aligned} & \text { PM Peak } \\ & (445-545) \end{aligned}$ | Approach Totals | AMI Peak （745－845） | Approars Totals | PM Peak (445-543) | Approzch Totals |
| EB | LT | 12 | 12 | 12 | 14 | 12 | 16 | 12 | 14 | 12 | 16. | 10 | 10 | 10 | 10 |
|  | Thru | 0 | 0 | 0 |  | 0 |  | 0 |  | 0 |  | O |  | 0 |  |
|  | RT | 2 | 4 | 2 |  | 4 |  | 2 |  | 4 |  | 0 |  | 0 |  |
| W／B | 切 | 0 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Thed | $=0$ | 0 | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 1 |  |
|  | RT | － 0 | 0 | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
| N日 | 13 | 0 | 3 | 0 | 313 | 3 | 725 | 0 | 305 | 3 | 767 | 0 | 310 | 0 | 705 |
|  | Thry | 326 | 737 | 313 |  | 722 |  | 305 | $\cdots$ \％ | 704 |  | 310 |  | 700 |  |
|  | RT | － 0 | 0 | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
| S8 | ［T | － 0 | B | 0 | 428 | 0 | 45\％ | 0 | 418 | 0 | 445 | 0 | 420 | 0 | 350 |
|  | Timer | $\because 428$ | 460 | 411 |  | 453 |  | 401 |  | 440 |  | 400 |  | $\because 440$ | aso |
|  | AT | 18 | 5 | 17 |  | 5 |  | 17 |  | 5 | $\vdots$ | 20 |  | 10 | $\because$ |
|  | total | 786 | 1221 | 755 | 755 | 1197 | 1197 | 737 | 737 | 1168 | 1568 | 740 | 740 | 1160 | 1160 |
| \＃lue Seasonal Factor |  |  |  |  |  |  |  | trse Annual Factor |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



|  |  | Southbound（A，High St．） |  |  |  |  | Northbound（N，Kigh St．］ |  |  |  |  | Fasibound（Wadden Md．） |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period Class： | $\bigcirc \mathrm{B}$ | $\bigcirc$ | U | 1 | 0 | T | L | Y | 1 | 0 | 中 | 1 | 1 | 1 | 0 | Total |
| Peak 1 交ghts | 4 | 417 | 0 | 421 | 314 | 31.3 | 0 | 0 | 313 | 419 | 2 | 1 | 0 | 3 | 4 | 737 |
| Specified Yetiad \％ | 2zas | 9ise | m | 34\％ | 93\％ | 趛 | 年 | 御 | Esi | － | 10x： | ${ }^{3} \times$ | 6\％ | 21\％ | 32\％ | 545 |
| 7\％0 AM－9：DOAPOther veliclex | 34 | 11 | f | 75 | $\because 24$ | 13 | － | 0 | 13 | $\therefore 11$ | 0 | 11 | 0 | 11 | 14 | 49 |
| One fibir Fear ，\％$\because$ | $\cdots$ | 3＊ | nt | Ex． | 7 za | 45 | $0 \times$ | Sm． | 4\％ | 3 | $0 \%$ | 9z\％ | D 15 | 70\％ | 于旡 | $\underline{6}$ |
| 7：30 Ant－S：304P Fotal | 18 | 428 | 0 | 446 | 338 | 326 | 9 | 0 | 326 | 430 | 2 | 12 | 0 | 14 | 18 | 786 |
| Pat | 6．5E | 0.95 | \＄ | 0.56 | 0.9 | 0.95 | 0 | 0 | 0.5 | 0.95 | 0.5 | 0.78 | D | 0.44 | 0.55 | 0.94 |
| Agereeth\％ |  |  | $\therefore$ | $57 \%$ | 435 |  |  |  | 4\％ |  |  |  |  |  |  |  |





a 12 Locetia Tsienneto Rd-Pinkerton $5 t$

| Grewtirate |  |  |
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| Annue! | 2014-32015 | 1.625 |
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| A¢̣!ual | 2014->2015 | 1025 |
|  | 2016-32015 | 10.975 |
| Seasona |  |  |

thersection furning Movement Counts

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\text { Mray-15 } \quad \because \text { Ad Fector= } \quad 0.96
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| 2016. Raw |  |  |  | 2016-AADE |  |  |  | 2015.AAD |  |  |  | 2055-AADT- Rounded |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Aty Peak } \\ & \text { (pyosjob } \end{aligned}$ | $\begin{aligned} & \text { FM Peak } \\ & 1439.536 i 1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { AMPeck } \\ & 1730-530 \end{aligned}$ | Approzch Totols | PM Peak (5CO-ETO) | $\begin{gathered} \text { Apipead } \\ \text { Totels } \end{gathered}$ | $\begin{aligned} & \text { AM Peak } \\ & (745.345) \end{aligned}$ | Approzich Tatals | PMFeak [445.545\} | Aproan <br> Totals | $\begin{aligned} & \text { AM Peak } \\ & (745-645) \end{aligned}$ | Approach Tntals | PMPeak [ $1.2 .55-545$ ) | Approsth Toizls |
| 的 | 4 T | 17 | 42 | 16 | 752 | 41 | 1193 | 16 | 739 | 40 | 1163 | 15 | 735 | 60 | 3165 |
|  | Thru | 757 | 5175 | 735 |  | \$152 |  | 718 |  | 127 |  | 720 |  | 1125 |  |
|  | RI | 0 | 0 | 0 |  | 0 |  | 0 |  | 0 |  | 1 | : | 0 |  |
| Wib | tT | 0 | 0 | 9 | $7 \mathrm{Pb1}$ | 0 | 880 | 0 | 583 | 0 | 858 | 0 | E85 | 0 | EES |
|  | Thersi | 589 | 733 | 651 | : | 718 |  | 644 |  | 700 |  | 645 |  | 700 |  |
|  | RT | 42 | 165 | 10 |  | 162 |  | 39 |  | 158 |  | 40 |  | 150 |  |
| NE | Lt | i | b | 0 | 0 | ${ }^{\circ}$ | D | 0 | 1 | \% | 0 | 0 | 0 | 0 | 0 |
|  | Tincte | 1 | $\therefore 0$ | 0 |  | 0 |  | 0 |  | 9 |  | 0 |  | $\square$ |  |
|  | RT | B | 0 | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
| 58 | LT | 83 | 74 | 80 | 116 | 73 | 103 | 78 | 113 | 71. | 106 | 8 | 115 | 70 | 100 |
|  | Thits | $\because$ | 0 | 0 | $\cdots$ | 0 |  | 0 |  | 0 |  | 0 |  | 0 |  |
|  | ET | 37 | 31 | 36 |  | 30 |  | 35 |  | 29 |  | 35 |  | 30 |  |
|  | total | 1635 | 2220 | 1589 | 1569 | 2176 | 2276 | 1530 | 1535 | 2121 | 2121 | 1535 | 1535 | 2125 | 2125 |
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## CLD/Fuss \& O'Neill Inc.

## 540 Commercial Street

Manchester, NH 03101


| English Range RD From North |  |  |  |  |  |  | Rt 102 <br> Ftom East |  |  | From South |  |  |  |  | Kt 102 From West |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ak Hour Analys | Left | Tha | $\begin{aligned} & \text { Right } \\ & \text { to 08: } \end{aligned}$ | Peds <br> AD - | Total 10 f | Leit | Thes | Right | Peds | App Total | Lef | Thfa | Right | Peds | App Tola | Left | Thay | Right | Peds | App T Tal | In Total |
| eak Hour for Enti | Inter | ction B | ins at | :00 A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:00 AM | 4 | 0 | 23 | 0 | 27 | 0 | 121 | B | 0 | 129 | G | 0 | 0 |  |  |  |  |  |  |  |  |
| 07:15 Ab | 2 | 0 | 17 | 0 | 19 | 0 | 140 | 4 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 10 | 67 | 0 | 9 | 77 | 233 |
| 07:30 AM | 3 | 0 | 16 | 0 | 19 | 0 | 137 | 4 | 0 | 138 | 0 | 0 | 0 | 0 | 0 | 20 | 49 | 0 | 0 | 69 | 232 |
| 07:45 AM | 1 | 0 | $\therefore 19$ | 0 | 20 | 0 | 152 | 3 | 0 | 138 155 | 0 | 0 | 0 | 0 | 0 | 13 | 56 | 1 | 0 | 70 | 227 |
| Toial Volume | 10 | 6 | 75 | 0 | 85 | 0 | 550 | 16 | 0 | 565 | 0 | 0 | 0 | 0 | 0 | 11 | 49 | 0 | 0 | 60 | 235 |
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## CLD/Fuss \& O'Neill Inc.

## 540 Commercial Street

Manchester, NH 03101


## English range kD

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| $04: 30 \mathrm{PM}$ | 4 | 0 | 11 | 0 | 15 |
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| Total volume | 18 | 0 | 43 | 0 | 61 |
| \%App Total | 29.5 | $\ddots 0$ | 70.5 | 0 |  |
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## APPENDIX B: SEASONAL, ANNUAL AND AXLE CORRECTION FACTORS

Year 2015 Monthy Data
Peak Hour Data
Group 4 Averages Urban Highways:

|  | Data |  |  |  |  | Factors |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Month | AM | Mid | PM | Sat Mid | AM | Mid | PM | Sat Mid |
| Jan | 17267 | 13564 | 20154 | 15524 | 1.11 | 1.14 | Q 11 | 1.17 |
| Feb | 17366 | 13436 | 20253 | 17441 | 1.10 | 1.16 | 111 | 1.05 |
| Mar | 19827 | 14389 | 22267 | 16671 | 0.97 | 1.08 | 1.04 | 1.09 |
| Apr | 19924 | 15214 | 22733 | 18484 | 0.96 | 1.02 | 0.99 | 0.99 |
| May | 20046 | 16198 | 23476 | 18916 | 0.96 | 0.96 | 0.96 | 0.96 |
| Juri | 19952 | 16451 | 23779 | 19485 | 0.96 | 0.94 | 0.94 | 0,94 |
| Jul | 18444 | 77126 | 23314 | 18349 | 1.04 | 0.91 | 0.96 | 0.99 |
| Aug | 18720 | 16672 | 23360 | 19436 | 1.02 | 0.93 | 0.96 | 0.94 |
| Sep | 20260 | 16000 | 23092 | 19374 | 0.95 | 0.97 | 0.97 | 0.94 |
| Oct | 20391 | 15823 | 23465 | 18951 | 0.94 | 0.98 | 0.96 | 0.96 |
| Nov | 19208 | 15635 | 21905 | 17902 | 100 | 0.99 | 1.02 | 1.02 |
| Dec | 18348 | 15787 | 21589 | 18339 | 1.04 | 0.98 | 1.04 | 0.99 |
| Average | 19146 | 15525 | 22449 | 18239 |  |  |  |  |

Factors are based on Average Monih.

NHDOT Seasonal Adjustment Factors by Roadway Group - 2015


## NHDOT Axle Correction Factors

by Functional Classification - 2015

|  | AcfYear | FC | Description | Factor |
| :---: | :---: | :---: | :---: | :---: |
| Rural | 2015 | 01 |  | 0.908 |
|  | 2015 | 02 |  | 0.962 |
|  | 2015 | 06 |  | 0.967 |
|  | 2015 | 07 |  | 0.959 |
|  | 2015 | 08 |  | 0.993 |
|  | 2015 | 09 |  | 0.997 |
| Urban | 2015 | 11 | Interstate | 0.953 |
|  | 2015 | 12 | Freeways/ <br> Expressways | 0.956 |
|  | 2015 | 14 | Principle Arterals | 0.973 |
|  | 2015 | 16 | Minor Arterials | 0.981 |
|  | 2015 | 17 | Colleciors | 0.989 |
|  | 2015 | 19 | Local Streets | 0.987 |
|  | 2015 | 00 |  | 1.000 |

## APPENDIX C: INTERSTATE COUNTS AND BALANCING CALCULATIONS AT RAMP TERMINALS

## 1-93 interstate Balancing based on ATR and TMC counts - 2015 and 2016




## 2015 AWDT - Mandinine 193



2015 AWOL - Mbinline -93
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3410 | 31.87 | 785 |  | 30.1 | 458 | 769 | 3322 |
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APPENDIX D: TRAVEL DEMAND FORECAST MODEL DEVELOPMENT AND CALIBRATION REPORT - SOUTHERN NH PLANNING COMMISSION, JANUARY 2018

# Travel Demand Forecast Model Development and <br> Calibration Report for I-93 Exit 4A Supplemental Draft Environmental Impact Statement 

Prepared by the Southern NH Planning Commission and CLD/Fuss \& O'Neill


January, 2018

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## 1.INTRODUCTION

The report serves the purpose of documenting the methodology for development and calibration of the travel demand model for the update of I-93 Exit 4A SDEIS. The report includes development and calibration for the 2015 24-hour base year model, and development for 2040 No-Build 24-hour model. This report doesn't include detailed network and land use description for 2040 build scenarios, alternative A, B, C, D, E and F, because this information is included in the traffic and land use reports prepared by CLD|Fuss \& O'Neill and Louis Berger.

## 2. 2015 BASE YEAR MODEL

### 2.1 Network

The updated 2015 base year regional travel demand model was built based on the 2010 base year SNHPC regional model. The 2010 Travel Demand Forecast Model Development and Calibration Report ${ }^{[1]}$ detailed development and calibration of the 2010 model. The model covers fifteen communities: Auburn, Bedford, Candia, Chester, Deerfield, Derry, Francestown, Goffstown, Hooksett, Londonderry, Manchester, New Boston, Raymond, Weare, and Windham. The change to the functional classification system for roadway system was incorporated into the 2015 base year model due to changes to the urbanized area from the 2010 U.S. Census. In addition, projects completed between 2010 and 2015, the Manchester Airport Access Road, Pettengill Road in Londonderry, NH 28 Manchester Road improvement in Derry, Hooksett Open Road Tolling, I-93 Exit 5 reconstruction, US 3/NH 28 widening in Hooksett, I93 Exit 3 area reconstruction, were added to the 2015 model.

### 2.2 Traffic Analysis Zone (TAZ) System

The fifteen communities in the model area were disaggregated into 306 internal TAZs in the 2010 model. To better reflect traffic patterns around the I-93 Exit 4A study area, TAZs 69 in Londonderry, 123, 124, 125 and 133 in Derry were split into additional smaller TAZs indicated in Table 1. Layouts of these TAZs are displayed in Appendix A.

Table 1 TAZ Splits

| TAZ 2010 | TAZ 2015 for I-93 Exit 4A |
| :---: | :---: |
| 69 | $69 \mathrm{~A}, 69 \mathrm{~B}$ and 69C |
| 123 | 123 A and 123B |
| 124 | $124 \mathrm{~A}, 124 \mathrm{~B}$, and 124C |
| 125 | 125 A and 125B |
| 133 | 133 A and 133B |

### 2.3 Population and Households

Population estimates from 2015 Population Estimates of New Hampshire Cities and Towns prepared by the New Hampshire Office of Strategic Initiatives (NHOSI) ${ }^{[2]}$ were used for the 2015 base year model. A summary table including 2015 population estimates for communities within the model area from the NHOSI estimates is presented in Appendix D. Dwelling units collected by SNHPC annually that were issued Certification of Occupancy between 2010 and 2015 by communities were used in allocating change in population into TAZs, and calculating number of households in a TAZ.

The formula used for calculating dwelling unit increases between April 2010 (Census day on April 1) and December 31, 2015 is shown below.

$$
\left.\Delta D_{T A Z}=\Delta D_{2015 T A Z}+\Delta D_{2014 T A Z}+\Delta D_{2013 T A Z}+\Delta D_{2012 T A Z}+\Delta D_{2011 T A Z}+\frac{3}{4} \Delta D_{2010 T A Z}\right)
$$

Where:
$\Delta D_{T A Z}=$ Increase of dwelling units in a TAZ between April 1, 2010 and December 31, 2015
$\Delta D_{2015 T A Z}=$ Increase of dwelling units in a TAZ in 2015
$\Delta D_{2014 T A Z}=$ Increase of dwelling units in a TAZ in 2014
$\Delta D_{2013 T A Z}=$ Increase of dwelling units in a TAZ in 2013
$\Delta D_{2012 T A Z}=$ Increase of dwelling units in a TAZ in 2012
$\Delta D_{2011 T A Z}=$ Increase of dwelling units in a TAZ in 2011
$\Delta D_{2010 T A Z}=$ Increase of dwelling units in a TAZ in 2010
2015 dwelling units were calculated as follows:

$$
D_{2015 T A Z}=D_{2010 T A Z}+\Delta D_{T A Z}
$$

The 2015 population in TAZs were calculated by allocating the difference in population between 2010 and 2015 in a community. If the population increased during 2010-2015, the following formula was used.

Where:

$$
P_{2015 T A Z}=P_{2010 T A Z}+\left(P_{2015 c o m}-P_{2010 \mathrm{com}}\right) * \frac{\Delta D_{T A Z}}{\Delta D_{\text {com }}}
$$

$P_{2015 T A Z}=2015$ population in a TAZ
$P_{2010 T A Z}=2010$ population in a TAZ
$P_{2015 \text { com }}=2015$ population in the community (NHOEP estimates) in which the TAZ located
$P_{2010 \text { com }}=2010$ population in the community (2010 US Census) in which the TAZ located
$\Delta D_{T A Z}=$ Increase of dwelling units in a TAZ between April 1, 2010 and December 31, 2015
$\Delta D_{\text {com }}=$ Increase of dwelling units in the community in which the TAZ located between April 1, 2010 and December 31, 2015

The 2015 population in TAZs were calculated by allocating the difference of population between 2010 and 2015 in a community. If the population decreased during 2010-2015, the following formula was used.

$$
P_{2015 T A Z}=P_{2010 T A Z}+\Delta P_{D W T A Z}+\left(P_{2015 c o m}-P_{2010 c o m}-\Delta P_{D W c o m}\right) * \frac{D_{2015 T A Z}}{D_{2015 c o m}}
$$

Where:
$P_{\text {2015TAZ }}=2015$ population in a TAZ
$P_{2010 T A Z}=2010$ population in a TAZ
$P_{2015 \mathrm{com}}=2015$ population in the community (NHOEP estimates) in which the TAZ located
$\Delta P_{D W T A Z}=\frac{P_{2010 T A Z}}{H H_{2010 T A Z}} * \Delta D_{T A Z}$ - Assume population change in a TAZ due to dwelling units change between 2010 and 2015
$H H_{2010 T A Z}=2010$ number of households in a TAZ
$\Delta P_{D W c o m}=\sum \Delta P_{T A Z}$ - Assume population change in the community in which the TAZ located due to dwelling units change between 2010 and 2015
$P_{2010 \text { com }}=2010$ population in the community (2010 US Census) in which the TAZ located
$D_{2015 T A Z}=2015$ dwelling units in a TAZ
$D_{2015 \mathrm{com}}=2015$ dwelling units in the community in which the TAZ located
Number of households in a TAZ was calculated as follows.

$$
H H_{2015 T A Z}=D_{2015 T A Z} * O R_{2010 T A Z}
$$

Where:

$$
\begin{aligned}
& H H_{2015 T A Z}=2015 \text { number of households in a TAZ } \\
& D_{2015 T A Z}=2015 \text { dwelling units in a TAZ } \\
& O R_{2010 T A Z}=2010 \text { Occupancy rate in a TAZ }
\end{aligned}
$$

### 2.4 Student Enrollment

School enrollments for 2014-2015 for all elementary, middle and high schools in the region were collected from the New Hampshire Department of Education. College enrollments were collected by contacting colleges in the region.

### 2.5 Employment

The quarterly employment of 2015 for each community in the region including first, second, third and fourth quarters was downloaded from the New Hampshire Employment Security (NHES) website. A Summary table containing these data is shown in Appendix E.

The average annual employment for communities was calculated by averaging the four quarters of employment. Considering that the 2010 SNHPC employment for model input calculated directly from the employer database is slightly higher than NHES's annual average, the 2015 annual employment was adjusted to reflect the difference between the two data sets. The adjustment was made according to the following equation.

$$
E_{2015 \text { comadjusted }}=E_{2015 \text { comNHES }}+\left(E_{2010 \text { comSNHPC }}-E_{2010 \text { comNHES }}\right)
$$

Where:

$$
\begin{aligned}
& E_{2015 \text { comadjusted }}=\text { Adjusted } 2015 \text { employment in a community } \\
& E_{2015 \text { com }} \text { HES }=2015 \text { employment average in a community based on NHES data } \\
& E_{2010 \text { comNHES }}=2010 \text { employment average in a community based on NHES data } \\
& E_{2010 \text { comSNHPC }}=2015 \text { employment average in a community based on SNHPC } \\
& \text { employment database }
\end{aligned}
$$

Building permits issued 2011-2015 were used to identify new businesses in a TAZ. Employment in a new building was estimated based on a similar business type in 2010 employment database obtained from NHES. Employment in businesses we were aware closed during 2011-2015 was estimated based on the 2010 employment database.

To allocate the difference between 2010 and 2015 to TAZs by employment category, the following formula was used.

$$
\begin{aligned}
E_{2015 T A Z-E C}= & E_{2010 T A Z-E C}+\Delta E_{D W T A Z-E C}+\left(E_{A n n 2015}-E_{A n n 2010}-\Delta E_{D W 2011-2015}\right) \\
& *\left(E_{2010 T A Z-E C} / E_{A n n 2010}\right)
\end{aligned}
$$

Where:

$$
E_{2015 T A Z-E C}=2015 \text { Employment in a TAZ by employment category group }
$$

$E_{2010 T A Z-E C}=2010$ Employment in a TAZ by employment category group
$\Delta E_{D W T A Z-E C}=$ Assumed Change of Employment in a TAZ by employment category group due to number of building permits change between 2010 and 2015
$E_{\text {Ann } 2015}=2015$ Annual employment in the community in which TAZ located
$E_{\text {Ann2010 }}=2010$ Annual employment in the community in which TAZ located
$\Delta E_{D W 2011-2015}=$ Change of employment in the community due to number building permits change between 2010 and 2015

### 2.6. Base Year Model Calibration and Validation

Highway assignment is crucial for models to produce traffic volume estimates within acceptable ranges of tolerance compared to actual ground counts. For detailed model calibration and validation methodology information, refer to 2010 Travel Demand Forecast Model Development and Calibration Report for the Southern New Hampshire Planning Commission ${ }^{[1]}$. Model calibration and validation results for the 2015 base year are as follows.

- The difference of Vehicle Mile Traveled (VMT) estimates between the model and the Highway Performance Monitoring System (HPMS) is $1.28 \%$, which is acceptable according to the Model Validation and Reasonableness Checking Manual ${ }^{[3]}$, which is allowed a $3 \%$ difference by Environmental Protection Agency (EPA).
- The Coefficient of Determination $\left(\mathrm{R}^{2}\right)$ region wide equals 0.91 which is greater than the Model Validation and Reasonableness Checking Manual ${ }^{[3]}$ recommended, which is 0.88 for all roadways with functional class collector and higher. Percent Root Mean Square of the Error (\% RMSE) equals 27.28 for all roadways with functional class collector and higher which is less than the commonly accepted standard of $30{ }^{[3]}$.
- Absolute percentage differences of total observed versus model estimated volumes at a Merrimack River screen line crossing and external station cordon line crossings are less than $2 \%$.
- Absolute percentage differences of observed versus model estimated volumes at locations within I-93 Exit 4A area shown in Appendix C are within acceptable ranges of tolerance based on FHWA targets ${ }^{[3]}$.


## 3. FUTURE YEAR 2040 NO-BUILD MODEL

### 3.1 Network

2040 No-Build model network was built by adding projects documented in Regional Transportation Plan 2017-2040 for the SNHPC Region ${ }^{[6]}$ to the 2015 base year model except I-93 Exit 4A project. The list of the projects is shown in Appendix B.

### 3.2 Population and Households

Population projections used in the 2040 No-Build model were based on the State of New Hampshire County Population Projections 2015-2040 By Municipality ${ }^{[5]}$ prepared by New Hampshire Office of Strategic Initiatives (NHOSI) in partnership with the state's Regional Planning Commissions and additional adjustments to NHOSI projections were made according to the final numbers in the Land Use Scenarios Report ${ }^{[4]}$ to reflect additional population and households for relevant 2040 No-Build development projects. The population projections from 2015 through 2040 for each community in the region from the NHOSI projections are presented in Appendix D.

Due to the fact that numbers of dwelling units changes in five-year increments was used in distributing population changes to TAZs, and calculating numbers of households in a TAZ, SNHPC dwelling unit projections for 2010 through 2040 (Completed 2012) were adjusted for 2020 through 2040 to reflect number of dwelling units change between 2010 and 2015. An assumption was made that numbers of dwelling unit growth rates 2015-2040 were kept the same as the 2012 Southern NH Planning Commission dwelling unit projection for 2010-2040, which were reviewed by corresponding communities in the region. Two conditions were considered as the population was allocated to TAZs: 1) population increase in a five-year period; 2) Population decrease in a five-year period.

## Condition one

When the population increases during a five-year period, the allocation is calculated using the following formula.

$$
\Delta \boldsymbol{P}_{T A Z}=\frac{\Delta \boldsymbol{P}_{\text {com }}}{\Delta \boldsymbol{D}_{\text {com }}} * \Delta \boldsymbol{D}_{T A Z}
$$

Where:
$\Delta P_{T A Z}=$ population change in a TAZ during a five-year period
$\Delta P_{\text {com }}=$ Population change in the community in which the TAZ located during the five-year period
$\Delta D_{T A Z}=$ Number of dwelling units change in a TAZ during the five-year period
$\Delta D_{\text {com }}=$ Number of dwelling units change in the community in which the TAZ located during the five-year period

## Condition two

When the population decreases during a five-year period, the allocation is calculated using the following formula.

$$
\Delta \boldsymbol{P}_{T A Z}=\Delta \boldsymbol{P}_{D W T A Z}+\left(\Delta \boldsymbol{P}_{\text {com }}-\Delta \boldsymbol{P}_{\text {DWcom }}\right) * \frac{\boldsymbol{D}_{T A Z}}{\boldsymbol{D}_{\text {com }}}
$$

Where:
$\Delta P_{T A Z}=$ Population change in a TAZ during a five-year period
$\Delta P_{D W T A Z}=H H S_{2015 T A Z} * \Delta D_{T A Z}=$ Assume population change in a TAZ during a five-year period due to number of dwelling units change
$H H S_{2015 T A Z}=2015$ household size within the TAZ
$\Delta P_{\text {com }}=$ Change of population in the community in which the TAZ located during the 5-year period
$\Delta P_{d w c o m}=\sum \Delta P_{d w T A Z}=$ Population change in the community in which the TAZ located during the five-year period due to number of dwelling units change
$D_{T A Z}=$ Number of dwelling units in the TAZ at the end of the five-year period

$$
D_{c o m}
$$

= Number of dwelling units in the cummunity in which the TAZ located at end of the five - year period

Population within a TAZ at end of a five-year period was calculated as follows.

$$
\boldsymbol{P}_{T A Z}=\boldsymbol{P}_{T A Z-1}+\Delta \boldsymbol{P}_{T A Z}
$$

Where:
$\mathrm{P}_{\mathrm{TAZ}}=$ Population in the TAZ at end of the five-year period
$\mathrm{P}_{\mathrm{TAZ}-1}=$ Population in the TAZ at end of the prior five-year period

## Number of Households Calculation

Numbers of households for TAZs were calculated using the following formula.

$$
\boldsymbol{H H}_{T A Z}=\left(\boldsymbol{P}_{T A Z}-\boldsymbol{P}_{\text {specialTAZ }}\right) / \boldsymbol{H} \boldsymbol{H} S_{2015}
$$

Where:

$$
H H_{T A Z}=\text { Number of households in a TAZ }
$$

$$
P_{\text {specialtaz }}=\text { Special population such population in nursing homes, jails, etc. in the }
$$

TAZ

$$
H H S_{2015 T A Z}=\text { Household size in the TAZ }
$$

### 3.3 Employment

In order to reflect changes in employment between 2010 and 2015, the original SNHPC employment projection for 2010 through 2040 (completed in 2012) was adjusted for 2020 through 2040. Three steps are followed in calculating the 2015-2040 employment projection. Additional adjustments were made to the final numbers based on the Land Use Scenarios Report ${ }^{[4]}$ to account for additional employment for relevant 2040 No-Build development projects.

## Step 1: Growth rates

The study assumes that employment growth rates by employment category group for 2015-2040 were kept the same as the 2012 Southern NH Planning Commission employment projection for 2010-2040, which were reviewed by corresponding communities in the region. The following formula was used in calculating growth rates over a five-year interval.

$$
G R_{\text {Com EC } i}=\left(E_{2012 \text { Com EC } i}-E_{2012 \text { Com EC } i-1}\right) / E_{2012 \text { Com EC } i-1}
$$

Where:


Step 2: Total employment projection for an employment category group in a community 2020 through 2040

The 2015 total employment estimate for an employment category group in a community was considered as base. Total employment projections for the employment category group in the community 2020 through 2040 were calculated as follows:

$$
E_{2016 \text { Com EC } i}=E_{2016 \text { Com EC } i-1} *\left(1+G R_{\text {Com EC } i}\right)
$$

Where:
$i$ = projection years 2020,2025,2030,2035 and 2040
$E_{2016 \operatorname{comeC} i}=$ Total employment for an employment category group in the community at projection year i in the 2016 projection
$E_{2016 \text { com EC i-1 }}=$ Total employment for the employment category group in the community at projection year i-1 in the 2016 projection

Step 3: Total employment for an employment category group in the community for 2020-2040 projection distributed to TAZs

Two conditions were used as total projected employment for an employment category group in the community was allocated into TAZs.

## Condition one

When the data for developable land for a land use category is available and appropriate to use in a community, employment is distributed based on percentage of developable land in a TAZ in total of developable land in the community.

$$
E_{2016 T A Z E C i}=E_{2016 T A Z E C i-1}+\left(E_{2016 \text { Com EC } i}-E_{2016 \text { Com EC } i-1}\right) * \text { Percentage }
$$

Where:
$E_{2016 \text { TAZ EC } i}=2016$ Employment projection in a TAZ for an employment category group at projection year i
 projection year i-1 in the 2016 projection
$E_{2016 \text { com EC } i}=$ Total employment for the employment category group in the community at projection year i in the 2016 projection
$E_{2016 \text { com EC } \text { i-1 }^{\prime}}=$ Total employment for the employment category group in the community at projection year i-1 in the 2016 projection

## Condition two

When the data for developable land for the land use category is not available or not appropriate to use in a community, employment in a TAZ is calculated using the same growth rate as that of employment of the employment category.

$$
E_{2016 T A Z E C ~} i=E_{2016 \text { TAZ EC } i-1} *\left(1+G R_{2016 \text { Com EC } i}\right)
$$

Where:
$E_{2016 \text { TAZ EC } i}=2016$ Employment projection in a TAZ for an employment category group at projection year i
$E_{2016 \text { TAZ EC i-1 }}=2016$ Employment projection in a TAZ for the employment category group at projection year i-1 in the 2016 projection


## 4. REFERENCES

1. 2010 Travel Demand Forecast Model Development and Calibration Report, Southern New Hampshire Planning Commission, 2012.
2. 2015 Population Estimates of New Hampshire Cities and Towns, The New Hampshire Office of Strategic Initiatives (NHOSI), 2016.
3. Model Validation and Reasonableness Checking Manual, Travel Model Improvement Program, 2001.
4. I-93 Exit 4A Supplemental Draft Environmental Impact Statement Land Use Scenarios Report, Louis Berger, 2017.
5. State of New Hampshire County Population Projections, By Municipality, The New Hampshire Office of Strategic Initiatives (NHOSI) in Partnership with the State's Regional Planning Commissions, 2016
6. FY 2017 - FY 2040 Regional Transportation Plan for the Southern NH Planning Commission, Southern New Hampshire Planning Commission, 2017.

## APPENDIX A STUDY AREA TAZ SPLIT









Projects Coded in the 2040 No-Build Model

| Community ${ }^{1}$ | Project | Project \# |
| :---: | :---: | :---: |
| BE | NH 101 - Widen NH 101 to 5 Lanes from NH 114 up to Wallace Rd | 13953 |
| BE | NH 101 - Widen NH 101 to 5 Lanes from Wallace Rd up to Amherst TL ${ }^{2}$ |  |
| BE | US 3 - Widen US 3 to 5 Lanes from Hawthorne Drive North to Manchester Airport Access Road | 40664 |
| BE-ME | F.E.E Turnpike - Improvement to Bedford Mainline Toll Plaza to Institute Open Road Tolling | 16100 |
| NA-ME-BE | F.E.E.Turnpike - Widen existing 2-Lane Sections of the Turnpike to a 3-Lane Typical From Exit 8 in Nashua to I-293 in Bedford | 13761 |
| CH | NH 102 - NH 102/North Pond Road Intersection Improvements. |  |
| DE-LO | I-93-Construction of I-93 Exit 4A | 13065 |
| HO | US 3/NH 28 - Widen US 3/NH 28 to 5 Lanes from Martins Ferry Rd to West Alice Ave | 29611 |
| HO | US 3/NH 28 - Construct Southern Segment of US 3/NH 28 Alternate Bypass ${ }^{2}$ |  |
| HO | US 3/NH 28 - Construct Northern Segment of US3/NH28 Alternate Bypass ${ }^{2}$ |  |
| HO | Widen US3/NH28 to 5 Lanes from Legends Dr to Hunt Street ${ }^{2}$ |  |
| HO | Hackett Hill Road - Reconstruction intersection of NH 3A/Hackett Hill Road | 14950 |
| HO | NH 3A - Reconstruct and Widen from Commerce Road North to Goonan Rd. | 24862 |
| LO | NH 28 - Widening NH 28 from NH 128 to Page Rd. |  |
| LO | NH 102 - Widen NH 102 to 4 Lanes from Hudson Town Line to NH $128^{2}$ - Lower Corridor |  |
| LO | NH 102 - Widen NH 102 to 5 Lanes from I-93 East to Londonderry Road ${ }^{2}$ - Upper Corridor |  |
| LO | NH 102 - Widen NH 102 to 6 Lanes from I-93 to NH $128^{2}$ - Central Corridor |  |
| LO | Intersection Improvements at NH28/NH128 for Safety and Traffic Flow |  |
| MA | I-293 - Reconstruction of Exit 4 on I-293 |  |
| MA | I-293-Reconstruct and Widening of Exit 6 (Amoskeag) | 16099A |
| MA | I-293-Reconstruct Exit 7 | 16099B |
| SA-MA | I-93- Reconstruct and Widen Mainline, Environmental Impact Study and Final Design From Mass S/L in Salem to I-293 in Manchester. Capacity Improvements, Reconstruction, and Widening from North of Exit 3 to I-293 | 10418C |
| SA-MA | I-93 - NB \& SB Mainline Weigh Station to Kendall | 14633B |
| SA-MA | I-93 - Exit 4 Ramps, NB \& SB Mainline, NH 102 Approach Work | 14633D |
| SA-MA | I-93- NB \& SB Mainline, Exit 5 to I-293 Split (Londonderry \& Manchester) | 14633H |
| SA-MA | I-93- NB \& SB Mainline, Exit 4 and 5 (Londonderry) | 14633I |
| SA-MA | I-93-Exit 1 to Exit 5 - Construct 4th Lane Northbound and Southbound | 14633J |
| SA-MA | I-93 - Final Design (PE) and ROW for I-93 Salem to Manchester | 10418X |
| Windham | NH 111 - Corridor Improvements Within Town Center (Construction not in TYP) | 40663 |
| Windham | NH 28 - Intersection NH 28/Roulston Road Improvements | 40665 |

Source: FY 2017-2020 Transportation Improvement Program, FY 2017-2026 Ten-Year Transportation Improvement Plan, and 2017-2040 SNHPC Regional Transportation Plan.
${ }^{1}$ BE=Bedford, $\mathrm{CH}=$ Chester, $\mathrm{DE}=$ Derry, $\mathrm{HO}=$ Hooksett, LO=Londonderry, MA=Manchester, NB=New Boston, RA=Raymond, SA=Salem, NA=Nashua
${ }^{2}$ These projects are taken from various studies and are part of the Regional Transportation Plan

Updated 10/21/2016

APPENDIX C 2015 BASE YEAR MODEL STUDY AREA CALIBRATION RESULTS

# 2015 Base Year Model Study Area Calibration Results 

| Location | A | B | Assign | Count | \% Diff |
| :--- | ---: | ---: | ---: | ---: | ---: |
| NH 28 N. of Liberty Dr. | 589 | 3645 | 15,406 | 13,000 | 18.51 |
| NH 102 at Derry Town line | 594 | 3556 | 20,817 | 22,270 | -6.52 |
| NH 28 at Derry Town line | 793 | 1621 | 19,392 | 17,454 | 11.10 |
| Exit 5 SB Off ramp | 999 | 3650 | 9,234 | 9,282 | -0.52 |
| Exit 4 SB On ramp | 1003 | 1764 | 8,157 | 9,615 | -15.16 |
| Exit 4 NB Off ramp | 1006 | 6519 | 10,389 | 9,843 | 5.55 |
| Exit 5 NB Off ramp | 1010 | 3652 | 4,430 | 5,601 | -20.91 |
| Gilcreast Rd. N. of NH 102 | 1334 | 3557 | 9,397 | 10,000 | -6.03 |
| Ash St. E. of Londonderry Rd. | 1348 | 3555 | 5,950 | 6,900 | -13.77 |
| Ash St. at Londonderry Town line | 1349 | 2125 | 5,936 | 6,765 | -12.25 |
| Exit 4 SB On ramp EB to SB | 1767 | 1005 | 4,907 | 5,010 | -2.06 |
| Exit 4 SB On ramp WB to SB | 1770 | 1004 | 3,637 | 4,648 | -21.75 |
| NH28 Bypass N. of Tsienneto Rd. | 1838 | 1839 | 9,377 | 11,943 | -21.49 |
| NH28 Bypass N. of Academy Dr. | 1839 | 3532 | 7,318 | 7,329 | -0.15 |
| NH28 Bypass S. of Thornton Rd. | 1840 | 2143 | 12,015 | 13,981 | -14.06 |
| NH102 E. of NH 28 Bypass | 1841 | 1878 | 7,017 | 7,329 | -4.26 |
| Crystal Ave. NH 28 S of Rollins | 1860 | 1861 | 13,215 | 13,000 | 1.65 |
| Crystal Ave. NH 28 S of Tsienneto | 1862 | 1863 | 13,407 | 15,193 | -11.76 |
| Folsom Rd. W. of NH 28 | 1863 | 3483 | 8,960 | 11,672 | -23.24 |
| NH 102 E. of Griffin St. | 1870 | 1871 | 18,002 | 16,400 | 9.77 |
| NH 102 W. of Abbot St. | 1876 | 1877 | 11,128 | 14,350 | -22.45 |
| Tsienneto Rd. W. of NH 102 | 1883 | 2082 | 5,666 | 5,393 | 5.06 |
| Franklin St. Ext N. of Folsom Rd. | 2106 | 3484 | 1,255 | 1,845 | -31.98 |
| Tsienneto Rd. E. of Pinkerton | 2107 | 2108 | 14,200 | 14,636 | -2.98 |
| Pinkerton St. E. of Tsienneto | 2107 | 2109 | 8,776 | 11,672 | -24.81 |
| Fordway over Beaver Brook | 2135 | 2136 | 5,114 | 5,330 | -4.05 |
| NH102 E. of Hampton Dr. | 3234 | 1766 | 30,419 | 32,000 | -4.94 |
| Exit 5 NB On ramp | 3651 | 1011 | 9,101 | 9,341 | -2.57 |
| Exit 5 SB On ramp | 3653 | 1000 | 3,919 | 5,503 | -28.78 |
| Exit 4 NB On ramp | 6518 | 1007 | 9,550 | 10,045 | -4.93 |

FHWA Targets

| Upper Limit Lower Limit |  |
| :---: | ---: |
| 25 | -25 |
| 25 | -25 |
| 25 | -25 |
| 29 | -29 |
| 29 | -29 |
| 29 | -29 |
| 29 | -29 |
| 25 | -25 |
| 29 | -29 |
| 29 | -29 |
| 29 | -29 |
| 36 | -36 |
| 25 | -25 |
| 29 | -29 |
| 25 | -25 |
| 29 | -29 |
| 25 | -25 |
| 25 | -25 |
| 25 | -25 |
| 25 | -25 |
| 25 | -25 |
| 29 | -29 |
| 47 | -47 |
| 25 | -25 |
| 25 | -25 |
| 29 | -29 |
| 22 | -22 |
| 29 | -29 |
| 29 | -29 |
| 25 | -25 |
|  |  |
| 25 |  |

Note: Traffic volumes were taken from NHDOT traffic count program, SNHPC traffic count program, and CLD|Fuss \& O'Neil traffic counts for the project.

# APPENDIX D POPULATION PROJECTION ${ }^{[2][5]}$ 



Population Projection 2015-2040

| Town | $\mathbf{2 0 1 5}$ | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 2 5}$ | $\mathbf{2 0 3 0}$ | $\mathbf{2 0 3 5}$ | $\mathbf{2 0 4 0}$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Auburn | 5,315 | 5,560 | 5,828 | 5,959 | 6,033 | 6,048 |
| Bedford | 22,236 | 23,451 | 24,797 | 25,276 | 25,576 | 25,680 |
| Candia | 3,909 | 3,891 | 3,880 | 3,967 | 4,016 | 4,026 |
| Chester | 4,887 | 5,199 | 5,536 | 5,660 | 5,731 | 5,744 |
| Deerfield | 4,413 | 4,631 | 4,869 | 4,978 | 5,040 | 5,052 |
| Derry | 32,948 | 32,459 | 32,018 | 32,733 | 33,144 | 33,222 |
| Francestown | 1,562 | 1,576 | 1,597 | 1,628 | 1,647 | 1,654 |
| Goffstown | 17,846 | 18,051 | 18,335 | 18,689 | 18,911 | 18,988 |
| Hooksett | 14,473 | 15,403 | 16,508 | 17,089 | 17,532 | 17,823 |
| Londonderry | 24,891 | 25,434 | 26,057 | 26,639 | 26,973 | 27,036 |
| Manchester | 109,419 | 109,469 | 109,963 | 112,087 | 113,420 | 113,881 |
| New Boston | 5,457 | 5,818 | 6,214 | 6,334 | 6,409 | 6,435 |
| Raymond | 10,257 | 10,403 | 10,577 | 10,814 | 10,949 | 10,975 |
| Weare | 8,811 | 9,051 | 9,334 | 9,514 | 9,627 | 9,667 |
| Windham | 14,301 | 15,414 | 16,612 | 16,983 | 17,196 | 17,237 |
| Total | $\mathbf{2 8 0 , 7 2 5}$ | $\mathbf{2 8 5 , 8 1 0}$ | $\mathbf{2 9 2 , 1 2 5}$ | $\mathbf{2 9 8 , 3 5 0}$ | $\mathbf{3 0 2 , 2 0 4}$ | $\mathbf{3 0 3 , 4 6 8}$ |

Source: $\quad$ New Hampshire Office of Strategic Initiatives.

# APPENDIX E 2015 EMPLOYMENT AVERAGE 

2015 Employment Average

| Town | Q1 | Q2 | Q3 | Q4 | Average |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Auburn | 1,706 | 1,766 | 1,806 | 1,852 | 1,783 |
| Bedford | 15,223 | 15,487 | 15,446 | 15,617 | 15,443 |
| Candia | 673 | 820 | 865 | 818 | 794 |
| Chester | 364 | 371 | 349 | 376 | 365 |
| Deerfield | 384 | 454 | 437 | 411 | 422 |
| Derry | 8,123 | 8,240 | 7,806 | 8,251 | 8,105 |
| Francestown | 94 | 125 | 136 | 117 | 118 |
| Goffstown | 3,129 | 3,304 | 3,159 | 3,235 | 3,207 |
| Hooksett | 9,275 | 9,496 | 9,591 | 9,700 | 9,516 |
| Londonderry | 12,812 | 13,345 | 13,185 | 13,454 | 13,199 |
| Manchester | 67,548 | 68,384 | 68,349 | 69,812 | 68,523 |
| New Boston | 727 | 756 | 732 | 794 | 752 |
| Raymond | 2,965 | 3,051 | 2,902 | 3,074 | 2,998 |
| Weare | 1,764 | 1,852 | 1,762 | 1,836 | 1,804 |
| Windham | 3,428 | 3,534 | 3,463 | 3,689 | 3,529 |

Source: New Hampshire Department of Employment Security.

## APPENDIX E: HCM 2010 LOS CRITERIA

# HCM2010 HIGHWAY CAPACITY MANUAL 



## VDLUME 3: INTERRUPTED FLDW

URED TRANSPORTATION RESEARCH BOARD
OF THE NATIONAL ACADEMIES

WASHINGTGN, DE I WWW TAF, OFE





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## LOS: COMPONENT SEGMENTS AND THE FREEWAY FACILITY

## LOS of Component Segments

Chapters 11, 12, and 13 provide methotologes to determine the IOS in

 are peferme thens chaper.


 when the segmen io/cis greater than lind and (b) when a ghe from a kownstrean breahdownexterdsinto an upstrem stement. The hater carnot be
 mot 13.

 ways:

- When efsistmater than 1 on os
 or $43 \mathrm{pofm} / \mathrm{h}$ torweaving merge or tiverge segments.
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## LOS for a Freeway Facility


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 compoment segment. The facilty los will be beres on the weighted averge

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\begin{aligned}
& \sum 1 \\
& \sum 1
\end{aligned}
$$

Equation 10.2
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| Level of Service | Density (pc/mi/ln) |
| :---: | :---: |
| A | $\leq 11$ |
| B | P11-18 |
| C | $>18-25$ |
| 0 | >26-35 |
| E | - $35 \times 45$ |
| F | 245 or |
|  | caponeft 4 icatio $>1.00$ |









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 (blay



 13645ms.

Exhibit 10-7
tos Crter for formy fations

1s-3. The symbol whown in thisexhbit represens the wort tophase" whe the number Tolowing the symbet reperants the phase number.

Exhbit $10-3$ shows ont woty that thatic movements an be assigned to gach of the eight phases. These assigmments are illustrolive, but they are not uncommon. Each hefteturn monement is asigned to an exelusive phase During this phase, the teft-timn movement "protected" so that it rectives a green armot molicalion. Each though, right-turn, and pedestrion movement ombination is also assifged to an exclusive phane. The dashed arows indionte tum movements that areserved in a "permitted". manner so that the tum can be compheted onfy after yielding the rightot-way to conticting movements. Additional information about traflic signal controler opuration is provided in Chapter 3L, Signalized Intasections: Supplemental.


## LOS CRITERYA

This subsection describes the LOS criteria for the automobile pedestrian, and bicycle modes. The criteria for the automobile mode are different from those for the nonatomobite modes, Specifatly, the autumobile-mode criteria are based on performance measures that are field measurable and perceivable by travelers. The criteria for the nonatumobils modes are based on scores reported by travelers indicating their perception of service quatity

## Automobile Mode

TOS can be characterized for the matim intersedion, ench intersection appoach, and each hone group. Control deloy ahone is used to characterize LOS for the entire intersction or an approadf, Control delay and volume to copacity Falio are used to characterize 10 for a hane group. Detay quantifes the incrase in trovel time due to traffic sigmal controh. It is also a surrogate measure of driver tisomfort and fuef consumption. The whume-to-gacity ratio quantifies the degree to which a phase's capacity is ullized by a bne gromp The following paragrophs describesen LOS.

LOS A describes operations with a control delay th $10 \mathrm{~s} / \mathrm{yeh}$ or less and a volumerto-capacity ratio no freater than 10 . This levet is typhally assigned when the voltme-th-apacily ration how and either progression is exceptomaly

Exhibit 18-3
Dual-Ring Structure with Hustative Movement Assignmants

Alt uses of the word "volumes" of the phrase "valume-io-gapacity ratio" in this chapter refer to demand volume of demond volume to caparity rotio.

















 moticowbe.









A hate group can incur a delay hes than st sheth when the whme-to-






 a signafine materserthon.

| Control Delay ( $5 / \mathrm{veh}$ ) | LOS by Volume-to Capacity Ratio? |  |
| :---: | :---: | :---: |
| $\leq 10$ | A. | F |
| $\therefore>10-20$ | B | $F$ |
| >20-35 | C | $F$ |
| > $35 \times 5$ | D | $F$ |
| >55-80 | E | F |
| $>80$ | F | F |



## 1. INTRODUCTION









 Ang for TWSC intersedions.
 underatanting of the interaction butween fovelers on the minor, of stan-

 Wherbed in this thapter rety promaty on hed measumment of TWSC.
 muded fretoped and retmed in Germany (2).

## INTERSECTION ANALYSIS BOUNDARIES AND TRAVEL MODES


 fotersethans, with the exception of TWSC intersetions that are homed within





## LEVEL-OF-SERVICE CRITERIA














The los criterin for TVSC interections are sonewnot diferent trom the




## 19. TWSC Intersections

Thre-ting intersextons anc considered a standard type of THEC mersection, when the stem of the $J$ is controlted by a moy sigh

105 ss no tether for the major. street approdhes or for the overatf introrsection, as major-strect though wehicles ate assumed to Expuriepae no ditas.

Exhibit 19-1
Lever of Servie Criteria:
Autonobile Mote

Exthibit 19-2
Level-of-Service Criteria:
Pegestrian Mode




| Control Delay | LoS by Volume-to-Capacity Ratio |  |
| :---: | :---: | :---: |
| (s/vehicte) | $v / c \leq 1.0$ | $v / C>1.0$ |
| Q-10 | A | $F$ |
| $\bigcirc 10-15$ | 8 | F |
| >15-25 | $c$ | f |
| 25-35. | D | F |
| -35-50 | E | F |
| $>50$ | F | F |







| Los | Control Detay (s/pedestrian) | Comments |
| :---: | :---: | :---: |
| A | 0-5 | Usuaty no monficting traffic |
| B | 5-10 | Occasionally sorse delay due to contlicting traffic |
| C | 10 m 20 | Delay noticeabte to pedestrians, but not inconveniencing |
| D | 29-30 | Defay noticebte and is ritating, increased thelithod of risk taking |
| E | 30-45 | Delay approaches toderance teved, risk-taking betavior likely |
| F | $>45$ | Delay exceeds tolerance tevel, high ifetihood of pedestran risk taking |




LOS For petestrims whes when there ate not condeh gaps of subable sive






## REQUIRED INPUT DATA




3. Whar wif the following



 Fownother for host


 storage (ar both),

## 1. INTRODUCTION






Chapter 21, Roundabouts, presents comeptemd procedmestor andyang


 hargely fonded on that staty's reommembtions. These prowedures allow the Amaly to assess the operational perfomano of an existing or plamed westane or two-hme roundabont given maffe demand levels.

## INTERSECTION ANALYSIS BOUNDARIES AND TRAVEL MODES

The andytical procedure presented in thes chapter assumes that the analysis bombtariss are the roundabout itself, inchathg asociated pedestran crusswalks. Alternatice touls discussed in this chapter can, in some coses, expond the analysis boundaries to inchate adpaent intersections. The methodology prosented here includes discussion of motor vehicter, podestrians, ant beycles.

## LEVEL OF SERVICE CRITERIA

The level of service (LOS) eriteria for atombbiles in romdabouts are given In Exhbit 21-1. As the table motes, LOS 年 is assigned th the volume-to-copacity ratio of a bane exceds 1.0 regandess of the controldeday. For assessment of 105 at the approath and intersection levels, LOS is based solely on control detay,

The thesholds in Exhibit $21-1$ are based on the considered judgment or the Tansporlation Reseach Board Commilew on Hohway Capacily and Qually of Service. As discussed hater in this chapler, romedabots share the same basis: control deday formetation with wo-way and all-way sur-controlled

 Was avabobe on traveler perteption of ghatity of service at retindatombs It the
 comsistent with those tor other magnalized intersectens, primarily on the basts of this siminar control day formutation.

| Control Delay | 105 by Volume-to-Capacity Ratio ${ }^{*}$ |  |
| :---: | :---: | :---: |
| (s/ven) | $v / c \leq 1.0$ | $v / c>2.0$ |
| 0-10 | A | F |
| $>10-15$ | B | F |
| >15-25 | C | F |
| >25-35. | D | $F$ |
| >35-50 | E | F |
| $\bigcirc 50$ | F | F |





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21. Roundabouts
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Exhibit 21-1
LOS Criteria: Attomoble Mode

## APPENDIX F: HCS 2010 FREEWAY FACILITY ANALYSES - 2015 BASE

## Segment Identification Listing

## Northbound Direction

Segment 1 - Basic - I-93 Mainline south of Exit 4
Segment 2 - Diverge - Exit 4 NB off-ramp
Segment 3 - Basic - I-93 Mainline between Exit 4 ramps
Segment 4 - Merge - Exit 4 NB on-ramp
Segment 5 - Basic - I-93 Mainline between Exit 4 NB on- and Exit 5 NB offramps
Segment 6 - Diverge - Exit 5 NB off-ramp
Segment 7 - Basic - I-93 Mainline between Exit 5 ramps
Segment 8 - Merge - Exit 5 NB on-ramp
Segment 9 - Basic - I-93 Mainline north of Exit 5

## Southbound Direction

Segment 1 - Basic - I-93 Mainline north of Exit 5
Segment 2 - Diverge - Exit 5 SB off-ramp
Segment 3 - Basic - I-93 Mainline between Exit 5 ramps
Segment 4 - Merge - Exit 5 SB on-ramp
Segment 5 - Basic - I-93 Mainline between Exit 5 SB on- and Exit 4 SB off-ramps
Segment 6 - Diverge - Exit 4 SB off-ramp
Segment 7 - Basic - I-93 Mainline between Exit 4 SB off- and SB on ramp from east
Segment 8 - Merge - Exit 4 SB on-ramp from east
Segment 9 - Basic - I-93 Mainline between Exit 4 SB on-ramps
Segment 10 - Merge - Exit 4 SB on-ramp from west
Segment 11 - Basic - I-93 Mainline south of Exit 4

## HCS 2010 Facilities Report

## Project Information

| Analyst | PK/LCG | Agency |  |
| :--- | :--- | :--- | :--- |
| Jurisdiction |  | Time Period Analyzed | AM Peak - NB |
| Analysis Year | 2015 Base - AM | Date | $5 / 1 / 2017$ |
| Project Description | I-93 - from S. of Exit 4 to N of Exit S |  |  |

Facility Global Input

| Jam Density, pc/mi/ln | 190.0 | Density at Capacity, pc/mi/ln | 45.0 |
| :--- | :--- | :--- | :--- |
| Queue Discharge Capacity Drop, \% | 7 | Total Segments | 9 |
| Total Time Periods | 4 | Time Period Duration, min | 15 |

Segment Geometric Data

| No. | Coded | Analyzed | Name | Length, ft | Lanes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Basic | Basic | $a->b$ | 5280 | 2 |
| 2 | Diverge | Diverge | b.->c | 1500 | 2 |
| 3 | Basic | Basic | $c->d$ | 2575 | 2 |
| 4 | Merge | Merge | d->e | 1500 | 2 |
| 5 | Basic | Basic | e->f | 13225 | 2 |
| 6 | Diverge | Diverge | $f \rightarrow \mathrm{~g}$ | 1500 | 2 |
| 7 | Basic | Basic | $g->h$ | 4100 | 2 |
| 8 | Merge | Merge | $h->i$ | 1500 | 2 |
| 9 | Basic | Basic | i->j | 5280 | 2 |

## Facility Segment Data

| Segment 1: Basic |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| 1 | 1.00 |  | 0.979 |  | 2022 |  | 4700 |  | 0.43 |  | 65.0 |  | 15.6 |  | B |
| 2 | 1.00 |  | 0.979 |  | 2022 |  | 4700 |  | 0.43 |  | 65.0 |  | 15.6 |  | B |
| 3 | 1.00 |  | 0.979 |  | 2022 |  | 4700 |  | 0.43 |  | 65.0 |  | 15.6 |  | B |
| 4 | 1.00 |  | 0.979 |  | 2022 |  | 4700 |  | 0.43 |  | 65.0 |  | 15.6 |  | 8 |
| Segment 2: Diverge |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.979 | 0.962 | 2022 | 426 | 4700 | 1900 | 0.43 | 0.22 | 51.3 | 51.3 | 19.7 | 14.3 | B |
| 2 | 1.00 | 1.00 | 0.979 | 0.962 | 2022 | 426 | 4700 | 1900 | 0.43 | 0.22 | 51.3 | 51.3 | 19.7 | 14.3 | B |
| 3 | 1.00 | 1.00 | 0.979 | 0.962 | 2022 | 426 | 4700 | 1900 | 0.43 | 0.22 | 51.3 | 51.3 | 19.7 | 14.3 | B |
| 4 | 1.00 | 1.00 | 0.979 | 0.962 | 2022 | 426 | 4700 | 1900 | 0.43 | 0.22 | 51.3 | 51.3 | 19.7 | 14.3 | 8 |

## Segment 3: Basic

| Time Period | PHF | fHV | Flow Rate (pc/h) | Capacity (pc/h) | d/c <br> Ratio | Speed ( $\mathrm{mi} / \mathrm{h}$ ) | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.984 | 1596 | 4700 | 0.34 | 65.0 | 12.3 | B |
| 2 | 1.00 | 0.984 | 1596 | 4700 | 0.34 | 65.0 | 12.3 | B |
| 3 | 1.00 | 0.984 | 1596 | 4700 | 0.34 | 65.0 | 12.3 | B |
| 4 | 1.00 | 0.984 | 1596 | 4700 | 0.34 | 65.0 | 12.3 | 8 |

## Segment 4: Merge

| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | $F$ | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.973 | 0.984 | 2691 | 1077 | 4700 | 2100 | 0.57 | 0.51 | 59.2 | 59.2 | 22.7 | 17.2 | B |
| 2 | 1.00 | 1.00 | 0.973 | 0.984 | 2691 | 1077 | 4700 | 2100 | 0.57 | 0.51 | 59.2 | 59.2 | 22.7 | 17.2 | B |
| 3 | 1.00 | 1.00 | 0.973 | 0.984 | 2691 | 1077 | 4700 | 2100 | 0.57 | 0.51 | 59.2 | 59.2 | 22.7 | 17.2 | B |
| 4 | 1.00 | 1.00 | 0.973 | 0.984 | 2691 | 1077 | 4700 | 2100 | 0.57 | 0.51 | 59.2 | 59.2 | 22.7 | 17.2 | 8 |

## Segment 5: Basic

| Time Period | PHF | fHV | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) | d/c <br> Ratio | Speed (mi/h) | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.973 | 2703 | 4700 | 0.58 | 65.0 | 20.8 | C |
| 2 | 1.00 | 0.973 | 2703 | 4700 | 0.58 | 65.0 | 20.8 | C |
| 3 | 1.00 | 0.973 | 2703 | 4700 | 0.58 | 65.0 | 20.8 | C |
| 4 | 1.00 | 0.973 | 2703 | 4700 | 0.58 | 65.0 | 20.8 | C |

Segment 6: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | $F$ | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.973 | 0.957 | 2703 | 428 | 4700 | 2000 | 0.58 | 0.21 | 54.3 | 54.3 | 24.9 | 23.2 | C |
| 2 | 1.00 | 1.00 | 0.973 | 0.957 | 2703 | 428 | 4700 | 2000 | 0.58 | 0.21 | 54.3 | 54.3 | 24.9 | 23.2 | C |
| 3 | 1.00 | 1.00 | 0.973 | 0.957 | 2703 | 428 | 4700 | 2000 | 0.58 | 0.21 | 54.3 | 54.3 | 24.9 | 23.2 | C |
| 4 | 1.00 | 1.00 | 0.973 | 0.957 | 2703 | 428 | 4700 | 2000 | 0.58 | 0.21 | 54.3 | 54.3 | 24.9 | 23.2 | C |

Segment 7: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> ( $\mathbf{p c / h}$ ) | Capacity <br> ( $\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> (pc/mi/ln) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.976 | 2275 | 4700 | 0.48 | 65.0 | 17.5 |  |
| 2 | 1.00 | 0.976 | 2275 | 4700 | 0.48 | 65.0 | 17.5 | B |
| 3 | 1.00 | 0.976 | 2275 | 4700 | 0.48 | 65.0 | 8 |  |
| 4 | 1.00 | 0.976 | 2275 | 4700 | 0.48 | 65.0 | 17.5 | 17.5 |

Segment 8: Merge

| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity (pc/h) |  | d/c Ratio |  | Speed ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.983 | 0.971 | 3267 | 1009 | 4700 | 2100 | 0.70 | 0.48 | 56.8 | 56.8 | 28.8 | 25.8 | C |
| 2 | 1.00 | 1.00 | 0.983 | 0.971 | 3267 | 1009 | 4700 | 2100 | 0.70 | 0.48 | 56.8 | 56.8 | 28.8 | 25.8 | c |


| 3 | 1.00 | 1.00 | 0.983 | 0.971 | 3267 | 1009 | 4700 | 2100 | 0.70 | 0.48 | 56.8 | 56.8 | 28.8 | 25.8 | C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 1.00 | 1.00 | 0.983 | 0.971 | 3267 | 1009 | 4700 | 2100 | 0.70 | 0.48 | 56.8 | 56.8 | 28.8 | 25.8 | C |

## Segment 9: Basic

| Time <br> Period | PHF | $\mathbf{f H V}$ | Flow Rate <br> $(\mathbf{p c / h})$ | Capacity <br> ( $\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i} / \mathbf{l n})$ | $\mathbf{L O S}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.983 | 3255 | 4700 | 0.69 | 64.3 | 25.3 |  |
| 2 | 1.00 | 0.983 | 3255 | 4700 | 0.69 | 64.3 | C |  |
| 3 | 1.00 | 0.983 | 3255 | 4700 | 0.69 | 64.3 | 25.3 |  |
| 4 | 1.00 | 0.983 | 3255 | 4700 | 0.69 | 64.3 | 25.3 | C |

## Facility Time Period Results

| $\mathbf{T}$ | Speed, mi/h | Density, pc/mi/ln | Density, veh/mi/ln | Travel Time, min | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 63.2 | 20.3 | 19.8 | 6.6 | C |
| 2 | 63.2 | 20.3 | 19.8 | 6.6 | C |
| 3 | 63.2 | 20.3 | 19.8 | 6.6 | C |
| 4 | 63.2 | 20.3 | 19.8 | 6.6 | C |

## Facility Overall Results

| Space Mean Speed, mi/h | 63.2 | Density, veh/mi/ln | 19.8 |
| :--- | :--- | :--- | :--- |
| Average Travel Time, min | 6.6 |  |  |
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## HCS 2010 Facilities Report

## Project Information

| Analyst | PK/LCG | Agency |  |
| :--- | :--- | :--- | :--- |
| Jurisdiction |  | Time Period Analyzed | AM Peak - SB |
| Analysis Year | 2015 - Base AM (3 pgs) | Date | $5 / 1 / 2017$ |
| Project Description | $1-93$ SB - from N of Exit 5 to S of Exit 4 |  |  |

## Facility Global Input

| Jam Density, pc/mi/ln | 190.0 | Density at Capacity, pc/mi/ln | 45.0 |
| :--- | :--- | :--- | :--- |
| Queue Discharge Capacity Drop, \% | 7 | Total Segments | 11 |
| Total Time Periods | 4 | Time Period Duration, min | 15 |

## Segment Geometric Data

| No. | Coded | Analyzed | Name | Length, ft | Lanes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Basic | Basic | $a->b$ | 5280 | 2 |
| 2 | Diverge | Diverge | $b->c$ | 1500 | 2 |
| 3 | Basic | Basic | $c->d$ | 3920 | 2 |
| 4 | Merge | Merge | d->e | 1500 | 2 |
| 5 | Basic | Basic | e->f | 11980 | 2 |
| 6 | Diverge | Diverge | $f->\mathrm{g}$ | 1500 | 2 |
| 7 | Basic | Basic | g->h | 1600 | 2 |
| 8 | Merge | Merge | h->i | 1500 | 2 |
| 9 | Basic | Basic | i->j | 900 | 2 |
| 10 | Merge | Merge | $j->k$ | 1500 | 2 |
| 11 | Basic | Basic | $1->m$ | 5230 | 2 |

## Facility Segment Data

Segment 1: Basic

| Time <br> Period | PHF | $\mathbf{f H V}$ | Flow Rate <br> (pc/h) | Capacity <br> ( $\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> ( $\mathbf{m i} / \mathbf{h})$ | Density <br> (pc/mi/ln) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.980 | 3321 | 4700 | 0.71 | 64.0 | 25.9 | C |
| 2 | 1.00 | 0.980 | 3321 | 4700 | 0.71 | 64.0 | 25.9 | C |
| 3 | 1.00 | 0.980 | 3321 | 4700 | 0.71 | 64.0 | 25.9 | C |
| 4 | 1.00 | 0.980 | 3321 | 4700 | 0.71 | 64.0 | 25.9 | C |

## Segment 2: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | $F$ | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.980 | 0.971 | 3321 | 783 | 4700 | 2000 | 0.71 | 0.39 | 53.5 | 53.5 | 31.0 | 28.1 | D |
| 2 | 1.00 | 1.00 | 0.980 | 0.971 | 3321 | 783 | 4700 | 2000 | 0.71 | 0.39 | 53.5 | 53.5 | 31.0 | 28.1 | D |
| 3 | 1.00 | 1.00 | 0.980 | 0.971 | 3321 | 783 | 4700 | 2000 | 0.71 | 0.39 | 53.5 | 53.5 | 31.0 | 28.1 | D |


| 4 | 1.00 1.00 | 0.980 0.971 | 3321 783 | 4700 2000 | 0.71 0.39 | $53.5 \times 53.5$ | 31.0 28.1 | D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segment 3: Basic |  |  |  |  |  |  |  |  |
| Time <br> Period | PHF | fHV | Flow Rate (pc/h) | Capacity (pc/h) | d/c <br> Ratio | Speed ( $\mathrm{mi} / \mathrm{h}$ ) | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) | LOS |
| 1 | 1.00 | 0.983 | 2538 | 4700 | 0.54 | 65.0 | 19.5 | C |
| 2 | 1.00 | 0.983 | 2538 | 4700 | 0.54 | 65.0 | 19.5 | C |
| 3 | 1.00 | 0.983 | 2538 | 4700 | 0.54 | 65.0 | 19.5 | C |
| 4 | 1.00 | 0.983 | 2538 | 4700 | 0.54 | 65.0 | 19.5 | C |

Segment 4: Merge

| Time <br> Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.983 | 0.952 | 3079 | 541 | 4700 | 2100 | 0.66 | 0.26 | 57.5 | 57.5 | 26.8 | 23.7 | C |
| 2 | 1.00 | 1.00 | 0.983 | 0.952 | 3079 | 541 | 4700 | 2100 | 0.66 | 0.26 | 57.5 | 57.5 | 26.8 | 23.7 | C |
| 3 | 1.00 | 1.00 | 0.983 | 0.952 | 3079 | 541 | 4700 | 2100 | 0.66 | 0.26 | 57.5 | 57.5 | 26.8 | 23.7 | C |
| 4 | 1.00 | 1.00 | 0.983 | 0.952 | 3079 | 541 | 4700 | 2100 | 0.66 | 0.26 | 57.5 | 57.5 | 26.8 | 23.7 | C |

Segment 5: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c} / \mathbf{h})$ | Capacity <br> $(\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i} / \mathbf{l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.983 | 3062 | 4700 | 0.65 | 64.8 | 23.6 | C |
| 2 | 1.00 | 0.983 | 3062 | 4700 | 0.65 | 64.8 | 23.6 | C |
| 3 | 1.00 | 0.983 | 3062 | 4700 | 0.65 | 64.8 | 23.6 | C |
| 4 | 1.00 | 0.983 | 3062 | 4700 | 0.65 | 64.8 | 23.6 | C |

Segment 6: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | $F$ | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.983 | 0.971 | 3062 | 778 | 4700 | 1900 | 0.65 | 0.41 | 50.6 | 50.6 | 30.3 | 23.9 | C |
| 2 | 1.00 | 1.00 | 0.983 | 0.971 | 3062 | 778 | 4700 | 1900 | 0.65 | 0.41 | 50.6 | 50.6 | 30.3 | 23.9 | C |
| 3 | 1.00 | 1.00 | 0.983 | 0.971 | 3062 | 778 | 4700 | 1900 | 0.65 | 0.41 | 50.6 | 50.6 | 30.3 | 23.9 | C |
| 4 | 1.00 | 1.00 | 0.983 | 0.971 | 3062 | 778 | 4700 | 1900 | 0.65 | 0.41 | 50.6 | 50.6 | 30.3 | 23.9 | C |

Segment 7: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> ( $\mathbf{p c} / \mathbf{h}$ ) | Capacity <br> ( $\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> (pc/mi/ln) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.987 | 2285 | 4700 | 0.49 | 65.0 | 17.6 | 8 |
| 2 | 1.00 | 0.987 | 2285 | 4700 | 0.49 | 65.0 | 17.6 | 8 |
| 3 | 1.00 | 0.987 | 2285 | 4700 | 0.49 | 65.0 | 17.6 | 8 |
| 4 | 1.00 | 0.987 | 2285 | 4700 | 0.49 | 65.0 | 17.6 | $B$ |

Segment 8: Merge

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathrm{pc} / \mathrm{h})$ | Capacity <br> $(\mathrm{pc} / \mathrm{h})$ | $\mathrm{d} / \mathrm{c}$ <br> Ratio | Speed <br> $(\mathrm{mi} / \mathrm{h})$ | Density <br> $(\mathrm{pc} / \mathrm{mi} / \mathrm{ln})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 1.00 | 0.985 | 0.980 | 2820 | 531 | 4700 | 2000 | 0.60 | 0.27 | 58.2 | 58.2 | 24.2 | 17.8 | B |
| 2 | 1.00 | 1.00 | 0.985 | 0.980 | 2820 | 531 | 4700 | 2000 | 0.60 | 0.27 | 58.2 | 58.2 | 24.2 | 17.8 | 8 |
| 3 | 1.00 | 1.00 | 0.985 | 0.980 | 2820 | 531 | 4700 | 2000 | 0.60 | 0.27 | 58.2 | 58.2 | 24.2 | 17.8 | 8 |
| 4 | 1.00 | 1.00 | 0.985 | 0.980 | 2820 | 531 | 4700 | 2000 | 0.60 | 0.27 | 58.2 | 58.2 | 24.2 | 17.8 | B |

## Segment 9: Basic

| Time <br> Period | PHF | $\mathbf{f H V}$ | Flow Rate <br> (pc/h) | Capacity <br> ( $\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i / l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.985 | 2817 | 4700 | 0.60 | 65.0 | 21.7 | C |
| 2 | 1.00 | 0.985 | 2817 | 4700 | 0.60 | 65.0 | 21.7 | C |
| 3 | 1.00 | 0.985 | 2817 | 4700 | 0.60 | 65.0 | 21.7 | C |
| 4 | 1.00 | 0.985 | 2817 | 4700 | 0.60 | 65.0 | 21.7 | C |

Segment 10: Merge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c Ratio |  | Speed ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.984 | 0.980 | 3499 | 679 | 4700 | 2100 | 0.74 | 0.32 | 57.2 | 57.2 | 30.6 | 23.7 | C |
| 2 | 1.00 | 1.00 | 0.984 | 0.980 | 3499 | 679 | 4700 | 2100 | 0.74 | 0.32 | 57.2 | 57.2 | 30.6 | 23.7 | C |
| 3 | 1.00 | 1.00 | 0.984 | 0.980 | 3499 | 679 | 4700 | 2100 | 0.74 | 0.32 | 57.2 | 57.2 | 30.6 | 23.7 | C |
| 4 | 1.00 | 1.00 | 0.984 | 0.980 | 3499 | 679 | 4700 | 2100 | 0.74 | 0.32 | 57.2 | 57.2 | 30.6 | 23.7 | C |

Segment 11: Basic

| Time <br> Period | PHF | $\mathbf{f H V}$ | Flow Rate <br> $(\mathbf{p c / h})$ | Capacity <br> $(\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i} / \mathbf{l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.984 | 3496 | 4700 | 0.74 | 63.3 | 27.6 |  |
| 2 | 1.00 | 0.984 | 3496 | 4700 | 0.74 | 63.3 | D |  |
| 3 | 1.00 | 0.984 | 3496 | 4700 | 0.74 | 63.3 | 27.6 | 27.6 |
| 4 | 1.00 | 0.984 | 3496 | 4700 | 0.74 | 63.3 | D |  |

## Facility Time Period Results

| $\mathbf{T}$ | Speed, mi/h | Density, $\mathbf{p c} / \mathbf{m i} / \mathbf{l n}$ | Density, veh/mi/ln | Travel Time, min | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 62.5 | 24.8 | 24.4 | 6.6 | C |
| 2 | 62.5 | 24.8 | 24.4 | 6.6 | C |
| 3 | 62.5 | 24.8 | 24.4 | 6.6 | C |
| 4 | 62.5 | 24.8 | 24.4 | 6.6 | C |

## Facility Overall Results

| Space Mean Speed, mi/h | 62.5 | Density, veh/mi/ln | 24.4 |
| :--- | :--- | :--- | :--- |
| Average Travel Time, min | 6.6 |  |  |

## Project Information

| Analyst | PK/LCG | Agency |  |
| :--- | :--- | :--- | :--- |
| Jurisdiction |  | Time Period Analyzed | 2015 PM Peak - NB |
| Analysis Year | 2015-Base PM (3 pgs) | Date | 5/1/2017 |
| Project Description |  |  |  |

## Facility Global Input

| Jam Density, pc/mi//n | 190.0 | Density at Capacity, pc/mi/ln | 45.0 |
| :--- | :--- | :--- | :--- |
| Queue Discharge Capacity Drop, \% | 7 | Total Segments | 9 |
| Total Time Periods | 4 | Time Period Duration, min | 15 |

## Segment Geometric Data

| No. | Coded | Analyzed | Name | Length, ft | Lanes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Basic | Basic | $\mathrm{a}->\mathrm{b}$ | 5280 | 2 |
| 2 | Diverge | Diverge | $\mathrm{b}->\mathrm{c}$ | 1500 | 2 |
| 3 | Basic | Basic | $\mathrm{c}->\mathrm{d}$ | 2575 | 2 |
| 4 | Merge | Merge | $\mathrm{d}>\mathrm{e}$ | $\mathrm{e}->\mathrm{f}$ | 1500 |
| 5 | Basic | Basic | $\mathrm{f} \rightarrow>\mathrm{g}$ | 13225 | 2 |
| 6 | Diverge | Diverge | $\mathrm{g} \gg \mathrm{h}$ | 1500 | 2 |
| 7 | Basic | Basic | $\mathrm{h} \rightarrow>\mathrm{i}$ | 4100 | 2 |
| 8 | Merge | Merge | Basic |  | 1500 |
| 9 | Basic |  | 5280 | 2 |  |

## Facility Segment Data

Segment 1: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c} / \mathbf{h})$ | Capacity <br> $(\mathbf{p c} / \mathbf{h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i / l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.979 | 3483 | 4700 | 0.74 | 63.3 | 27.5 | D |
| 2 | 1.00 | 0.979 | 3483 | 4700 | 0.74 | 63.3 | 27.5 | $D$ |
| 3 | 1.00 | 0.979 | 3483 | 4700 | 0.74 | 63.3 | 27.5 | $D$ |
| 4 | 1.00 | 0.979 | 3483 | 4700 | 0.74 | 63.3 | 27.5 | $D$ |

Segment 2: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate (pc/h) |  | Capacity (pc/h) |  | d/c <br> Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.979 | 0.995 | 3483 | 1191 | 4700 | 1900 | 0.74 | 0.63 | 49.7 | 49.7 | 35.0 | 26.9 | C |
| 2 | 1.00 | 1.00 | 0.979 | 0.995 | 3483 | 1191 | 4700 | 1900 | 0.74 | 0.63 | 49.7 | 49.7 | 35.0 | 26.9 | C |
| 3 | 1.00 | 1.00 | 0.979 | 0.995 | 3483 | 1191 | 4700 | 1900 | 0.74 | 0.63 | 49.7 | 49.7 | 35.0 | 26.9 | C |
| 4 | 1.00 | 1.00 | 0.979 | 0.995 | 3483 | 1191 | 4700 | 1900 | 0.74 | 0.63 | 49.7 | 49.7 | 35.0 | 26.9 | C |

## Segment 3: Basic

| Time Period | PHF | fHV | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) | d/c <br> Ratio | Speed (mi/h) | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.971 | 2291 | 4700 | 0.49 | 65.0 | 17.6 | B |
| 2 | 1.00 | 0.971 | 2291 | 4700 | 0.49 | 65.0 | 17.6 | B |
| 3 | 1.00 | 0.971 | 2291 | 4700 | 0.49 | 65.0 | 17.6 | B |
| 4 | 1.00 | 0.971 | 2291 | 4700 | 0.49 | 65.0 | 17.6 | B |

Segment 4: Merge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.977 | 0.988 | 3077 | 800 | 4700 | 2100 | 0.65 | 0.38 | 58.6 | 58.6 | 26.3 | 20.3 | C |
| 2 | 1.00 | 1.00 | 0.977 | 0.988 | 3077 | 800 | 4700 | 2100 | 0.65 | 0.38 | 58.6 | 58.6 | 26.3 | 20.3 | C |
| 3 | 1.00 | 1.00 | 0.977 | 0.988 | 3077 | 800 | 4700 | 2100 | 0.65 | 0.38 | 58.6 | 58.6 | 26.3 | 20.3 | C |
| 4 | 1.00 | 1.00 | 0.977 | 0.988 | 3077 | 800 | 4700 | 2100 | 0.65 | 0.38 | 58.6 | 58.6 | 26.3 | 20.3 | C |

Segment 5: Basic

| Time <br> Period | PHF | $\mathbf{f H V}$ | Flow Rate <br> ( $\mathbf{p c} / \mathrm{h})$ | Capacity <br> $(\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i} / \mathbf{l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.977 | 3086 | 4700 | 0.66 | 64.7 | 23.8 | C |
| 2 | 1.00 | 0.977 | 3086 | 4700 | 0.66 | 64.7 | 23.8 | C |
| 3 | 1.00 | 0.977 | 3086 | 4700 | 0.66 | 64.7 | 23.8 | C |
| 4 | 1.00 | 0.977 | 3086 | 4700 | 0.66 | 64.7 | 23.8 | C |

Segment 6: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.977 | 0.971 | 3086 | 474 | 4700 | 2000 | 0.66 | 0.24 | 54.2 | 54.2 | 28.5 | 26.5 | C |
| 2 | 1.00 | 1.00 | 0.977 | 0.971 | 3086 | 474 | 4700 | 2000 | 0.66 | 0.24 | 54.2 | 54.2 | 28.5 | 26.5 | $C$ |
| 3 | 1.00 | 1.00 | 0.977 | 0.971 | 3086 | 474 | 4700 | 2000 | 0.66 | 0.24 | 54.2 | 54.2 | 28.5 | 26.5 | C |
| 4 | 1.00 | 1.00 | 0.977 | 0.971 | 3086 | 474 | 4700 | 2000 | 0.66 | 0.24 | 54.2 | 54.2 | 28.5 | 26.5 | C |

## Segment 7: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> (pc/h) | Capacity <br> (pc/h) | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> (mi/h) | Density <br> (pc/mi/ln) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.978 | 2612 | 4700 | 0.56 | 65.0 | 20.1 | C |
| 2 | 1.00 | 0.978 | 2612 | 4700 | 0.56 | 65.0 | 20.1 | C |
| 3 | 1.00 | 0.978 | 2612 | 4700 | 0.56 | 65.0 | 20.1 | C |
| 4 | 1.00 | 0.978 | 2612 | 4700 | 0.56 | 65.0 | 20.1 | C |

Segment 8: Merge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.983 | 0.981 | 3384 | 785 | 4700 | 2100 | 0.72 | 0.37 | 56.5 | 56.5 | 29.9 | 26.8 | C |


| 2 | 1.00 | 1.00 | 0.983 | 0.981 | 3384 | 785 | 4700 | 2100 | 0.72 | 0.37 | 56.5 | 56.5 | 29.9 | 26.8 | C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 1.00 | 1.00 | 0.983 | 0.981 | 3384 | 785 | 4700 | 2100 | 0.72 | 0.37 | 56.5 | 56.5 | 29.9 | 26.8 | C |
| 4 | 1.00 | 1.00 | 0.983 | 0.981 | 3384 | 785 | 4700 | 2100 | 0.72 | 0.37 | 56.5 | 56.5 | 29.9 | 26.8 | C |

Segment 9: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c / h})$ | Capacity <br> $(\mathbf{p c} / \mathbf{h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i / l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.983 | 3383 | 4700 | 0.72 | 63.8 | 26.5 | D |
| 2 | 1.00 | 0.983 | 3383 | 4700 | 0.72 | 63.8 | 26.5 | $D$ |
| 3 | 1.00 | 0.983 | 3383 | 4700 | 0.72 | 63.8 | 26.5 | $D$ |
| 4 | 1.00 | 0.983 | 3383 | 4700 | 0.72 | 63.8 | 26.5 | $D$ |

## Facility Time Period Results

| $\mathbf{T}$ | Speed, mi/h | Density, pc/mi/ln | Density, veh/mi/ln | Travel Time, min | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 62.7 | 24.9 | 24.4 | 6.6 | C |
| 2 | 62.7 | 24.9 | 24.4 | 6.6 | C |
| 3 | 62.7 | 24.9 | 24.4 | 6.6 | C |
| 4 | 62.7 | 24.9 | 24.4 | 6.6 | C |

## Facility Overall Results

| Space Mean Speed, mi/h | 62.7 | Density, veh/mi/ln | 24.4 |
| :---: | :---: | :---: | :---: |
| Average Travel Time, min | 6.6 |  |  |

## HCS 2010 Facilities Report

## Project Information

| Analyst | PK/LCG | Agency |  |
| :--- | :--- | :--- | :--- |
| Jurisdiction |  | Time Period Analyzed | 2015 PM Peak - S8 |
| Analysis Year | 2015 Base - PM (3 pgs) | Date | $5 / 1 / 2017$ |
| Project Description | 193 SB - from N of Exit S to S of Exit 4 |  |  |

Facility Global Input

| Jam Density, pc/mi/ln | 190.0 | Density at Capacity, pc/mi/ln | 45.0 |
| :--- | :--- | :--- | :--- |
| Queue Discharge Capacity Drop, \% | 7 | Total Segments | 11 |
| Total Time Periods | 4 | Time Period Duration, min | 15 |

## Segment Geometric Data

| No. | Coded | Analyzed | Name | Length, ft | Lanes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Basic | Basic | a->b | 5280 | 2 |
| 2 | Diverge | Diverge | $b->c$ | 1500 | 2 |
| 3 | Basic | Basic | $c \rightarrow$ d | 3920 | 2 |
| 4 | Merge | Merge | d->e | 1500 | 2 |
| 5 | Basic | Basic | e->f | 11980 | 2 |
| 6 | Diverge | Diverge | $f->\mathrm{g}$ | 1500 | 2 |
| 7 | Basic | Basic | $g->h$ | 1600 | 2 |
| 8 | Merge | Merge | h->i | 1500 | 2 |
| 9 | Basic | Basic | i->j | 900 | 2 |
| 10 | Merge | Merge | $j \gg k$ | 1500 | 2 |
| 11 | Basic | Basic | l->m | 5230 | 2 |

## Facility Segment Data

| Time <br> Period | PHF | fHV | Flow Rate <br> (pc/h) | Capacity <br> (pc/h) | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> (pc/mi/ln) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.980 | 3434 | 4700 | 0.73 | 63.6 | 27.0 | D |
| 2 | 1.00 | 0.980 | 3434 | 4700 | 0.73 | 63.6 | 27.0 | $D$ |
| 3 | 1.00 | 0.980 | 3434 | 4700 | 0.73 | 63.6 | 27.0 | $D$ |
| 4 | 1.00 | 0.980 | 3434 | 4700 | 0.73 | 63.6 | 27.0 | $D$ |

## Segment 2: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity ( $\mathrm{pc} / \mathrm{h}$ ) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | $F$ | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.980 | 0.980 | 3434 | 929 | 4700 | 2000 | 0.73 | 0.46 | 53.2 | 53.2 | 32.3 | 29.1 | D |
| 2 | 1.00 | 1.00 | 0.980 | 0.980 | 3434 | 929 | 4700 | 2000 | 0.73 | 0.46 | 53.2 | 53.2 | 32.3 | 29.1 | D |
| 3 | 1.00 | 1.00 | 0.980 | 0.980 | 3434 | 929 | 4700 | 2000 | 0.73 | 0.46 | 53.2 | 53.2 | 32.3 | 29.1 | D |


| 4 | 1.00 1.00 | 0.980 0.980 | 3434 929 | 4700 2000 | 0.73 0.46 | 53.2 53.2 | 32.3 29.1 | D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Segment 3: Basic |  |  |  |  |  |  |  |  |
| Time Period | PHF | fHV | Flow Rate (pc/h) | Capacity (pc/h) | d/c <br> Ratio | Speed ( $\mathrm{mi} / \mathrm{h}$ ) | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) | LOS |
| 1 | 1.00 | 0.980 | 2505 | 4700 | 0.53 | 65.0 | 19.3 | C |
| 2 | 1.00 | 0.980 | 2505 | 4700 | 0.53 | 65.0 | 19.3 | C |
| 3 | 1.00 | 0.980 | 2505 | 4700 | 0.53 | 65.0 | 19.3 | C |
| 4 | 1.00 | 0.980 | 2505 | 4700 | 0.53 | 65.0 | 19.3 | C |

Segment 4: Merge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c <br> Ratio |  | Speed <br> ( $\mathrm{mi} / \mathrm{h}$ ) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | $F$ | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.980 | 0.977 | 2930 | 425 | 4700 | 2100 | 0.62 | 0.20 | 57.8 | 57.8 | 25.3 | 22.6 | C |
| 2 | 1.00 | 1.00 | 0.980 | 0.977 | 2930 | 425 | 4700 | 2100 | 0.62 | 0.20 | 57.8 | 57.8 | 25.3 | 22.6 | C |
| 3 | 1.00 | 1.00 | 0.980 | 0.819 | 3012 | 507 | 4700 | 2100 | 0.64 | 0.24 | 57.6 | 57.6 | 26.1 | 23.2 | C |
| 4 | 1.00 | 1.00 | 0.980 | 0.977 | 2930 | 425 | 4700 | 2100 | 0.62 | 0.20 | 57.8 | 57.8 | 25.3 | 22.6 | C |

Segment 5: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c} / \mathbf{h})$ | Capacity <br> $(\mathbf{p c / h})$ | d/c <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i / l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.980 | 2929 | 4700 | 0.62 | 64.9 | 22.6 |  |
| 2 | 1.00 | 0.980 | 2929 | 4700 | 0.62 | 64.9 | C |  |
| 3 | 1.00 | 0.980 | 2929 | 4700 | 0.62 | 64.9 | C |  |
| 4 | 1.00 | 0.980 | 2929 | 4700 | 0.62 | 64.9 | 22.6 | 22.6 |

Segment 6: Diverge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c <br> Ratio |  | Speed <br> (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.980 | 0.985 | 2929 | 939 | 4700 | 1900 | 0.62 | 0.49 | 50.2 | 50.2 | 29.2 | 22.8 | C |
| 2 | 1.00 | 1.00 | 0.980 | 0.985 | 2929 | 939 | 4700 | 1900 | 0.62 | 0.49 | 50.2 | 50.2 | 29.2 | 22.8 | C |
| 3 | 1.00 | 1.00 | 0.980 | 0.985 | 2929 | 939 | 4700 | 1900 | 0.62 | 0.49 | 50.2 | 50.2 | 29.2 | 22.8 | C |
| 4 | 1.00 | 1.00 | 0.980 | 0.985 | 2929 | 939 | 4700 | 1900 | 0.62 | 0.49 | 50.2 | 50.2 | 29.2 | 22.8 | C |

## Segment 7: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c / h})$ | Capacity <br> $(\mathbf{p c} / \mathbf{h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i} / \mathbf{n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.978 | 1989 | 4700 | 0.42 | 65.0 | 15.3 | B |
| 2 | 1.00 | 0.978 | 1989 | 4700 | 0.42 | 65.0 | 15.3 | $B$ |
| 3 | 1.00 | 0.978 | 1989 | 4700 | 0.42 | 65.0 | 15.3 | $B$ |
| 4 | 1.00 | 0.978 | 1989 | 4700 | 0.42 | 65.0 | 15.3 | $B$ |

Segment 8: Merge

| Time <br> Period | PHF | fHV | Flow Rate <br> (pc/h) | Capacity <br> (pc/h) | d/c <br> Ratio | Speed <br> $(\mathrm{mi} / \mathrm{h})$ | Density <br> $(\mathrm{pc} / \mathrm{mi} / \mathrm{ln})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | $F$ | R | F | R | Freeway | Ramp |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 1.00 | 0.978 | 0.980 | 2208 | 219 | 4700 | 2000 | 0.47 | 0.11 | 58.9 | 58.9 | 18.7 | 13.2 | B |
| 2 | 1.00 | 1.00 | 0.978 | 0.980 | 2208 | 219 | 4700 | 2000 | 0.47 | 0.11 | 58.9 | 58.9 | 18.7 | 13.2 | 8 |
| 3 | 1.00 | 1.00 | 0.978 | 0.980 | 2208 | 219 | 4700 | 2000 | 0.47 | 0.11 | 58.9 | 58.9 | 18.7 | 13.2 | B |
| 4 | 1.00 | 1.00 | 0.978 | 0.980 | 2208 | 219 | 4700 | 2000 | 0.47 | 0.11 | 58.9 | 58.9 | 18.7 | 13.2 | B |

Segment 9: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c / h})$ | Capacity <br> $(\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i / l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.978 | 2209 | 4700 | 0.47 | 65.0 | 17.0 | 8 |
| 2 | 1.00 | 0.978 | 2209 | 4700 | 0.47 | 65.0 | 17.0 | 8 |
| 3 | 1.00 | 0.978 | 2209 | 4700 | 0.47 | 65.0 | 17.0 | 8 |
| 4 | 1.00 | 0.978 | 2209 | 4700 | 0.47 | 65.0 | 17.0 | 8 |

Segment 10: Merge

| Time Period | PHF |  | fHV |  | Flow Rate ( $\mathrm{pc} / \mathrm{h}$ ) |  | Capacity (pc/h) |  | d/c Ratio |  | Speed (mi/h) |  | Density ( $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ ) |  | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | F | R | F | R | Freeway | Ramp | Freeway | Ramp | F | R | F | R | Freeway | Ramp |  |
| 1 | 1.00 | 1.00 | 0.978 | 0.980 | 2515 | 306 | 4700 | 2100 | 0.54 | 0.15 | 59.1 | 59.1 | 21.3 | 16.2 | 8 |
| 2 | 1.00 | 1.00 | 0.978 | 0.980 | 2515 | 306 | 4700 | 2100 | 0.54 | 0.15 | 59.1 | 59.1 | 21.3 | 16.2 | B |
| 3 | 1.00 | 1.00 | 0.978 | 0.980 | 2515 | 306 | 4700 | 2100 | 0.54 | 0.15 | 59.1 | 59.1 | 21.3 | 16.2 | $B$ |
| 4 | 1.00 | 1.00 | 0.978 | 0.980 | 2515 | 306 | 4700 | 2100 | 0.54 | 0.15 | 59.1 | 59.1 | 21.3 | 16.2 | B |

Segment 11: Basic

| Time <br> Period | PHF | fHV | Flow Rate <br> $(\mathbf{p c} / \mathbf{h})$ | Capacity <br> $(\mathbf{p c / h})$ | $\mathbf{d} / \mathbf{c}$ <br> Ratio | Speed <br> $(\mathbf{m i} / \mathbf{h})$ | Density <br> $(\mathbf{p c / m i / l n})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.00 | 0.978 | 2515 | 4700 | 0.54 | 65.0 | 19.4 |  |
| 2 | 1.00 | 0.978 | 2515 | 4700 | 0.54 | 65.0 | C |  |
| 3 | 1.00 | 0.978 | 2515 | 4700 | 0.54 | 65.0 | 19.4 | C |
| 4 | 1.00 | 0.978 | 2515 | 4700 | 0.54 | 65.0 | 19.4 | 19.4 |

## Facility Time Period Results

| $\mathbf{T}$ | Speed, mi/h | Density, pc/mi/ln | Density, veh/mi/ln | Travel Time, min | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 62.8 | 22.5 | 22.1 | 6.6 | C |
| 2 | 62.8 | 22.5 | 22.1 | 6.6 | C |
| 3 | 62.8 | 22.6 | 22.1 | 6.6 | C |
| 4 | 62.8 | 22.5 | 22.1 | 6.6 | C |

## Facility Overall Results

| Space Mean Speed, mi/h | 62.8 | Density, veh/mi/ln | 22.1 |
| :--- | :--- | :--- | :--- |
| Average Travel Time, min | 6.6 |  |  |
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| Base PM-S8.xff |  |  |  |

## APPENDIX G-1: HCM AND SYNCHRO PRINTOUTS SIGNALIZED INTERSECTION CAPACITY ANALYSES - 2015 AM PEAK HOURS - SYNCHRO PRINTOUTS



4A Zone $27: 30$ am 8/3/2016 Existing 2015 AM Peak


## Intersection Summary

Area Type: Other
Cyde Length: 100
Actuated Cycle Length: 100
Offset 0 (0\%), Referenced to phase 2:EBWB, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.75
Intersection Signal Delay: 12.8
Intersection LOS: B
Intersection Capacity Utifzation 58.3\%
ICU Level of Service B
Analysis Period (min) 15
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 7: Exit 4 SB Off


|  | 1 | 1 | $\cdots$ | $\downarrow$ | 3 | $\ngtr$ | จ | $\downarrow$ | $\checkmark$ | $k$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBR | SEL | SER | NEL | NET | NER | SWL | SWT | SWR | 30.aci |
| Lane Configurations | 7\% | 7 |  |  | ${ }^{7}$ | 个个 |  |  | $4 \uparrow$ | \% |  |
| Traffic Volume (vph) | 210 | 200 | 0 | 0 | 585 | 590 | 0 | 0 | 875 | 0 |  |
| Future Volume (vph) | 210 | 200 | 0 | 0 | 585 | 590 | 0 | 0 | 875 | 0 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Storage Length (ft) | 0 | 0 | 0 | 0 | 350 |  | 0 | 0 |  | 0 |  |
| Storage Lanes | 2 | 1 | 0 | 0 | 1 |  | 0 | 0 |  | 1 |  |
| Taper Length (ft) | 25 |  | 25 |  | 25 |  |  | 25 |  | 1 |  |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Frt |  | 0.850 |  |  |  |  |  |  |  |  |  |
| Fit Protected | 0.950 |  |  |  | 0.950 |  |  |  |  |  |  |
| Satd. Flow (prot) | 3242 | 1495 | 0 | 0 | 1719 | 3438 | 0 | 0 | 3505 | 1845 |  |
| Fit Permitted | 0.950 |  |  |  | 0.950 |  |  |  |  |  |  |
| Satd. Flow (perm) | 3242 | 1495 | 0 | 0 | 1719 | 3438 | 0 | 0 | 3505 | 1845 |  |
| Right Turn on Red |  | Yes |  |  |  |  | Yes |  |  | Yes |  |
| Satd. Flow (RTOR) |  | 227 |  |  |  |  |  |  |  |  |  |
| Link Speed (mph) | 25 |  | 30 |  |  | 30 |  |  | 30 |  |  |
| Link Distance ( ft ) | 347 |  | 390 |  |  | 494 |  |  | 346 |  |  |
| Travel Time (s) | 9.5 |  | 8.9 |  |  | 11.2 |  |  | 7.9 |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.92 | 0.92 | 0.94 | 0.94 | 0.94 | 0.92 | 0.92 | 0.92 |  |
| Heary Vehicles (\%) | 8\% | 8\% | 2\% | 2\% | 5\% | 5\% | 5\% | 3\% | 3\% | 3\% |  |
| Adj. Flow (vph) | 239 | 227 | 0 | 0 | 622 | 628 | 0 | 0 | 951 | 0 |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  | 0 |  |
| Lane Group Flow (vph) | 239 | 227 | 0 | 0 | 622 | 628 | 0 | 0 | 951 | 0 |  |
| Turn Type | Prot | Free |  |  | Prot | NA |  |  | NA | Free |  |
| Protected Phases | 2 |  |  |  | 7 | 4 |  |  | 8 |  |  |
| Permitted Phases |  | Free |  |  |  |  |  |  |  | Free |  |
| Detector Phase Switch Phase | 2 |  |  |  | 7 | 4 |  |  | 8 |  |  |
| Minimum Inital (s) | 10.0 |  |  |  | 5.0 | 10.0 |  |  | 10.0 |  |  |
| Minimum Split (s) | 46.0 |  |  |  | 11.0 | 46.0 |  |  | 46.0 |  |  |
| Total Split (s) | 31.0 |  |  |  | 35.0 | 69.0 |  |  | 34.0 |  |  |
| Total Split (\%) | 31.0\% |  |  |  | 35.0\% | 69.0\% |  |  | 34.0\% |  |  |
| Maximum Green (s) | 25.0 |  |  |  | 29.0 | 63.0 |  |  | 28.0 |  |  |
| Yellow Time (s) | 4.0 |  |  |  | 4.0 | 4.0 |  |  | 4.0 |  |  |
| All-Red Time (s) | 20 |  |  |  | 2.0 | 2.0 |  |  | 2.0 |  |  |
| Lost Time Adjust (s) | 0.0 |  |  |  | 0.0 | 0.0 |  |  | 0.0 |  |  |
| Total Lost Time (s) | 6.0 |  |  |  | 6.0 | 6.0 |  |  | 6.0 |  |  |
| Lead/lag |  |  |  |  | Lead |  |  |  | Lag |  |  |
| Lead-Lag Optimize? <br> Vehicle Extension (s) | 3.0 |  |  |  |  |  |  |  |  |  |  |
| Recal Mode | C.Min |  |  |  | None | Min |  |  | 3.0 Min |  |  |
| Wak Time (s) | 7.0 |  |  |  |  | 7.0 |  |  | 7.0 |  |  |
| Flash Dont Walk (s) | 11.0 |  |  |  |  | 11.0 |  |  | 11.0 |  |  |
| Pedestrian Calls (\#\#tr) | 0 |  |  |  |  | 0 |  |  | 0 |  |  |
| Act Effict Green (s) | 12.9 | 100.0 |  |  | 41.1 | 75.1 |  |  | 28.0 |  |  |
| Actuated g/C Ratio | 0.13 | 1.00 |  |  | 0.41 | 0.75 |  |  | 0.28 |  |  |
| $v i c$ Ratio | 0.57 | 0.15 |  |  | 0.88 | 0.24 |  |  | 0.97 |  |  |
| Control Delay | 46.2 | 0.2 |  |  | 43.8 | 4.3 |  |  | 58.7 |  |  |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 | 0.0 |  |  | 0.0 |  |  |
| 4A Zone 27:30 am 8/3/20 LC | xisting 20 | 15 AM Pe |  |  |  |  |  |  |  |  | 9 Report Page 1 |


|  | 1 | \% | $\checkmark$ |  | $\bar{y}$ | $\pi$ | $\downarrow$ | $\downarrow$ | 4 | k |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBR | SEL | SER | NEL | NET | NER | SWL | SWT | SWR |
| Total Delay | 46.2 | 0.2 |  |  | 43.8 | 4.3 |  |  | 58.7 |  |
| LOS | D | A |  |  | D | A |  |  | E |  |
| Approach Delay | 23.8 |  |  |  |  | 23.9 |  |  | 58.7 |  |
| Approach LOS | C |  |  |  |  | C |  |  | E |  |
| Queue Length 50th (fi) | 75 | 0 |  |  | 357 | 52 |  |  | 315 |  |
| Queue Length 95th (ti) | 107 | 0 |  |  | \#610 | 83 |  |  | \#448 |  |
| Internal Link Dist ( t ) | 267 |  | 310 |  |  | 414 |  |  | 266 |  |
| Turn Bay Length ( t ) |  |  |  |  | 350 |  |  |  |  |  |
| Base Capacity (vph) | 810 | 1495 |  |  | 706 | 2582 |  |  | 981 |  |
| Stavation Cap Reductn | 0 | 0 |  |  | 0 | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 | 0 |  |  | 0 |  |
| Reduced vic Ratio | 0.30 | 0.15 |  |  | 0.88 | 0.24 |  |  | 0.97 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |
| Cyde Length: 100 |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |
| Offset $0(0 \%)$, Referenced to phase 2:NBL and 6: Start of Green |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 145 |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coorcinated |  |  |  |  |  |  |  |  |  |  |
| Maximum vic Rato: 0.97 |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 36.3 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |
| Intersection Capacity Utilization 84.6\% |  |  |  | ICU Level of Service E |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 11: Exit 4 NB Off \& NH 102


|  | 4 | $\rightarrow$ | $\checkmark$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $\nu$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | S8T | SBR |
| Lane Configurations |  | ¢ $\uparrow$ | \# | ${ }^{*}$ | ¢个 |  |  |  |  | \%* |  | 7 |
| Traffic Volume (vph) | 0 | 515 | 280 | 235 | 605 | 0 | 0 | 0 | 0 | 465 | 0 | 295 |
| Future Volume (vph) | 0 | 515 | 280 | 235 | 605 | 0 | 0 | 0 | 0 | 465 | 0 | 295 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 |
| Fit |  |  | 0.850 |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  | 0.950 |  |  |  |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 3167 | 1417 | 1687 | 3374 | 0 | 0 | 0 | 0 | 3303 | 0 | 1524 |
| Flt Permitted |  |  |  | 0.950 |  |  |  |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 0 | 3167 | 1417 | 1687 | 3374 | 0 | 0 | 0 | 0 | 3303 | 0 | 1524 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 304 |  |  |  |  |  |  |  |  | 123 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 35 |  |
| Link Distance (t) |  | 410 |  |  | 242 |  |  | 486 |  |  | 444 |  |
| Travel Time (s) |  | 9.3 |  |  | 5.5 |  |  | 11.0 |  |  | 8.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.73 | 0.73 | 0.73 | 0.92 | 0.92 | 0.92 | 0.74 | 0.74 | 0.74 |
| Heary Vehicles (\%) | 14\% | 14\% | 14\% | 7\% | 7\% | 7\% | 2\% | 2\% | 2\% | 6\% | 6\% | 6\% |
| Adj. Flow (vph) | 0 | 560 | 304 | 322 | 829 | 0 | 0 | 0 | 0 | 628 | 0 | 399 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (yph) | 0 | 560 | 304 | 322 | 829 | 0 | 0 | 0 | 0 | 628 | 0 | 399 |
| Turn Type |  | NA | Free | Prot | NA |  |  |  |  | Prot |  | Prot |
| Protecled Phases |  | 2 |  | 1 | 6 |  |  |  |  | 4 |  | 4 |
| Permited Phases |  |  | Free |  |  |  |  |  |  |  |  |  |
| Detector Phase |  | 2 |  | 1 | 6 |  |  |  |  | 4 |  | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) |  | 5.0 |  | 4.0 | 5.0 |  |  |  |  | 3.0 |  | 3.0 |
| Minimum Split (s) |  | 26.0 |  | 24.0 | 26.0 |  |  |  |  | 36.0 |  | 36.0 |
| Total Split (s) |  | 24.0 |  | 22.0 | 46.0 |  |  |  |  | 34.0 |  | 34.0 |
| Total Split (\%) |  | 30.0\% |  | 27.5\% | 57.5\% |  |  |  |  | 42.5\% |  | 42.5\% |
| Maximum Green (s) |  | 18.0 |  | 16.0 | 40.0 |  |  |  |  | 28.0 |  | 28.0 |
| Yellow Time (s) |  | 4.0 |  | 4.0 | 4.0 |  |  |  |  | 4.0 |  | 4.0 |
| All-Red Time (s) |  | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 |  | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 |  |  |  |  | 0.0 |  | 0.0 |
| Total Lost Time (s) |  | 6.0 |  | 6.0 | 6.0 |  |  |  |  | 6.0 |  | 6.0 |
| LeadLag |  | Lag |  | Lead |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  | Yes |  | Yes |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  | 3.0 | 3.0 |  |  |  |  | 3.0 |  | 3.0 |
| Recal Mode |  | C.Max |  | None | C-Max |  |  |  |  | None |  | None |
| Walk Time (s) |  | 7.0 |  | 7.0 | 7.0 |  |  |  |  | 7.0 |  | 7.0 |
| Flash Dont Walk (s) |  | 11.0 |  | 11.0 | 11.0 |  |  |  |  | 11.0 |  | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 |  | 0 | 0 |  |  |  |  | 0 |  | 0 |
| Act Efftet Green (s) |  | 20.9 | 80.0 | $18.8{ }^{\text {. }}$ | 45.7 |  |  |  |  | 22.3 |  | 223 |
| Actuated g/C Ratio |  | 0.26 | 1.00 | 0.24 | 0.57 |  |  |  |  | 0.28 |  | 0.28 |
| vic Ratio |  | 0.68 | 0.21 | 0.81 | 0.43 |  |  |  |  | 0.68 |  | 0.78 |
| Control Delay |  | 32.7 | 0.3 | 40.0 | 7.0 |  |  |  |  | 29.2 |  | 28.7 |
| Queve Delay |  | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  | 0.0 |  | 0.0 |
| Total Delay |  | 32.7 | 0.3 | 40.0 | 7.0 |  |  |  |  | 29.2 |  | 28.7 |
| LOS |  | C | A | D | A |  |  |  |  | C |  | C |
| Approach Delay |  | 21.3 |  |  | 16.3 |  |  |  |  |  | 29.0 |  |


|  | $\rangle$ | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach LOS |  | C |  |  | B |  |  |  |  |  | C |  |
| Queue Length 50\% (fi) |  | 139 | 0 | 87 | 46 |  |  |  |  | 142 |  | 127 |
| Queue Length 95th (f) |  | \#212 | 0 | \#211 | 59 |  |  |  |  | 138 |  | 146 |
| Internal Link Dist (f) |  | 330 |  |  | 162 |  |  | 406 |  |  | 364 |  |
| Turn Bay Length (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 828 | 1417 | 396 | 1929 |  |  |  |  | 1156 |  | 613 |
| Starvation Cap Reductn |  | 0 | 0 | 0 | 0 |  |  |  |  | 0 |  | 0 |
| Spilback Cap Reductn |  | 0 | 0 | 0 | 0 |  |  |  |  | 0 |  | 0 |
| Storage Cap Reductn |  | 0 | 0 | 0 | 0 |  |  |  |  | - |  | 0 |
| Reduced vic Rasio |  | 0.68 | 0.21 | 0.81 | 0.43 |  |  |  |  | 0.54 |  | 0.65 |


| Intersection Summary |  |
| :--- | :--- |
| Area Type: |  |
| Other |  |

Cycie Length: 80
Actuated Cycle Length: 80
Offset $38(48 \%)$, Referenced to phase $2:$ EBT and $6:$ WBT. Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.81
Intersection Signal Delay. 22.0 Intersection LOS: C
Intersection Capaaty Ublization 65.7\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queve may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: $\quad 3:$ Exit 5 S8 On/Exit 5 SB Off \& NH 28


|  | $\rangle$ | $\rightarrow$ | $\checkmark$ | $\checkmark$ | $\longleftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 9 | $4 \uparrow$ |  |  | $\uparrow \uparrow$ | 7 | ${ }^{*}$ |  | * |  |  |  |
| Traffic Volume (vph) | 240 | 740 | 0 | 0 | 540 | 740 | 300 | 0 | 110 | 0 | 0 | 0 |
| Future Volume (yph) | 240 | 740 | 0 | 0 | 540 | 740 | 300 | 0 | 110 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  |  |  |  | 0.850 |  |  | 0.850 |  |  |  |
| Fil Protected | 0.950 |  |  |  |  |  | 0.950 |  |  |  |  |  |
| Sald. Flow (prot) | 1641 | 3282 | 0 | 0 | 3438 | 1538 | 1656 | 0 | 1482 | 0 | 0 | 0 |
| Fil Permitted | 0.950 |  |  |  |  |  | 0.950 |  |  |  |  |  |
| Satd. Flow (perm) | 1641 | 3282 | 0 | 0 | 3438 | 1538 | 1656 | 0 | 1482 | 0 | 0 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  |  |  |  | 822 |  |  | 205 |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 35 |  |  | 30 |  |
| Link Distance (ft) |  | 196 |  |  | 451 |  |  | 450 |  |  | 368 |  |
| Travel Time (s) |  | 4.5 |  |  | 10.3 |  |  | 8.8 |  |  | 8.4 |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.90 | 0.90 | 0.90 | 0.78 | 0.78 | 0.78 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 10\% | 10\% | 10\% | 5\% | 5\% | 5\% | 9\% | 9\% | 9\% | 2\% | 2\% | 2\% |
| Adj. Flow (yph) | 276 | 851 | 0 | 0 | 600 | 822 | 385 | 0 | 141 |  | 0 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 276 | 851 | 0 | 0 | 600 | 822 | 385 | 0 | 141 | 0 | 0 | 0 |
| Turn Type | Prot | NA |  |  | NA | Free | Prot |  | Free |  |  | 0 |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 |  |  |  |  |  |
| Permitted Phases |  | 2 |  |  | 6 | Free |  |  | Free |  |  |  |
| Detector Phase | 5 | 2 |  |  | 6 |  | 8 |  |  |  |  |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Intital (s) | 5.0 | 5.0 |  |  | 5.0 |  | 5.0 |  |  |  |  |  |
| Minimum Split (s) | 24.0 | 24.0 |  |  | 24.0 |  | 11.0 |  |  |  |  |  |
| Total Split (s) | 22.0 | 51.0 |  |  | 29.0 |  | 29.0 |  |  |  |  |  |
| Total Split (\%) | 27.5\% | 63.8\% |  |  | 36.3\% |  | 36.3\% |  |  |  |  |  |
| Maximum Green (s) | 16.0 | 45.0 |  |  | 23.0 |  | 23.0 |  |  |  |  |  |
| Yellow Time (s) | 4.0 | 4.0 |  |  | 4.0 |  | 4.0 |  |  |  |  |  |
| All-Red Time (s) | 2.0 | 2.0 |  |  | 2.0 |  | 2.0 |  |  |  |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  |  | 0.0 |  | 0.0 |  |  |  |  |  |
| Total Lost Time (s) | 6.0 | 6.0 |  |  | 6.0 |  | 6.0 |  |  |  |  |  |
| Leadlag | Lead |  |  |  | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  |  | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  |  | 3.0 |  | 3.0 |  |  |  |  |  |
| Recall Mode | None | C-Max |  |  | C-Max |  | None |  |  |  |  |  |
| Walk Time (s) | 7.0 | 7.0 |  |  | 7.0 |  |  |  |  |  |  |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  |  | 11.0 |  |  |  |  |  |  |  |
| Pedestrian Calls (\#frr) | 0 | 0 |  |  | 0 |  |  |  |  |  |  |  |
| Act Effl Green (s) | 15.7 | 46.6 |  |  | 24.9 | 80.0 | 21.4 |  | 80.0 |  |  |  |
| Actuated g/C Ratio | 0.20 | 0.58 |  |  | 0.31 | 1.00 | 0.27 |  | 1.00 |  |  |  |
| vic Ratio | 0.86 | 0.44 |  |  | 0.56 | 0.53 | 0.87 |  | 0.10 |  |  |  |
| Control Delay | 55.0 | 22 |  |  | 26.1 | 1.3 | 49.4 |  | 0.1 |  |  |  |
| Queve Delay | 0.0 | 0.0 |  |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  |  |
| Total Delay | 55.0 | 2.2 |  |  | 26.1 | 1.3 | 49.4 |  | 0.1 |  |  |  |
| LOS | D | A |  |  | C | A | D |  | A |  |  |  |
| Approach Delay |  | 15.1 |  |  | 11.8 |  |  | 36.2 |  |  |  |  |


|  | $\Rightarrow$ | $\rightarrow$ |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | S8T | SBR |
| Approach LOS |  | B |  |  | B |  |  | D |  |  |  |  |
| Queue Length 50th (ft) | 130 | 0 |  |  | 135 | 0 | 178 |  | 0 |  |  |  |
| Queue Length 95th (f) | \#251 | 5 |  |  | 189 | 0 | 233 |  | 0 |  |  |  |
| Internal Link Dist (tt) |  | 116 |  |  | 371 |  |  | 370 |  |  | 288 |  |
| Turn Bay Length ( f ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 333 | 1913 |  |  | 1071 | 1538 | 476 |  | 1482 |  |  |  |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 |  |  |  |
| Spilback Cap Reductr | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 |  |  |  |
| Storage Cap Reductn | 0 | 0 |  |  | 0 | 0 | 0 |  | 0 |  |  |  |
| Reduced vic Ratio | 0.83 | 0.44 |  |  | 0.56 | 0.53 | 0.81 |  | 0.10 |  |  |  |

Intersection Summary

Cycle Length: 80
Actuated Cycle Length: 80
Offset $0(0 \%)$, Referenced to phase 2:EBT and 6:WBT, Start of Green
Natural Cycle: 70
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.87
Intersection Signal Delay: 17.2 Intersection LOS: B
Intersection Capacity Ubilization 65.7\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shomn is maximum after two cycles.
Spits and Phases: 2: Exit 5 NB Off \& NH 28


| Lane Group | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | 4 |  |  | 4 |  |  | F |  |  | 4 |  |
| Traffic Volume (vph) | 5 | 25 | 10 | 345 | 0 | 70 | 0 | 400 | 125 | 15 | 595 | 0 |
| Future Volume (yph) | 5 | 25 | 10 | 345 | 0 | 70 | 0 | 400 | 125 | 15 | 595 | 0 |
| Ideal Flow (yphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Uti. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.966 |  |  | 0.977 |  |  | 0.968 |  |  |  |  |
| Fll Protected |  | 0.994 |  |  | 0.960 |  |  |  |  |  | 0.999 |  |
| Satd. Flow (prot) | 0 | 1789 | 0 | 0 | 1730 | 0 | 0 | 1703 | 0 | 0 | 1808 | 0 |
| Filt Permitted |  | 0.937 |  |  | 0.716 |  |  |  |  |  | 0.981 |  |
| Satd. Flow (perm) | 0 | 1686 | 0 | 0 | 1290 | 0 | 0 | 1703 | 0 | 0 | 1775 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 17 |  |  | 55 |  |  | 36 |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 285 |  |  | 644 |  |  | 243 |  |  | 338 |  |
| Travel Time (s) |  | 6.5 |  |  | 14.6 |  |  | 5.5 |  |  | 7.7 |  |
| Peak Hour Factor | 0.60 | 0.60 | 0.60 | 0.96 | 0.96 | 0.96 | 0.89 | 0.89 | 0.89 | 0.86 | 0.88 | 0.86 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 3\% | 3\% | 3\% | 8\% | 8\% | 8\% | 5\% | 5\% | 5\% |
| Adj. Flow (vph) | 8 | 42 | 17 | 359 | 0 | 73 | 0 | 449 | 140 | 17 | 692 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 67 | 0 | 0 | 432 | 0 | 0 | 589 | 0 | 0 | 709 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  |  | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |
| Permitted Phases | 2 |  |  | 2 |  |  |  |  |  | 1 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  |  | 1 |  | 1 | 1 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Inital (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  |  | 5.0 |  | 5.0 | . 0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  |  | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 25.0 | 25.0 |  | 25.0 | 25.0 |  |  | 35.0 |  | 35.0 | 35.0 |  |
| Total Split (\%) | 41.7\% | 41.7\% |  | 41.7\% | 41.7\% |  |  | 58.3\% |  | 58.3\% | 58.3\% |  |
| Maximum Green (s) | 19.0 | 19.0 |  | 19.0 | 19.0 |  |  | 29.0 |  | 29.0 | 29.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 20 | 2.0 |  | 2.0 | 2.0 |  |  | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Lead/lag | Lag | Lag |  | Lag | Lag |  |  | Lead |  | Lead | Lead |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  |  | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  |  | Min |  | Min | Min |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#hr) | 0 | 0 |  | 0 | 0 |  |  | 0 |  | 0 | 0 |  |
| Act Effict Green (s) |  | 19.1 |  |  | 19.1 |  |  | 27.3 |  |  | 27.3 |  |
| Actuated glC Rato |  | 0.33 |  |  | 0.33 |  |  | 0.47 |  |  | 0.47 |  |
| vic Ratio |  | 0.12 |  |  | 0.94 |  |  | 0.72 |  |  | 0.86 |  |
| Control Delay |  | 12.4 |  |  | 51.7 |  |  | 17.7 |  |  | 26.4 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay |  | 12.4 |  |  | 51.7 |  |  | 17.7 |  |  | 26.4 |  |
| LOS |  | B |  |  | D |  |  | B |  |  | c |  |
| Approach Delay |  | 12.4 |  |  | 51.7 |  |  | 17.7 |  |  | 26.4 |  |


|  | $\cdots$ | $\backslash$ | $\lambda$ | $m$ | $k$ | \% | 5 | $\not$ | 2 | 4 | 4 | k |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Approach LOS |  | 8 |  |  | D |  |  | 8 |  |  | C |  |
| Queve Length 50th (f) |  | 13 |  |  | 135 |  |  | 145 |  |  | 206 |  |
| Queue Length 95th (f) |  | 22 |  |  | \#304 |  |  | 247 |  |  | \#368 |  |
| Internal Link Dist (f) |  | 205 |  |  | 564 |  |  | 163 |  |  | 258 |  |
| Turn Bay Length (t) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) |  | 562 |  |  | 458 |  |  | 856 |  |  | 884 |  |
| Starvation Cap Reductn |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced vic Ratio |  | 0.12 |  |  | 0.94 |  |  | 0.68 |  |  | 0.80 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: Other
Cycle Length: 60
Actuated Cyde Length: 58.4
Natural Cyde: 70
Control Type: Actuated-Uncoorcinated
Maximum wic Ratio: 0.94
Intersection Signal Delay: 29.1
Intersection LOS C
Intersection Capacity Utízation 83.4\%
ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 4: NH 102 \& FordwayN. High St


|  | $\dagger$ |  |  | $t$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | S8T | SBR |
| Lane Configuratons | 7 | ち |  | \% | ¢ |  | ${ }^{5}$ | ¢ |  | 7 | $\uparrow$ | ¢ |
| Traffic Volume (vph) | 105 | 205 | 60 | 35 | 385 | 80 | 60 | 260 | 40 | 70 | 230 | 105 |
| Future Volume (vph) | 105 | 205 | 60 | 35 | 385 | 80 | 60 | 260 | 40 | 70 | 230 | 105 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.966 |  |  | 0.974 |  |  | 0.980 |  |  |  | 0.850 |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1656 | 1684 | 0 | 1703 | 1746 | 0 | 1719 | 1773 | 0 | 1703 | 1792 | 1524 |
| Fit Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1656 | 1684 | 0 | 1703 | 1746 | 0 | 1719 | 1773 | 0 | 1703 | 1792 | 1524 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 20 |  |  | 14 |  |  | O |  |  |  | 205 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ti) |  | 505 |  |  | 530 |  |  | 361 |  |  | 411 |  |
| Travel Time (s) |  | 11.5 |  |  | 12.0 |  |  | 8.2 |  |  | 9.3 |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.94 | 0.94 | 0.94 | 0.85 | 0.85 | 0.85 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 9\% | 9\% | 9\% | 6\% | 6\% | 6\% | 5\% | 5\% | 5\% | 6\% | 6\% | 6\% |
| Parking (\#/hr) |  |  | 0 |  |  |  |  |  |  |  |  |  |
| Adj. Flow (voh) | 109 | 214 | 63 | 37 | 410 | 85 | 71 | 306 | 47 | 77 | 253 | 115 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 109 | 277 | 0 | 37 | 495 | 0 | 71 | 353 | 0 | 77 | 253 | 115 |
| Turn Type | Prot | NA |  | Prot | NA |  | Prot | NA |  | Prot | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 8 |  | 7 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( s ) | 4.0 | 5.0 |  | 4.0 | 10.0 |  | 4.0 | 10.0 |  | 4.0 | 9.0 | 9.0 |
| Minimum Spit (s) | 10.0 | 30.0 |  | 10.0 | 30.0 |  | 10.0 | 25.0 |  | 10.0 | 25.0 | 25.0 |
| Total Spit (s) | 12.0 | 33.0 |  | 12.0 | 33.0 |  | 10.0 | 25.0 |  | 10.0 | 25.0 | 25.0 |
| Total Spit (\%) | 15.0\% | 41.3\% |  | 15.0\% | 41.3\% |  | 12.5\% | 31.3\% |  | 12.5\% | 31.3\% | 31.3\% |
| Maximum Green (s) | 6.0 | 27.0 |  | 6.0 | 27.0 |  | 4.0 | 19.0 |  | 4.0 | 19.0 | 19.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Lead/ag | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | Min |  | None | Mn |  | Min | None |  | Min | None | None |
| Wak Time (s) |  | 7.0 |  |  | 7.0 |  |  | 7.0 |  |  | 7.0 | 7.0 |
| Flash Dont Wak (s) |  | 11.0 |  |  | 11.0 |  |  | 11.0 |  |  | 11.0 | 11.0 |
| Pedestrian Calls (\#hr) |  | 10 |  |  | 10 |  |  | 0 | - |  | 10 | 10 |
| Act Effct Green (s) | 6.0 | 29.4 |  | 5.9 | 24.1 |  | 4.0 | 17.5 |  | 4.0 | 17.5 | 17.5 |
| Actuated g/C Ratio | 0.08 | 0.39 |  | 0.08 | 0.32 |  | 0.05 | 0.23 |  | 0.05 | 0.23 | 0.23 |
| vic Ratio | 0.83 | 0.42 |  | 0.28 | 0.88 |  | 0.79 | 0.85 |  | 0.86 | 0.61 | 0.23 |
| Control Delay | 83.0 | 20.1 |  | 40.6 | 42.7 |  | 90.6 | 48.3 |  | 103.4 | 33.9 | 1.1 |
| Queve Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 83.0 | 20.1 |  | 40.6 | 42.7 |  | 90.6 | 48.3 |  | 103.4 | 33.9 | 1.1 |
| LOS | F | C |  | D | D |  | F | D |  | F | C | A |


|  | $\dagger$ | $\rightarrow$ | $\rangle$ | $\checkmark$ | - | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR. | NBL | NBT | NBR | SBL | SBT | SBR |
| Approach Delay |  | 37.8 |  |  | 42.6 |  |  | 55.4 |  |  | 37.4 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | D |  |
| Queue Length 50th (t) | 55 | 99 |  | 18 | 218 |  | 36 | 164 |  | 39 | 113 | 0 |
| Queue Length 95th (f) | \#148 | 170 |  | 47 | \#385 |  | \#101 | \#274 |  | \#121 | 188 | 2 |
| Turn Bay Length (ft) 331 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 132 | 663 |  | 135 | 634 |  | 90 | 453 |  | 90 | 452 | 537 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced vic Ratio | 0.83 | 0.42 |  | 0.27 | 0.78 |  | 0.79 | 0.78 |  | 0.86 | 0.56 | 0.21 |

Intersection Summary
Area Type: Other
Cycle Length: 80
Actuated Cyde Length: 75.9
Natural Cycie: 80
Control Type: Actuated-Uncoordinated
Maximum vic Ratio: 0.88
Intersection Signal Delay: 43.3
Intersection LOS: D
Intersection Capacity Utifization 70.9\%
ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Spits and Phases: 23: Birch SUCrystal Ave \& NH 102 (E Broadway)


|  | $\cdots$ | $\uparrow$ | 1 | $\cdots$ | $\downarrow$ | ل | 4 | $\pi$ | $\downarrow$ | 1 | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | ${ }^{7}$ | 个个 | \＃ | 凩 | $\uparrow \uparrow$ | 1 | \％ | $\uparrow$ | F | $\dagger$ | $\uparrow$ | ＊ |
| Trafic Volume（vph） | 20 | 230 | 135 | 310 | 220 | 145 | 135 | 170 | 20 | 125 | 290 | 370 |
| Future Volume（vph） | 20 | 230 | 135 | 310 | 220 | 145 | 135 | 170 | 20 | 125 | 290 | 370 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（it） | 150 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ft） | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Uul．Factor | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fil Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Sald．Flow（prot） | 1736 | 3471 | 1553 | 3335 | 3438 | 1538 | 1752 | 1845 | 1568 | 1752 | 1845 | 1568 |
| Fil Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Sald．Flow（perm） | 1736 | 3471 | 1553 | 3335 | 3438 | 1538 | 1752 | 1845 | 1568 | 1752 | 1845 | 1568 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 255 |  |  | 184 |  |  | 327 |  |  | 259 |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（ t ） |  | 639 |  |  | 394 |  |  | 532 |  |  | 387 |  |
| Travel Time（s） |  | 14.5 |  |  | 9.0 |  |  | 12.1 |  |  | 8.8 |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.79 | 0.79 | 0.79 | 0.86 | 0.86 | 0.88 | 0.99 | 0.99 | 0.99 |
| Heary Vehicles（\％） | 4\％ | 4\％ | 4\％ | 5\％ | 5\％ | 5\％ | 3\％ | 3\％ | 3\％ | 3\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 24 | 274 | 161 | 392 | 278 | 184 | 157 | 198 | 23 | 126 | 293 | 374 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（yph） | 24 | 274 | 161 | 392 | 278 | 184 | 157 | 198 | 23 | 126 | 293 | 374 |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | Free | Prot | NA | ptov |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 | 81 |
| Permitted Phases |  | 2 | 2 |  | 6 | 6 |  | 4 | Free |  | 8 |  |
| Detector Pnase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 |  | 3 | 8 | 81 |
| Switch Prase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 6.0 | 8.0 |  | 7.0 | 8.0 |  |
| Minimum Split（s） | 14.0 | 31.0 | 31.0 | 14.0 | 40.0 | 40.0 | 12.0 | 21.0 |  | 13.0 | 21.0 |  |
| Total Split（s） | 14.0 | 31.0 | 31.0 | 23.0 | 40.0 | 40.0 | 15.0 | 21.0 |  | 15.0 | 21.0 |  |
| Total Split（\％） | 15．6\％ | 34．4\％ | 34．4\％ | 25．6\％ | 44．4\％ | 44．4\％ | 16．7\％ | 23．3\％ |  | 16．7\％ | 23．3\％ |  |
| Maximum Green（s） | 8.0 | 25.0 | 25.0 | 17.0 | 34.0 | 34.0 | 9.0 | 15.0 |  | 9.0 | 15.0 |  |
| Yellow Time（s） | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 | 2.0 | 2.0 | 20 | 2.0 | 2.0 | 20 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Leg |  | Lead | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Max | C－Max | C－Max | None | Max | Max | None | None |  | None | None |  |
| Walk Time（s） | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 |  |  | 5.0 |  |
| Flash Dont Walk（s） | 11.0 | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 |  |  | 11.0 |  |
| Pedestrian Calls（\＃hr） | 0 | 0 | 0 |  | 0 | 0 |  | 0 |  |  | 0 |  |
| Act Efft Green（s） | 8.0 | 26.8 | 26.8 | 15.2 | 34.0 | 34.0 | 9.0 | 15.3 | 90.0 | 8.7 | 15.0 | 36.2 |
| Actuated g／C Ratio | 0.09 | 0.30 | 0.30 | 0.17 | 0.38 | 0.38 | 0.10 | 0.17 | 1.00 | 0.10 | 0.17 | 0.40 |
| vic Ratio | 0.16 | 0.27 | 0.25 | 0.70 | 0.21 | 0.26 | 0.90 | 0.63 | 0.01 | 0.74 | 0.95 | 0.48 |
| Control Delay | 40.5 | 25.5 | 1.2 | 42.0 | 19.5 | 4.1 | 88.0 | 45.1 | 0.0 | 66.1 | 80.3 | 8.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


|  | $\cdots$ | $\uparrow$ | $\dagger$ | $\cdots$ | $\downarrow$ | $\downarrow$ | 4 | $\nearrow$ | $\downarrow$ | $\dagger$ | $\checkmark$ | $\psi$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Total Delay | 40.5 | 25.5 | 1.2 | 42.0 | 19.5 | 4.1 | 88.0 | 45.1 | 0.0 | 66.1 | 80.3 | 8.0 |
| LOS | D | c | A | D | B | A | F | D | A | E | F | A |
| Approach Delay |  | 17.8 |  |  | 26.5 |  |  | 60.2 |  |  | 44.0 |  |
| Approach LOS |  | B |  |  | C |  |  | E |  |  | D |  |
| Queue Length 50th (f) | 13 | 63 | 0 | 107 | 55 | 0 | 90 | 106 | 0 | 71 | 167 | 40 |
| Queue Length 95th (ft) | 35 | 90 | 0 | 131 | 72 | 27 | \#191 | 169 | 0 | \#157 | \#323 | 108 |
| Internal Link Dist (ft) |  | 559 |  |  | 314 |  |  | 452 |  |  | 307 |  |
| Turn Bay Length ( t ) | 150 |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 154 | 1032 | 641 | 629 | 1298 | 695 | 175 | 312 | 1568 | 175 |  |  |
| Starvasion Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | O | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced vic Ratio | 0.16 | 0.27 | 0.25 | 0.62 | 0.21 | 0.26 | 0.90 | 0.63 | 0.01 | 0.72 | 0.95 | 0.46 |
| Intersection Summay |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 90
Actuated Cycle Length: 90
Offset: 0 (0\%). Referenced to phase 2NBT, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum w/c Ratio: 0.95
Intersection Signal Delay: 35.6
Intersection Capacity Utilzation 58.3\%

Intersection LOS: D
ICU Level of Service B

Analysis Period (min) 15
\# 95th percentle volume exceeds capacity, queue may be longer.
Queve shown is maximum after two cycles.
Splits and Phases: 15: Folsom Rd/Tsienneto Rd \& Crystal AviNH 28


| Lane Group | $\begin{aligned} & S_{B} \\ & E B L \\ & \hline \end{aligned}$ | $\xrightarrow[\text { EBT }]{\rightarrow}$ | 7 EBR |  | WBT | WBR |  | $\underset{\text { NET }}{ }$ | $\xrightarrow{7}$ |  | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | WBT | WER | NEL | NET | NER | SWL | SWT | SWR |
| Lane Confgurations | \% | 个t |  | ${ }^{*}$ | 个t |  |  | $\uparrow$ | 7 |  | $\uparrow$ | * |
| Traffic Volume (vph) | 50 | 790 | 0 | 0 | 655 | 30 | 5 | 0 | 5 | 50 | d | 245 |
| Future Volume (vph) | 50 | 790 | 0 | 0 | 655 | 30 | 5 | 0 | 5 | 50 | 0 | 245 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 75 |  | 0 | 150 |  | 150 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 1 | 0 |  | 1 |
| Taper Length ( ft ) | 50 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  |  |  | 0.993 |  |  |  | 0.850 |  |  | 0.850 |
| Fil Protected | 0.950 |  |  |  |  |  |  | 0.950 |  |  | 0.950 |  |
| Satd. Flow (prot) | 1687 | 3374 | 0 | 1863 | 3514 | 0 | 0 | 1805 | 1615 | 0 | 1787 | 1599 |
| Fll Permitted | 0.950 |  |  |  |  |  |  | 0.720 |  |  | 0.751 |  |
| Satd. Flow (perm) | 1687 | 3374 | 0 | 1863 | 3514 | 0 | 0 | 1368 | 1615 | 0 | 1413 | 1599 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Sald. Flow (RTOR) |  |  |  |  | 6 |  |  |  | 109 |  |  | 227 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 277 |  |  | 755 |  |  | 218 |  |  | 433 |  |
| Travel Time (s) |  | 6.3 |  |  | 17.2 |  |  | 5.0 |  |  | 9.8 |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.92 | 0.92 | 0.92 | 0.50 | 0.50 | 0.50 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles (\%) | 7\% | 7\% | 7\% | 2\% | 2\% | 2\% | 0\% | 0\% | 0\% | 1\% | 1\% | 1\% |
| Adj. Flow (vph) | 60 | 952 | 0 | 0 | 712 | 33 | 10 | 0 | 10 | 56 | 0 | 272 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 60 | 952 | 0 | 0 | 745 | 0 | 0 | 10 | 10 | 0 | 56 | 272 |
| Tum Type | Prot | NA |  | Prot | NA |  | custom | NA | custom | Perm | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  |  |  |  |  | 4 |  |
| Permitted Phases |  |  |  |  | 6 |  | 8 | 8 | 8 | 4 |  | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 8 | 8 | 8 | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 8.0 |  | 5.0 | 8.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 14.0 | 46.0 |  | 11.0 | 43.0 |  | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 |
| Total Split (s) | 14.0 | 46.0 |  | 11.0 | 43.0 |  | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 |
| Total Spit (\%) | 15.6\% | 51.1\% |  | 12.2\% | 47.8\% |  | 36.7\% | 35.7\% | $36.7 \%$ | 36.7\% | 36.7\% | 36.7\% |
| Maximum Green (s) | 8.0 | 40.0 |  | 5.0 | 37.0 |  | 27.0 | 27.0 | 27.0 | 27.0 | 27.0 | 27.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 6.0 | 6.0 |  | 6.0 | 6.0 |
| Lead/Lag | Lead | Lag |  | Lead | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recal Mode | None | C-Max |  | None | None |  | None | None | None | None | None | None |
| Act Effet Green (s) | 9.2 | 67.7 |  |  | 55.2 |  |  | 10.3 | 10.3 |  | 10.3 | 10.3 |
| Actuated gic Raso | 0.10 | 0.75 |  |  | 0.61 |  |  | 0.11 | 0.11 |  | 0.11 | 0.11 |
| vic Ratio | 0.35 | 0.38 |  |  | 0.35 |  |  | 0.06 | 0.04 |  | 0.35 | 0.71 |
| Control Delay | 42.8 | 4.9 |  |  | 12.9 |  |  | 33.0 | 0.2 |  | 40.6 | 18.9 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay | 42.8 | 4.9 |  |  | 12.9 |  |  | 33.0 | 0.2 |  | 40.6 | 18.9 |
| LOS | D | A |  |  | B |  |  | C | A |  | D | B |
| Approach Delay |  | 7.1 |  |  | 129 |  |  | 16.6 |  |  | 22.6 |  |



Area Type: Other
Cyde Length: 90
Actuated Cycle Length: 90
Offset $63(70 \%)$, Referenced to phase 2:EBT, Start of Green
Natural Cycle: 90
Control Type: Actuated-Ccordinated
Maximum vic Rato: 0.71
Intersection Signal Delay: 11.7
Intersection LOS: B
Intersection Capacity Utilization 53.4\% ICU Level of Service A
Analysis Period (min) 15
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 6: ApplebeesLinlew Dr \& NH 28


|  | EBL | $\overrightarrow{S B}$ | EBR | WBL |  | N | 4 | $\begin{array}{r}\uparrow \\ \hline 8\end{array}$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | VBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configuratons | ${ }^{17}$ | 个t |  | \％ | 个t |  | \％ | な |  | ${ }_{1}$ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 100 | 630 | 5 | 5 | 610 | 220 | 10 | 5 | 5 | 180 | ${ }^{4}$ | 100 |
| Future Volume（vph） | 100 | 630 | 5 | 5 | 610 | 220 | 10 | 5 | 5 | 180 | 5 | 100 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length（ft） | 150 |  | 150 | 150 |  | 150 |  |  |  | 0 |  | 150 |
| Storage Lanes | 2 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 |
| Taper Length（fi） | 200 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Ufil．Factor | 0.97 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt |  | 0.999 |  |  | 0.960 |  |  | 0.925 |  |  |  | 0.850 |
| Flit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.955 |  |
| Satd．Flow（prot） | 3303 | 3402 | 0 | 1736 | 3332 | 0 | 1805 | 1758 | 0 | 1665 | 1674 | 1568 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.955 |  |
| Satd．Flow（perm） | 3303 | 3402 | 0 | 1736 | 3332 | 0 | 1805 | 1758 | 0 | 1665 | 1674 | 1568 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 1 |  |  | 79 |  |  | 7 |  |  |  | 111 |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（th） |  | 412 |  |  | 486 |  |  | 151 |  |  | 343 |  |
| Travel Time（s） |  | 9.4 |  |  | 11.0 |  |  | 3.4 |  |  | 7.8 |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.97 | 0.97 | 0.97 | 0.67 | 0.67 | 0.67 | 0.90 | 0.90 | 0.90 |
| Heavy Vehides（\％） | 6\％ | 6\％ | 6\％ | 4\％ | 4\％ | 4\％ | 0\％ | 0\％ | 0\％ | 3\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 120 | 759 | 6 | 5 | 629 | 227 | 15 | ＋ | 7 | 200 | 6 | 111 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  | 49\％ |  |  |
| Lane Group Flow（vph） | 120 | 765 | 0 | 5 | 856 | 0 | 15 | 14 | 0 | 102 | 104 | 111 |
| Turn Type | Prot | NA |  | Prot | NA |  | Split | NA |  | Splt | NA | ptoov |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | ， | 4 | 45 |
| Permitted Phases |  |  |  |  |  |  |  | 3 |  |  |  |  |
| Detector Phase Switch Pnase | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 | 45 |
| Minimum initial（s） | 5.0 | 8.0 |  | 5.0 | 8.0 |  | 5.0 | 5.0 |  | 8.0 | 8.0 |  |
| Minimum Solit（s） | 14.0 | 53.0 |  | 11.0 | 50.0 |  | 11.0 | 11.0 |  | 15.0 | 15.0 |  |
| Total Split（s） | 14.0 | 53.0 |  | 11.0 | 50.0 |  | 11.0 | 11.0 |  | 15.0 | 15.0 |  |
| Total Split（\％） | 15．6\％ | 58．9\％ |  | 12．2\％ | 55．6\％ |  | 12．2\％ | 12．2\％ |  | 16．7\％ | 16．7\％ |  |
| Maximum Green（s） | 8.0 | 47.0 |  | 5.0 | 44.0 |  | 5.0 | 5.0 |  | 9.0 | 9.0 |  |
| Yellow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 20 |  | 2.0 | 20 |  | 2.0 | 20 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／ag | Lead | Lag |  | Lead | Lag |  | Lead | Lead |  | Lag | Lag |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehide Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | Min |  | None | C．Min |  | None | None |  | None | None |  |
| Walk Time（s） |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 | ． |
| Flash Dont Walk（s） |  | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Cals（\＃／hr） |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | ． |  |
| Act Effict Green（s） | 8.0 | 57.4 |  | 5.6 | 45.5 |  | 6.3 | 6.3 |  | 10.7 | 10.7 | 24.7 |
| Actuated g／C Ratio | 0.09 | 0.64 |  | 0.06 | 0.51 |  | 0.07 | 0.07 |  | 0.12 | 0.12 | 0.27 |
| vic Ratio | 0.41 | 0.35 |  | 0.05 | 0.50 |  | 0.12 | 0.11 |  | 0.52 | 0.53 | 0.22 |
| Control Delay | 42.9 | 10.3 |  | 61.6 | 10.1 |  | 40.8 | 30.0 |  | 46.5 | 46.7 | 6.0 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |



Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset $0(0 \%)$, Referenced to phase 6:WBT, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.53
Intersection Signal Delay: 15.9
Intersection LOS: B
Intersection Capacity Utilization 54.8\% ICU Level of Service A
Analysis Period (min) 15
$m$ Volume for 95 th percenble queue is metered by upstream signal.
Splits and Phases: $\quad 9:$ VIP Dr/Ashleigh Dr \& NH 28


| Lane Group | NBL | NBT | NBR | S8L | S8T | SBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\dagger$ |  | ${ }^{*}$ | $\uparrow$ | $\overline{7}$ | \% | $\dagger$ |  | \% | 今 |  |
| Traffic Volume (vph) | 100 | 220 | 20 | 25 | 210 | 255 | 120 | 100 | 80 | 80 | 270 | 90 |
| Future Volume (vph) | 100 | 220 | 20 | 25 | 210 | 255 | 120 | 100 | 80 | 80 | 270 | 90 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (f) | 150 |  | 150 | 150 |  | 150 | 150 |  | 150 | 150 |  | 150 |
| Storage Lanes | 1 |  | , | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.988 |  |  |  | 0.850 |  | 0.933 |  |  | 0.963 |  |
| Fil Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Sald. Flow (prot) | 1752 | 1823 | 0 | 1736 | 1827 | 1553 | 1770 | 1738 | 0 | 1787 | 1812 | 0 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1752 | 1823 | 0 | 1736 | 1827 | 1553 | 1770 | 1738 | 0 | 1787 | 1812 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 5 |  |  |  | 202 |  | 48 |  |  | 20 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (t) |  | 481 |  |  | 347 |  |  | 479 |  |  | 371 |  |
| Travel Time (s) |  | 10.9 |  |  | 7.9 |  |  | 10.9 |  |  | 8.4 |  |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.81 | 0.81 | 0.81 | 0.68 | 0.68 | 0.68 | 0.78 | 0.78 | 0.78 |
| Heary Vehicles (\%) | 3\% | 3\% | 3\% | 4\% | 4\% | 4\% | 2\% | 2\% | $2 \%$ | 1\% | 1\% | 1\% |
| Adj. Flow (vph) | 122 | 268 | 24 | 31 | 259 | 315 | 176 | 147 | 118 | 103 | 346 | 115 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (yph) | 122 | 292 | 0 | 31 | 259 | 315 | 176 | 265 | 0 | 103 | 461 | 0 |
| Tum Type | Prot | NA |  | Prot | NA | pt+ov | Prot | NA |  | Prot | NA |  |
| Protecled Phases | 1 | 6 |  | 5 | 2 | 23 | 3 | . |  | 7 | 4 |  |
| Permitled Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector Phase | 1 | 6 |  | 5 | 2 | 23 | 3 | 8 |  | 7 | 4 |  |
| Switch Prase |  |  |  |  |  |  |  |  |  |  |  |  |
| Mnimum lnitial (s) | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Minimum Split (s) | 14.0 | 20.0 |  | 14.0 | 20.0 |  | 14.0 | 20.0 |  | 14.0 | 20.0 |  |
| Total Solit (s) | 14.0 | 24.0 |  | 14.0 | 24.0 |  | 15.0 | 26.0 |  | 16.0 | 27.0 |  |
| Total Split (\%) | 17.5\% | 30.0\% |  | 17.5\% | 30.0\% |  | 18.8\% | 32.5\% |  | 20.0\% | 33.8\% |  |
| Maximum Green (s) | 8.0 | 18.0 |  | 8.0 | 18.0 |  | 9.0 | 20.0 |  | 10.0 | 21.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Al-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 20 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Leadhag | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehide Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | C-Max |  | None | None |  | None | None |  |
| Act Effl Green (s) | 8.0 | 26.5 |  | 8.0 | 18.1 | 33.1 | 9.0 | 23.4 |  | 9.2 | 20.9 |  |
| Actuated g/C Ratio | 0.10 | 0.33 |  | 0.10 | 0.23 | 0.41 | 0.11 | 0.29 |  | 0.12 | 0.26 |  |
| vic Ratio | 0.70 | 0.48 |  | 0.18 | 0.63 | 0.41 | 0.88 | 0.49 |  | 0.50 | 0.95 |  |
| Control Delay | 57.5 | 26.8 |  | 35.8 | 35.7 | 7.9 | 77.5 | 24.2 |  | 41.9 | 59.4 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 57.5 | 26.8 |  | 35.8 | 35.7 | 7.9 | 77.5 | 24.2 |  | 41.9 | 59.4 |  |
| LOS | E | C |  | D | D | A | E | c |  | D | E |  |
| Approach Delay |  | 35.9 |  |  | 21.2 |  |  | 45.5 |  |  | 56.2 |  |


|  | \# | $\uparrow$ | 1 | $\cdots$ | $\downarrow$ | \} | 4 | $\not$ | $\downarrow$ | $\downarrow$ | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | S8L | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Approach LOS |  | D |  |  | C |  |  | D |  |  | E |  |
| Queve Length 50th (ft) | 60 | 99 |  | 15 | 117 | 35 | 88 | 94 |  | 49 | 217 |  |
| Queue Length 95th (ft) | \#119 | 193 |  | 36 | 171 | 71 | \#126 | 114 |  | 82 | \#309 |  |
| Internal Link Dist (ft) |  | 401 |  |  | 267 |  |  | 399 |  |  | 291 |  |
| Tum Bay Length (ft) | 150 |  |  | 150 |  | 150 | 150 |  |  | 150 |  |  |
| Base Capacity (yph) | 175 | 607 |  | 173 | 414 | 761 | 199 | 543 |  | 223 | 490 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 |  |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced vic Ratio | 0.70 | 0.48 |  | 0.18 | 0.63 | 0.41 | 0.88 | 0.49 |  | 0.46 | 0.94 |  |

## ntersection Summary

```
Area Type:
```


## Other

Cycle Length: 80
Acluated Cycle Length: 80
Offset: 0 (0\%), Referenced to phase 2:S8T, Start of Green
Natural Cycle: 80
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.95
Intersection Signal Delay: 39.2
Intersection Capacity Utiization $65.8 \%$
Intersection LOS: D
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splts and Phases: $\quad$ 1: Tsienneto Rd \& NH 28 Byp S/NH 28 Byp N


APPENDIX G-2: HCM AND SYNCHRO PRINTOUTS - SIGNALIZED INTERSECTION CAPACITY ANALYSES - 2015 PM PEAK HOURS SYNCHRO PRINTOUTS


|  | $\Rightarrow \rightarrow$ | $\leftarrow$ | $\pm \downarrow$ | $\downarrow$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | E8L EBT | WBT | WBR SBL | SER | 69 |  |
| Approach LOS | 8 | A | E |  |  |  |
| Queue Length 50th (ti) | 186 | 15 | 214 | -392 |  |  |
| Queue Length 95th (ti) | 230 | 18 | 317 | \#630 |  |  |
| Internal Link Dist (tt) | 237 | 186 | 351 |  |  |  |
| Turn Bay Length (ti) |  |  |  |  |  |  |
| Base Capacity (yph) | 2323 | 2323 | 438 | 650 |  |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |  |  |
| Spilback Cap Reducth | 0 | 0 | 0 | 0 |  |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |  |  |
| Reduced vic Ratio | 0.44 | 0.41 | 0.69 | 1.08 |  |  |

## Intersection Summary

```
Area Type:
    Other
```

Cycle Length: 120
Actuated Cycle Length: 120
Offset $0(0 \%)$, Referenced to phase 2:EBWB, Start of Green
Natural Cycle: 95
Control Type: Actuated-Coordinated
Maximum vic Ratio: 1.08
Intersection Signal Delay: $28.5 \quad$ Intersection LOS: C
Intersection Capacity Utifzation 73.4\% ICU Level of Service D
Analysis Period (min) 15
~ Volume exceeds capacity, queue is theoreticaly infinite.
Queve shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer. Queve shown is maximum after two cycles.

Solits and Phases: 7: NH $102 \&$ Exit 4 S8 Off

| $\stackrel{H}{\leftrightarrows}$ |  | f8 |
| :---: | :---: | :---: |
|  |  | 26 s |
|  |  |  |


|  | 9 | $\cdots$ | 1 | $\cdots$ | $\downarrow$ | \% | $\triangle$ | $\downarrow$ | $\downarrow$ | 4 | $\cdots$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL2 | NBL | NBR | SEL | SER | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | 714 |  | F |  |  | \% | ¢ $\uparrow$ |  |  | 个4 | \% |
| Traffic Volume (vph) | 580 | 0 | 605 | 0 | 0 | 475 | 740 | 0 | 0 | 485 | 0 |
| Future Volume (vph) | 580 | 0 | 605 | 0 | 0 | 475 | 740 | 0 | O | 485 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Fit |  |  | 0.850 |  |  |  |  |  |  |  |  |
| Fit Protected | 0.950 |  |  |  |  | 0.950 |  |  |  |  |  |
| Satd. Flow (prot) | 3467 | 0 | 1599 | 0 | 0 | 1770 | 3539 | 0 | 0 | 3539 | 1863 |
| Fit Permitted | 0.950 |  |  |  |  | 0.950 |  |  |  |  |  |
| Satd. Flow (perm) | 3467 | 0 | 1599 | 0 | 0 | 1770 | 3539 | 0 | 0 | 3539 | 1863 |
| Right Turn on Red |  |  | Yes |  |  |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 499 |  |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 25 |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( f ) |  | 347 |  | 390 |  |  | 361 |  |  | 346 |  |
| Travel Time (s) |  | 9.5 |  | 8.9 |  |  | 8.2 |  |  | 7.9 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.96 | 0.96 | 0.96 | 0.87 | 0.87 | 0.87 |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Adj. Flow (vph) | 630 | 0 | 658 | 0 | 0 | 495 | 771 | 0 | 0 | 557 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (yph) | 630 | 0 | 658 | 0 | 0 | 495 | 771 | 0 | 0 | 557 | 0 |
| Turn Type | Prot |  | Free |  |  | Prot | NA |  |  | NA | Free |
| Protected Phases | 2 |  |  |  |  | 7 | 4 |  |  | 8 |  |
| Permitted Phases |  |  | Free |  |  |  | 7 |  |  |  | Free |
| Detector Phase | 2 |  |  |  |  | 7 | 4 |  |  | 8 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 |  |  |  |  | 5.0 | 10.0 |  |  | 10.0 |  |
| Minimum Split (s) | 9.5 |  |  |  |  | 9.5 | 66.0 |  |  | 66.0 |  |
| Total Split (s) | 38.0 |  |  |  |  | 44.0 | 82.0 |  |  | 38.0 |  |
| Total Split (\%) | 31.7\% |  |  |  |  | 36.7\% | 68.3\% |  |  | 31.7\% |  |
| Maximum Green (s) | 33.5 |  |  |  |  | 39.5 | 76.0 |  |  | 32.0 |  |
| Yellow Time (s) | 3.5 |  |  |  |  | 3.5 | 4.0 |  |  | 4.0 |  |
| All-Red Time (s) | 1.0 |  |  |  |  | 1.0 | 20 |  |  | 20 |  |
| Lost Time Acjust (s) | 0.0 |  |  |  |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.5 |  |  |  |  | 4.5 | 6.0 |  |  | 6.0 |  |
| LeadLag |  |  |  |  |  | Lead |  |  |  | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  | Yes |  |  |  | Yes |  |
| Vehicle Extension (s) | 3.0 |  |  |  |  | 3.0 | 3.0 |  |  | 3.0 |  |
| Recall Mode | C-Max |  |  |  |  | None | None |  |  | None |  |
| Walk Time (s) |  |  |  |  |  |  | 7.0 |  |  | 7.0 |  |
| Flash Dont Walk (s) |  |  |  |  |  |  | 11.0 |  |  | 11.0 |  |
| Pedestrian Calls (\#hr) |  |  |  |  |  |  | 0 |  |  | 0 |  |
| Act Effict Green (s) | 43.4 |  | 120.0 |  | , | 36.7 | 66.1 |  |  | 24.9 |  |
| Actuated g/C Ratio | 0.36 |  | 1.00 |  |  | 0.31 | 0.55 |  |  | 0.21 |  |
| vic Ratio | 0.50 |  | 0.41 |  |  | 0.91 | 0.40 |  |  | 0.76 |  |
| Control Delay | 33.3 |  | 0.8 |  |  | 62.3 | 19.5 |  |  | 51.5 |  |
| Queue Delay | 0.0 |  | 0.0 |  |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 33.3 |  | 0.8 |  |  | 62.3 | 19.5 |  |  | 51.5 |  |
| LOS | C |  | A |  |  | E | B |  |  | D |  |
| Approach Delay |  | 16.7 |  |  |  |  | 36.2 |  |  | 51.5 |  |


|  | $\cdots$ | 1 | 7 | $\cdots$ | \} | $y$ | $\pi$ | $\uparrow$ | $\downarrow$ | $\checkmark$ | k |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL2 | NBL | NBR | SEL | SER | NEL | NET | NER | SWL | SWT | SWR |
| Approach LOS |  | 8 |  |  |  |  | D |  |  | D |  |
| Queue Length 50it (ft) | 202 |  | 0 |  |  | 374 | 200 |  |  | 215 |  |
| Queue Length 95ih (ti) | 281 |  | 0 |  |  | \#548 | 242 |  |  | 250 |  |
| Internal Link Dist (ft) |  | 267 |  | 310 |  |  | 281 |  |  | 266 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (yph) | 1253 |  | 1599 |  |  | 582 | 2241 |  |  | 943 |  |
| Starvation Cap Reductn | 0 |  | 0 |  |  | 0 | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 |  | 0 |  |  | 0 | , |  |  | 0 |  |
| Storage Cap Reductn | 0 |  | 0 |  |  | 0 | 0 |  |  | 0 |  |
| Reduced vic Ratio | 0.50 |  | 0.41 |  |  | 0.85 | 0.34 |  |  | 0.59 |  |

## Intersection Summary

Area Type: Other

Cycle Length: 120
Actuated Cycle Length: 120
Offset: $0(0 \%)$, Referenced to phase 2:NBL and 6: Start of Green
Natural Cycle: 135
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.91
Intersection Signal Delay: 30.9 Intersection LOS: C
Intersection Capacity Ubiliza5ion 68.4\% ICU Level of Service C
Analysis Period (min) 15
\# 95th percentile wolume exceeds capacity, queve may be longer.
Queue shown is maximum after two cydes.

Splits and Phases: 11: Exit 4 NB Off \& NH 102


|  | 3 | $\rightarrow$ | $\nabla$ | $\checkmark$ | $\longleftarrow$ | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | VBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 $\uparrow$ | 1 | \% | 44 |  |  |  |  | \%* |  | \% |
| Traffic Votume (vph) | 0 | 650 | 280 | 135 | 490 | 0 | 0 | 0 | 0 | 645 | 0 | 265 |
| Future Volume (vph) | 0 | 650 | 280 | 135 | 490 | 0 | 0 | O | 0 | 645 | 0 | 265 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( f ) | - |  | 0 | 500 |  | 0 | 0 |  | 0 | 100 |  | 0 |
| Storage Lanes | 0 |  | 1 | 1 |  | 0 | 0 |  | 0 | 2 |  | 1 |
| Taper Length (9) | 25 |  |  | 30 |  |  | 25 |  |  | 25 |  |  |
| Lane Uell. Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 |
| Fft |  |  | 0.850 |  |  |  |  |  |  |  |  | 0.850 |
| Fll Protected |  |  |  | 0.950 |  |  |  |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 3471 | 1553 | 1719 | 3438 | 0 | 0 | 0 | 0 | 3367 | 0 | 1553 |
| Flt Permitted |  |  |  | 0.950 |  |  |  |  |  | 0.950 |  |  |
| Sald. Flow (perm) | 0 | 3471 | 1553 | 1719 | 3438 | 0 | 0 | 0 | 0 | 3367 | 0 | 1553 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 322 |  |  |  |  |  |  |  |  | 276 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 35 |  |
| Link Distance (t) |  | 410 |  |  | 699 |  |  | 485 |  |  | 444 |  |
| Travel Time (s) |  | 9.3 |  |  | 15.9 |  |  | 11.0 |  |  | 8.6 |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.86 | 0.86 | 0.86 | 0.92 | 0.92 | 0.92 | 0.91 | 0.91 | 0.91 |
| Heavy Vehicles (\%) | 4\% | 4\% | 4\% | 5\% | 5\% | 5\% | 2\% | 2\% | 2\% | 4\% | 4\% | 4\% |
| Ad. Flow (vph) | 0 | 747 | 322 | 157 | 570 | 0 | 0 | 0 | 0 | 709 | 0 | 291 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 747 | 322 | 157 | 570 | 0 | 0 | 0 | 0 | 709 | 0 | 291 |
| Turn Type |  | NA | Free | Prot | NA |  |  |  |  | Prot |  | Prot |
| Protected Prases |  | 2 |  | 1 | 6 |  |  |  |  | 4 |  | 4 |
| Permitted Phases |  |  | Free |  | 1 |  |  |  |  |  |  |  |
| Delector Phase |  | 2 |  | 1 | 6 |  |  |  |  | 4 |  | 4 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Inital ( s ) |  | 5.0 |  | 4.0 | 5.0 |  |  |  |  | 3.0 |  | 3.0 |
| Minimum Spit (s) |  | 41.0 |  | 10.0 | 41.0 |  |  |  |  | 36.0 |  | 36.0 |
| Total Split (s) |  | 36.0 |  | 24.0 | 60.0 |  |  |  |  | 40.0 |  | 40.0 |
| Total Split (\%) |  | 36.0\% |  | 24.0\% | 60.0\% |  |  |  |  | 40.0\% |  | 40.0\% |
| Maximum Green (s) |  | 30.0 |  | 18.0 | 54.0 |  |  |  |  | 34.0 |  | 34.0 |
| Yellow Time (s) |  | 4.0 |  | 4.0 | 4.0 |  |  |  |  | 4.0 |  | 4.0 |
| Al-Red Time (s) |  | 2.0 |  | 2.0 | 2.0 |  |  |  |  | 2.0 |  | 2.0 |
| Lost Time Adjust (s) |  | 0.0 |  | 0.0 | 0.0 |  |  |  |  | 0.0 |  | 0.0 |
| Total Lost Time (s) Leadhag |  | 6.0 |  | 6.0 | 6.0 |  |  |  |  | 6.0 |  | 6.0 |
| Lead/Lag Lag Ootimize? |  | Lag |  | Lead |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  | Yes |  | Yes |  |  |  |  |  |  |  |  |
| Vehide Extension (s) |  | 4.0 |  | 4.0 | 4.0 |  |  |  |  | 4.0 |  | 4.0 |
| Recall Mode |  | C.Min |  | None | C-Min |  |  |  |  | None |  | None |
| Walk Time (s) |  | 7.0 |  |  | 7.0 |  |  |  |  | 7.0 |  | 7.0 |
| Flash Dont Walk (s) Pedestrian Calls (\#hr) |  | 11.0 |  |  | 11.0 |  |  |  |  | 11.0 |  | 11.0 |
| Pedestrian Calls (\#/hr) Act Effict Green (s) |  | 0 38.4 | 100.0 |  | 0 592 |  |  |  |  | 0 288 |  | 0 |
| Actuated g/C Ratio |  | 0.38 | 1.00 | 0.15 | 59.2 0.59 |  |  |  |  | 28.8 0.29 |  | 28.8 |
| wic Ratio |  | 0.56 | 0.21 | 0.62 | 0.28 |  |  |  |  | 0.73 |  | 0.45 |
| Control Delay |  | 27.8 | 0.3 | 45.3 | 4.8 |  |  |  |  | 36.5 |  | 6.2 |
| Queue Delay |  | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  | 0.0 |  | 0.0 |



Intersection Summary
Area Type: Other
Cycle Length: 100
Actuated Cycle Length: 100
Offset $48(48 \%)$, Referenced to phase 2:EBT and $6: W B T$, Start of Green
Natural Cycle: 90
Control Type: Actualed-Coordinated
Maximum vic Rato: 0.73
Intersection Signal Delay: 20.9
Intersection LOS: C
Intersection Capacity Utiliza5on 58.8\% ICU Level of Service B
Analysis Period (min) 15
Spits and Phases: 3 : NH 28 \& Exit 5 SB Off


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



Intersection Summary
Area Type: Other
Cycle Length: 100
Actuated Cycle Length: 100
Offset: $0(0 \%)$, Referenced to phase 2EBT and 6.WBT, Start of Green
Natural Cycle: 90
Control Type: Actuated-Coordinated
Maximum vic Ratio: 0.77
Intersection Signal Delay: $21.4 \quad$ Intersection LOS: C
Intersection Capacity Utilization 58.8\% ICU Level of Service 8
Analysis Period (min) 15
Splits and Phases: 2: Exit 5 NB Off \& NH 28


| Lane Group | $\begin{aligned} & \text { G } \\ & \text { SB } \\ & \text { SEL } \end{aligned}$ | $\lambda$ <br> SET | ) <br> SER | $m_{N B} k$ |  |  | VEB <br> NEL | NET |  |  | SWT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | NWL | NWT |  |  |  |  |  |  |  |
| Lane Configurations |  | ¢ |  |  | 4 |  |  | F |  |  | $\uparrow$ |  |
| Traffic Volume (vph) | 15 | 50 | 5 | 230 | 0 | 100 | 0 | 760 | 150 | 15 | 415 | 0 |
| Future Volume (vph) | 15 | 50 | 5 | 230 | 0 | 100 | 0 | 760 | 150 | 15 | 415 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.990 |  |  | 0.959 |  |  | 0.978 |  |  |  |  |
| Fit Protected |  | 0.989 |  |  | 0.966 |  |  |  |  |  | 0.998 |  |
| Satd. Flow (prot) | 0 | 1842 | 0 | 0 | 1743 | 0 | 0 | 1822 | 0 | 0 | 1841 | 0 |
| Flt Permitted |  | 0.902 |  |  | 0.740 |  |  |  |  |  | 0.620 |  |
| Satd. Flow (perm) | 0 | 1680 | 0 | 0 | 1335 | 0 | 0 | 1822 | 0 | 0 | 1144 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 6 |  |  | 55 |  |  | 24 |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (fi) |  | 170 |  |  | 373 |  |  | 245 |  |  | 336 |  |
| Travel Time (s) |  | 3.9 |  |  | 8.5 |  |  | 5.6 |  |  | 7.6 |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.98 | 0.98 | 0.98 | 0.95 | 0.95 | 0.95 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 2\% | 2\% | 2\% | 3\% | 3\% | 3\% |
| Adj. Flow (yph) | 18 | 60 | 6 | 235 | 0 | 102 | 0 | 800 | 158 | 17 | 466 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 84 | 0 | 0 | 337 | 0 | 0 | 958 | 0 | 0 | 483 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  |  | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 2 |  |  | 1 |  |  | 1 |  |
| Permitted Phases | 2 |  |  | 2 |  |  |  |  |  | 1 |  |  |
| Detector Phase | 2 | 2 |  | 2 | 2 |  |  | 1 |  | 1 | 1 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Inital (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  |  | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  |  | 36.0 |  | 36.0 | 36.0 |  |
| Total Split (\%) | 40.0\% | 40.0\% |  | 40.0\% | 40.0\% |  |  | 60.0\% |  | $60.0 \%$ | 60.0\% |  |
| Maximum Green (s) | 18.0 | 18.0 |  | 18.0 | 18.0 |  |  | 30.0 |  | 30.0 | 30.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  |  | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| LeadLag | Lag | Lag |  | Lag | Lag |  |  | Lead |  | Lead | Lead |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  |  | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | Min | Mn |  | Min | Min |  |  | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#hr) | 0 | 0 |  | 0 | 0 |  |  | , |  | 0 | 0 |  |
| Act Efft Green (s) |  | 15.8 |  |  | 15.8 |  |  | 30.1 |  |  | 30.1 |  |
| Actuated g/C Ratio |  | 0.27 |  |  | 0.27 |  |  | 0.52 |  |  | 0.52 |  |
| vic Ratio |  | 0.18 |  |  | 0.84 |  |  | 1.00 |  |  | 0.81 |  |
| Control Delay |  | 15.9 |  |  | 36.6 |  |  | 47.1 |  |  | 26.8 |  |
| Queue Delay |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay |  | 15.9 |  |  | 36.6 |  |  | 47.1 |  |  | 26.8 |  |
| LOS |  | B |  |  | D |  |  | D |  |  | c |  |
| Approach Delay |  | 15.9 |  |  | 36.6 |  |  | 47.1 |  |  | 26.8 |  |


|  | $\cdots$ | 2 | $\cdots$ | k | $\pi$ |  | $\lambda$ | 7 | 4 | $\checkmark$ | $k$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL SET | SER | NWL | NWT | NVR | NEL | NET | NER | SWL | SWT | SWR |
| Approach LOS | 8 |  |  | D |  |  | D |  |  | C |  |
| Queue Length 50th ( t ) | 21 |  |  | 91 |  |  | -382 |  |  | 140 |  |
| Queve Length 95th (t) | 45 |  |  | \#215 |  |  | \# 499 |  |  | \#306 |  |
| Internal Link Dist (ti) | 90 |  |  | 293 |  |  | 165 |  |  | 256 |  |
| Turn Bay Length ( $t$ ) |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 528 |  |  | 454 |  |  | 959 |  |  | 595 |  |
| Starvation Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Reduced vic Ratio | 0.16 |  |  | 0.74 |  |  | 1.00 |  |  | 0.81 |  |


| Intersection Summary |  |
| :--- | :--- |
| Area Type: | Other |

Cycle Length: 60
Actuated Cycle Length: 57.9
Natural Cycle: 80
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 1.00
Intersection Signal Delay: $38.5 \quad$ Intersection LOS: D
Intersection Capacity Utiization 95.4\% ICU Level or Service F
Analysis Period (min) 15

- Volume exceeds capacity, queue is theoreticaly infinite. Queue shown is maximum after two cycles.
\# 95th percentle volume exceeds capacity, queue may be longer.
Queue shown is maximum ater two cycles.
Solits and Phases: 4: NH 102 \& FordwayN. High St


|  | $\cdots$ | $\uparrow$ | 1 | W | $\downarrow$ | ل | $\mathcal{E}_{\text {E }}$ | $\ngtr$ | $\uparrow$ | $\boldsymbol{f}_{w / s}$ | 4 | $\vartheta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Confgurations | 7 | ち |  | \％ | $\uparrow$ | ＊ | $\dagger$ | ち |  | ＊ | 今 |  |
| Traffic Volume（vph） | 70 | 295 | 35 | 135 | 340 | 150 | 135 | 410 | 40 | 75 | 250 | 65 |
| Future Volume（voh） | 70 | 295 | 35 | 135 | 340 | 150 | 135 | 410 | 40 | 75 | 250 | 65 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.984 |  |  |  | 0.850 |  | 0.987 |  |  | 0.969 |  |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Sald．Flow（prot） | 1752 | 1815 | 0 | 1752 | 1845 | 1568 | 1787 | 1857 | 0 | 1787 | 1823 | 0 |
| Fit Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 1752 | 1815 | 0 | 1752 | 1845 | 1568 | 1787 | 1857 | 0 | 1787 | 1823 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 7 |  |  |  | 161 |  | 6 |  |  | 15 |  |
| Link Speed（mph） |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance（t） |  | 361 |  |  | 411 |  |  | 477 |  |  | 530 |  |
| Travel Time（s） |  | 8.2 |  |  | 9.3 |  |  | 10.8 |  |  | 12.0 |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.93 | 0.93 | 0.93 | 0.95 | 0.95 | 0.95 | 0.94 | 0.94 | 0.94 |
| Heavy Vehides（\％） | 3\％ | 3\％ | 3\％ | 3\％ | 3\％ | 3\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ | 1\％ |
| Adj．Flow（yph） | 77 | 324 | 38 | 145 | 366 | 161 | 142 | 432 | 42 | 80 | 266 | 69 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（yph） | 77 | 362 | 0 | 145 | 366 | 161 | 142 | 474 | 0 | 80 | 335 | 0 |
| Turn Type | Prot | NA |  | Prot | NA | pm＋ov | Prot | NA |  | Prot | NA |  |
| Protected Phases | 3 | 8 |  | 7 | 4 | 5 | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  |  |  |  | 4 |  |  |  |  |  |  |
| Detector Phase | 3 | 8 |  | 7 | 4 | 5 | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initiol（s） | 4.0 | 5.0 |  | 4.0 | 10.0 | 4.0 | 4.0 | 10.0 |  | 4.0 | 9.0 |  |
| Minimum Spit（s） | 17.0 | 24.0 |  | 11.0 | 24.0 | 16.0 | 16.0 | 24.0 |  | 11.0 | 24.0 |  |
| Total Split（s） | 17.0 | 27.0 |  | 15.0 | 25.0 | 16.0 | 16.0 | 32.0 |  | 11.0 | 27.0 |  |
| Total Split（\％） | 20．0\％ | 31．8\％ |  | 17．6\％ | 29．4\％ | 18．8\％ | 18．8\％ | 37．6\％ |  | 12．9\％ | 31．8\％ |  |
| Maximum Green（s） | 11.0 | 21.0 |  | 9.0 | 19.0 | 10.0 | 10.0 | 26.0 |  | 5.0 | 21.0 |  |
| Yelow Time（s） | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time（s） | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead／ag | Lead | Lag |  | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  |
| Lead－Lag Opoimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 30 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None | None | None | C－Max |  | None | None |  |
| Act Effer Green（s） | 8.8 | 19.5 |  | 8.9 | 22.0 | 37.6 | 9.7 | 29.5 |  | 5.6 | 22.9 |  |
| Actuated gic Ratio | 0.10 | 0.23 |  | 0.10 | 0.26 | 0.44 | 0.11 | 0.35 |  | 0.07 | 0.27 |  |
| vic Ratio | 0.43 | 0.86 |  | 0.79 | 0.77 | 0.21 | 0.70 | 0.73 |  | 0.68 | 0.67 |  |
| Control Delay | 42.5 | 51.3 |  | 67.9 | 43.3 | 3.5 | 55.8 | 34.2 |  | 69.5 | 35.1 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 42.5 | 51.3 |  | 67.9 | 43.3 | 3.5 | 55.8 | 34.2 |  | 69.5 | 35.1 |  |
| LOS | D | 0 |  | E | D | A | E | C |  | E | D |  |
| Approach Delay |  | 49.7 |  |  | 39.1 |  |  | 39.1 |  |  | 41.7 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |
| Queve Length 50th（fi） | 39 | 178 |  | 77 | 184 | 0 | 74 | 231 |  | 43 | 157 |  |
| Queve Length 95th（fi） | 80 | \＃316 |  | \＃174 | \＃346 | 35 | \＃155 | \＃393 |  | \＃119 | \＄272 |  |



Cycle Length: 85
Actuated Cycle Length: 85
Offset: $0(0 \%)$, Referenced to phase 2 NET, Start of Green
Natural Syce: 85
Control Type: Actuated-Coordinated
Maximum wc e Ratio: 0.85
Intersection Signal Delay: $41.8 \quad$ Intersection LOS: 0
Intersection Capacity Utízation 87.5\% ICU Level of Service E
Analysis Period (min) 15

* 95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.
Splits and Phases: 23: NH 102 (E Broadway) \& Birch SUCrystal Av


|  | 4 | 4 | \% | $\cdots$ | $\downarrow$ | $\downarrow$ | $\stackrel{4}{e r}^{4}$ | $\not$ | $\uparrow$ | $W_{W C}$ | $\checkmark$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | \% | $\uparrow \uparrow$ | ¢ | \% 11 | $\uparrow$ | \% | \% | $\uparrow$ | 7 | \% | $\uparrow$ | 7 |
| Traffic Volume (vph) | 80 | 350 | 150 | 520 | 430 | 190 | 240 | 320 | 90 | 150 | 220 | 380 |
| Future Volume (vph) | 80 | 350 | 150 | 520 | 430 | 190 | 240 | 320 | 90 | 150 | 220 | 380 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( $f$ ) | 150 |  | 150 | 0 |  | 0 | 0 |  | , | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 2 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (t) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Sald Flow (prot) | 1770 | 3539 | 1583 | 3433 | 1863 | 1583 | 1770 | 1863 | 1583 | 1787 | 1881 | 1599 |
| Fit Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1770 | 3539 | 1583 | 3433 | 1863 | 1583 | 1770 | 1853 | 1583 | 1787 | 1881 | 1599 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTCR) |  |  | 256 |  |  | 202 |  |  | 199 |  |  | 142 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (tt) |  | 639 |  |  | 394 |  |  | 532 |  |  | 387 |  |
| Travel Time (s) |  | 14.5 |  |  | 9.0 |  |  | 12.1 |  |  | 8.8 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.94 | 0.94 | 0.94 | 0.96 | 0.96 | 0.96 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | $2 \%$ | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% |
| Adj. Flow (vph) | 87 | 391 | 163 | 553 | 457 | 202 | 250 | 333 | 94 | 158 | 232 | 400 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 87 | 391 | 163 | 553 | 457 | 202 | 250 | 333 | 94 | 158 | 232 | 400 |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | pm+ov |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | , |  | 3 | 8 | 1 |
| Permitted Phases |  |  | 2 |  |  | 6 |  |  | 4 |  |  | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | , | 3 | 8 | 1 |
| Swich Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 15.0 | 25.0 | 25.0 | 35.0 | 45.0 | 45.0 | 14.0 | 40.0 | 40.0 | 15.0 | 25.0 | 35.0 |
| Total Split (s) | 15.0 | 25.0 | 25.0 | 35.0 | 45.0 | 45.0 | 25.0 | 40.0 | 40.0 | 15.0 | 25.0 | 35.0 |
| Total Spit (\%) | 13.0\% | 21.7\% | 21.7\% | 30.4\% | 39.1\% | 39.1\% | 21.7\% | 34.8\% | $34.8 \%$ | 13.0\% | 21.7\% | 30.4\% |
| Maximum Green (s) | 9.0 | 19.0 | 19.0 | 29.0 | 39.0 | 39.0 | 19.0 | 34.0 | 34.0 | 9.0 | 19.0 | 29.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 20 | 2.0 | 2.0 | 2.0 | 2.0 | 20 | 2.0 | 2.0 | 20 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Lead/ag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recal Mode | None | C-Max | C.Max | None | None | None | None | None | None | None | None | None |
| Wakk Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  | 5.0 |  |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 |  |
| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |  |
| Act Effit Green (s) | 9.8 | 29.4 | 29.4 | 24.3 | 44.0 | 44.0 | 18.4 | 28.3 | 28.3 | 9.0 | 18.9 | 49.2 |
| Actuated g/C Ratio | 0.09 | 0.26 | 0.26 | 0.21 | 0.38 | 0.38 | 0.16 | 0.25 | 0.25 | 0.08 | 0.16 | 0.43 |
| vic Raso | 0.58 | 0.43 | 0.27 | 0.76 | 0.64 | 0.28 | 0.89 | 0.73 | 0.17 | 1.14 | 0.75 | 0.52 |
| Control Delay | 66.6 | 40.0 | 1.1 | 49.7 | 35.6 | 4.8 | 78.7 | 49.0 | 0.7 | 165.5 | 60.7 | 16.4 |
| Queve Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |


|  | 4 | $\uparrow$ | $\%$ | $\cdots$ | $\downarrow$ | $\downarrow$ | $\uparrow$ | $\nearrow$ | $\downarrow$ | 1 | $\checkmark$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | S8L | SBT | S8R | NEL. | NET | NER | SWL | SWT | SWR |
| Total Delay | 66.6 | 40.0 | 1.1 | 49.7 | 35.6 | 4.8 | 78.7 | 49.0 | 0.7 | 165.5 | 60.7 | 16.4 |
| LOS | E | D | A | D | D | A | E | D | A | F | E | B |
| Approach Delay |  | 33.7 |  |  | 36.9 |  |  | 53.3 |  |  | 59.2 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | E |  |
| Queue Length 50th (ft) | 62 | 130 | 0 | 199 | 284 | 0 | 182 | 224 | 0 | $\sim 136$ | 165 | 134 |
| Queue Length 95th (fi) | \#134 | 198 | 0 | 248 | 419 | 51 | \#324 | 310 | 0 | \#273 | 241 | 190 |
| Internal Link Dist (ti) |  | 559 |  |  | 314 |  |  | 452 |  |  | 307 |  |
| Turn Bay Length ( f ) | 150 |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 153 | 905 | 595 | 865 | 712 | 730 | 292 | 550 | 608 | 139 | 392 | 824 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.57 | 0.43 | 0.27 | 0.64 | 0.64 | 0.28 | 0.86 | 0.61 | 0.15 | 1.14 | 0.59 | 0.49 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

## Area Type: Other

Cycle Length: 115
Actuated Cycle Length: 115
Offset: 0 (0\%), Referenced to phase 2:NBT, Start of Green
Natural Cycle: 115
Control Type: Actuated-Ccordinated
Maximum vic Ratio: 1.14
Intersection Signal Delay: $44.9 \quad$ Intersection LOS: D
Intersection Capacity Utilization 74.5\% ICU Level of Service D
Analysis Period (min) 15
~ Volume exceeds capacity, queve is theoretically infnite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queve shown is maximum after two cycles.


| 6: Applebee's/Linlew Dr \& NH 28 |  |  |  |  |  |  |  |  | Existing 2015 PM Peak <br> 12/23/2016 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\cdots$ | 4 | 2 | $\cdots$ | $k$ | $\%$ |  | $\cdots$ | 74 |  | $\downarrow$ | c- |
| Lane Group | SEL | SET | SER | NML | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| Lane Configurations | ${ }^{*}$ | 个 ${ }_{\sim}^{\circ}$ |  | \% | 个\% |  |  | + | \% |  | $\uparrow$ | \% |
| Traffic Volume (vph) | 170 | 1400 | 5 | 20 | 855 | 80 | 15 | 10 | 15 | 45 | 10 | 215 |
| Future Volume (vph) | 170 | 1400 | 5 | 20 | 855 | 80 | 15 | 10 | 15 | 45 | 10 | 215 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.999 |  |  | 0.987 |  |  |  | 0.850 |  | 1.00 | 0.850 |
| Fit Protected | 0.950 |  |  | 0.950 |  |  |  | 0.971 |  |  | 0.961 | 0.850 |
| Satd. Flow (prot) | 1787 | 3571 | 0 | 1787 | 3528 | 0 | 0 | 1845 | 1615 | 0 | 1808 | 1599 |
| Fit Permitted | 0.950 |  |  | 0.950 |  |  |  | 0.774 |  | 0 | 0.747 | 1599 |
| Satd. Flow (perm) | 1787 | 3571 | 0 | 1787 | 3528 | 0 | 0 | 1471 | 1615 | 0 | 1405 | 1599 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes | 0 | 1405 | Yes |
| Sald. Flow (RTOR) |  | 1 |  |  | 13 |  |  |  | 172 |  |  | 269 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 | 209 |
| Link Distance ( ft ) |  | 277 |  |  | 755 |  |  | 230 |  |  | 387 |  |
| Travel Time (s) |  | 6.3 |  |  | 17.2 |  |  | 5.2 |  |  | 8.8 |  |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.95 | 0.95 | 0.95 | 0.90 | 0.90 | 0.90 | 0.80 | 0.80 | 0.80 |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 1\% | 1\% | 1\% |
| Adj. Flow (vph) | 175 | 1443 | 5 | 21 | 900 | 84 | 17 | 11 | 17 | 56 | 13 | 269 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  | 17 | 5 | 13 | 269 |
| Lane Group Flow (vph) | 175 | 1448 | 0 | 21 | 984 | 0 | 0 | 28 | 17 | 0 | 69 | 269 |
| Turn Type | Prot | NA |  | Prot | NA |  | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | 5 | 2 |  | 1 | 6 |  |  | 8 |  | Perm | 4 | Perm |
| Permitted Phases |  |  |  |  |  |  | 8 |  | 8 | 4 | 4 | 4 |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 8 | 8 | 8 | 4 | 4 | 4 |
| Switch Phase |  |  |  |  |  |  |  | 8 |  | 4 | 4 | 4 |
| Minimum Initial (s) | 5.0 | 8.0 |  | 5.0 | 8.0 |  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 26.0 | 63.0 |  | 11.0 | 48.0 |  | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 |
| Total Split (s) | 26.0 | 63.0 |  | 11.0 | 48.0 |  | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 | 21.0 |
| Total Split (\%) | 27.4\% | 66.3\% |  | 11.6\% | 50.5\% |  | 22.1\% | 22.1\% | 22.1\% | 22.1\% | 22.1\% | 22.1\% |
| Maximum Green ( s ) | 20.0 | 57.0 |  | 5.0 | 42.0 |  | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 15.0 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 6.0 | 6.0 |  | 6.0 | 6.0 |
| Lead/ag | Lead | Lag |  | Lead | Lag |  |  |  |  |  | 6.0 | 6.0 |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 30 |  |
| Recall Mode | None | C.Max |  | None | C-Max |  | None | None | None | None | None | None |
| Walk Time (s) |  | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | None |
| Flash Dont Walk (s) |  | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (\#)hr) |  | 0 |  |  | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 14.5 | 68.0 |  | 6.0 | 52.4 |  |  | 10.1 | 10.1 |  | 10.1 | 10.1 |
| Actuated g/C Ratio | 0.15 | 0.72 |  | 0.06 | 0.55 |  |  | 0.11 | 0.11 |  | 0.11 | 0.11 |
| v/c Ratio | 0.64 | 0.57 |  | 0.19 | 0.50 |  |  | 0.18 | 0.05 |  | 0.46 | 0.66 |
| Control Delay | 37.4 | 14.3 |  | 46.3 | 15.5 |  |  | 39.4 | 0.3 |  | 48.8 | 13.0 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |  | 0.0 | 0.0 |
| Total Delay | 37.4 | 14.3 |  | 46.3 | 15.5 |  |  | 39.4 | 0.3 |  | 48.8 | 13.0 |
| LOS | D | B |  | D | B |  |  | D | A |  | D | B |
| Approach Delay |  | 16.8 |  |  | 16.2 |  |  | 24.7 |  |  | 20.3 | B |


| Lanes, Volumes, Timings <br> 6: Applebee's/Linlew Dr \& NH 28 |  |  |  |  |  |  |  |  | Existing 2015 PM Peak |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\cdots$ | $\checkmark$ | $\lambda$ | $\cdots$ | $k$ | \# | $y$ | $\not$ | 3 | 4 | 4 | k |
| Lane Group | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL. | SWT | SWR |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | C |  |
| Queue Length 50th ( t ) | 104 | 284 |  | 12 | 179 |  |  | 16 | 0 |  | 40 | 0 |
| Queve Length 95th (ft) | m125 | 437 |  | 36 | 296 |  |  | 40 | 0 |  | 69 | 43 |
| Internal Link Dist (ft) |  | 197 |  |  | 675 |  |  | 150 |  |  | 307 |  |
| Turn Bay Length (f) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 376 | 2557 |  | 113 | 1951 |  |  | 232 | 399 |  | 221 | 479 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |  | 0 | 0 |
| Spilloack Cap Reductr | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |  | 0 | 0 |
| Reduced vic Ratio | 0.47 | 0.57 |  | 0.19 | 0.50 |  |  | 0.12 | 0.04 |  | 0.31 | 0.56 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 95 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 95 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset $69(73 \%)$, Referenced to phase 2:SET and 6:NWT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 95 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum vic Rato: 0.66 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay. 17.1 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |  |
| Intersection Capacity Ubilization 67.7\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95 th percentle queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Spits and Phases: 6: Applebee's/Linlew Dr \& NH 28


|  | 7 | $\overrightarrow{S B}$ |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7\% | 个t |  | ${ }_{7}$ | 个 $\uparrow$ |  | * | $\dagger$ |  | ${ }^{*}$ | $\uparrow$ | F |
| Traffic Volume (vph) | 110 | 1095 | 5 | 5 | 800 | 260 | 40 | 10 | 10 | 345 | 5 | 135 |
| Future Volume (vph) | 110 | 1095 | 5 | 5 | 800 | 260 | 40 | 10 | 10 | 345 | 5 | 135 |
| Ideal Flow (yphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (t) | 150 |  | 150 | 150 |  | 150 | - |  | O |  |  | 0 |
| Storage Lanes | 2 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 1 |
| Taper Length (t) | 150 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 0.97 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt |  | 0.999 |  |  | 0.963 |  |  | 0.925 |  |  |  | 0.850 |
| Fin Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.954 |  |
| Sadd. Flow (prot) | 3467 | 3571 | 0 | 1770 | 3408 | 0 | 1805 | 1758 | 0 | 1715 | 1722 | 1615 |
| Fit Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 | 0.954 |  |
| Satd. Flow (perm) | 3467 | 3571 | 0 | 1770 | 3408 | 0 | 1805 | 1758 | 0 | 1715 | 1722 | 1615 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 1 |  |  | 62 |  |  | 13 |  |  |  | 108 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (t) |  | 877 |  |  | 261 |  |  | 151 |  |  | 343 |  |
| Travel Time (s) |  | 19.9 |  |  | 5.9 |  |  | 3.4 |  |  | 7.8 |  |
| Peak Hour Factor | 0.84 | 0.84 | 0.84 | 0.90 | 0.90 | 0.90 | 0.78 | 0.78 | 0.78 | 0.86 | 0.86 | 0.86 |
| Heary Vehicles (\%) | 1\% | 1\% | 1\% | 2\% | 2\% | 2\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 131 | 1304 | 6 | 6 | 889 | 289 | 51 | 13 | 13 | 401 | 6 | 157 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  | 49\% |  |  |
| Lane Group Flow (vph) | 131 | 1310 | 0 | 6 | 1178 | 0 | 51 | 26 | 0 | 205 | 202 | 157 |
| Tum Type | Prot | NA |  | Prot | NA |  | Split | NA |  | Split | NA | pttov |
| Protecled Proses | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 | 45 |
| Permitled Phases |  | 2 |  |  | 6 |  |  |  |  |  |  |  |
| Detector Phase | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 | 45 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 8.0 |  | 5.0 | 8.0 |  | 50 | 5.0 |  | 8.0 | 8.0 |  |
| Minimum Spit (s) | 11.0 | 53.0 |  | 11.0 | 50.0 |  | 11.0 | 11.0 |  | 20.0 | 20.0 |  |
| Total Spit (s) | 14.0 | 53.0 |  | 11.0 | 50.0 |  | 11.0 | 11.0 |  | 20.0 | 20.0 |  |
| Total Spit (\%) | 14.7\% | 55.8\% |  | 11.6\% | 52.6\% |  | 11.6\% | 11.6\% |  | 21.1\% | 21.1\% |  |
| Maximum Green (s) | 8.0 | 47.0 |  | 5.0 | 44.0 |  | 5.0 | 5.0 |  | 14.0 | 14.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Leadlag | Lead | Lag |  | Lead | Lag |  | Lead | Lead |  | Lag | Lag |  |
| Lead-Lag Opómize? | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | C.Max |  | None | None |  | None | None |  | None | None |  |
| Walk Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Flash Dont Walk (s) |  | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Cals (\#hr) |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 7.7 | 58.5 |  | 5.1 | 47.0 |  | 5.0 | 5.0 |  | 13.5 | 13.5 | 27.2 |
| Actuated g/C Ratio | 0.08 | 0.62 |  | 0.05 | 0.49 |  | 0.05 | 0.05 |  | 0.14 | 0.14 | 0.29 |
| vic Ratio | 0.47 | 0.60 |  | 0.06 | 0.69 |  | 0.54 | 0.25 |  | 0.84 | 0.83 | 0.29 |
| Control Delay | 47.4 | 14.0 |  | 65.0 | 14.8 |  | 65.2 | 34.5 |  | 69.2 | 67.0 | 10.9 |
| Queve Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |


| Lane Group | EBL | $\underset{\text { EBT }}{\overrightarrow{S B}}$ | EBR WBL | $\leftarrow$ <br> NB WBT | WER | 4 | $\overbrace{\text { N }}^{4}$ | $p$ | SBL | $\downarrow$ | $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SER |
| Total Delay | 47.4 | 14.0 | 65.0 | 14.8 |  | 65.2 | 34.5 |  | 69.2 | 67.0 | 10.9 |
| LOS | 0 | B | E | B |  | E | C |  | E | E | . |
| Approach Delay |  | 17.1 |  | 15.0 |  |  | 54.8 |  |  | 522 |  |
| Approach LOS |  | B |  | B |  |  | D |  |  | D |  |
| Queue Length 50th (f) | 39 | 234 | 3 | 311 |  | 31 | 8 |  | 127 | 125 | 21 |
| Queue Length 95th (ft) | 63 | 356 | m7 | 408 |  | \#60 | 29 |  | \#232 | \#227 | 63 |
| Internal Link Dist (t) |  | 797 |  | 181 |  |  | 71 |  |  | 263 |  |
| Turn Bay Length (f) | 150 |  | 150 |  |  |  |  |  |  |  |  |
| Base Capacity (yph) | 291 | 2198 | 95 | 1717 |  | 95 | 104 |  | 252 | 253 | 533 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spilback Cap Reductn | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |  | 0 | , |  | 0 | 0 | 0 |
| Reduced vic Rato | 0.45 | 0.60 | 0.06 | 0.69 |  | 0.54 | 0.25 |  | 0.81 | 0.80 | 0.29 |

## Intersection Summary

Area Type:

## Other

Cycle Length: 95
Actuated Cycle Length: 95
Offset: 0 (0\%), Referenced to phase 2.EBT. Start of Green
Natural Cycle: 95
Control Type: Actuated-Ccordinated
Maximum w/c Ratio: 0.84
Intersection Signal Delay: 23.3
Intersection Capacity Utizzation 65.9\%
Intersection LOS: C ICU Level of Service C
Analysis Period (min) 15
\# 95th percentie volume exceeds capacity, queve may be longer.
Queue shown is maximum after two cycles.
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Spits and Phases: 9: VIP Dr/Ashleigh Dr \& NH 28


| Lane Group |  |  |  |  |  |  | EM |  |  | WO |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NEL | NBT | NBR | SEL | SBT | SBR | NEL | NET | NER | SWL | SWT | SVR |
| Lane Configurations | 7 | F |  | \% | $\uparrow$ | 7 | \% | ¢ |  | \% | ち |  |
| Traffic Volume (vph) | 100 | 320 | 25 | 75 | 185 | 185 | 280 | 345 | 75 | 25 | 175 | 70 |
| Future Volume (yph) | 100 | 320 | 25 | 75 | 185 | 185 | 280 | 345 | 75 | 25 | 175 | 70 |
| Ideal Flow (vphpl') | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ti) | 150 |  | 150 | 150 |  | 150 | 150 |  | 150 | 150 |  | 150 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 0 |  |  | 0 |
| Taper Length (fi) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.989 |  |  |  | 0.850 |  | 0.973 |  |  | 0.957 |  |
| FIt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1842 | 0 | 1787 | 1881 | 1599 | 1805 | 1849 | 0 | 1805 | 1818 | 0 |
| Fit Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 1770 | 1842 | 0 | 1787 | 1881 | 1599 | 1805 | 1849 | 0 | 1805 | 1818 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 4 |  |  |  | 195 |  | 13 |  |  | 21 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 481 |  |  | 347 |  |  | 479 |  |  | 371 |  |
| Travel Time (s) |  | 10.9 |  |  | 7.9 |  |  | 10.9 |  |  | 8.4 |  |
| Peak Hour Factor | 0.99 | 0.99 | 0.99 | 0.95 | 0.95 | 0.95 | 0.89 | 0.89 | 0.89 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 101 | 323 | 25 | 79 | 195 | 195 | 315 | 388 | 84 | 27 | 188 | 75 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (yph) | 101 | 348 | 0 | 79 | 195 | 195 | 315 | 472 | 0 | 27 | 263 | 0 |
| Turn Type | Prot | NA |  | Prot | NA | pt+ov | Prot | NA |  | Prot | NA |  |
| Protected Phases | 1 | 6 |  | 5 | 2 | 23 | 3 | 8 |  | 7 | 4 |  |
| Permitted Phases |  | 6 |  |  | 2 |  |  |  |  |  |  |  |
| Detector Phase | 1 | 6 |  | 5 | 2 | 23 | 3 | 8 |  | 7 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Minimum Split (s) | 14.0 | 20.0 |  | 14.0 | 20.0 |  | 14.0 | 28.0 |  | 14.0 | 14.0 |  |
| Total Split (s) | 15.0 | 24.0 |  | 14.0 | 23.0 |  | 23.0 | 28.0 |  | 14.0 | 19.0 |  |
| Total Split (\%) | 18.8\% | 30.0\% |  | 17.5\% | 28.8\% |  | 28.8\% | 35.0\% |  | 17.5\% | 23.8\% |  |
| Maximum Green (s) | 9.0 | 18.0 |  | 8.0 | 17.0 |  | 17.0 | 22.0 |  | 8.0 | 13.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 20 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 20 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/lag | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  | Lead | Lag |  |
| Lead-Lag Optimize? Lead Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehide Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | C-Max |  | None | None |  | None | None |  |
| Walk Time (s) |  |  |  |  |  |  |  | 7.0 |  |  |  |  |
| Flash Dont Walk (s) |  |  |  |  |  |  |  | 15.0 |  |  |  |  |
| Pedestrian Calls (\#hr) |  |  |  |  |  |  |  | 0 |  |  |  |  |
| Act Effict Green (s) | 8.7 | 21.8 |  | 8.0 | 21.2 | 43.5 | 16.3 | 29.4 |  | 8.0 | 12.7 |  |
| Actuated g/C Ratio | 0.11 | 0.27 |  | 0.10 | 0.26 | 0.54 | 0.20 | 0.37 |  | 0.10 | 0.16 |  |
| wic Ratio | 0.53 | 0.69 |  | 0.44 | 0.39 | 0.20 | 0.86 | 0.69 |  | 0.15 | 0.86 |  |
| Control Delay | 44.2 | 37.0 |  | 42.4 | 29.4 | 2.3 | 54.0 | 30.0 |  | 35.1 | 58.0 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |

4A Zone $55: 00$ pm 12/30/2016 Existing 2015 PM Peak PK

Synchro 9 Report Page 1

|  | M | $\uparrow$ | 1 | $\cdots$ | $\downarrow$ | $\downarrow$ | $\xlongequal{4}$ | $\not$ | $\uparrow$ | $\downarrow$ | $\checkmark$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | NBL | NBT | NBR | S8L | SBT | SER | NEL | NET | NER | SWL | SWT | SWR |
| Total Delay | 44.2 | 37.0 |  | 42.4 | 29.4 | 2.3 | 54.0 | 30.0 |  | 35.1 | 58.0 |  |
| LOS | D | D |  | D | c | A | D | C |  | D | E |  |
| Approach Delay |  | 38.6 |  |  | 20.4 |  |  | 39.6 |  |  | 55.9 |  |
| Approach LOS |  | D |  |  | c |  |  | D |  |  | E |  |
| Queue Length 50th (fi) | 48 | 165 |  | 38 | 86 | 0 | 151 | 162 |  | 13 | 119 |  |
| Queue Length 95th (fi) | 97 | \#307 |  | 80 | 149 | 30 | \#278 | \#394 |  | 36 | \#248 |  |
| Internal Link Dist ( ft ) |  | 401 |  |  | 267 |  |  | 399 |  |  | 291 |  |
| Tum Bay Length ( f ) | 150 |  |  | 150 |  | 150 | 150 |  |  | 150 |  |  |
| Base Capacity (vph) | 199 | 505 |  | 178 | 497 | 970 | 383 | 687 |  | 180 | 313 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Spilback Cap Reductn |  | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Reduced vic Ratio | 0.51 | 0.69 |  | 0.44 | 0.39 | 0.20 | 0.82 | 0.69 |  | 0.15 | 0.84 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maxímum vic Rato: 0.86 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 37.2 |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 74.4\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Tsienneto Rd \& NH 28 Byp NEINH 28 Byp SB


APPENDIX G-3: HCM PRINTOUTS - SIGNALIZED INTERSECTION CAPACITY ANALYSES - 2015 AM AND PM PEAK HOURS

HCM Signalized Intersection Capacity Analysis
7: Exit 4 SB Off


|  | 1 | 1 | $\cdots$ | \% | V | $\nearrow$ | $\downarrow$ | $\checkmark$ | 1 | k |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBR | SEL | SER | NEL | NET | NER | SWL | SWT | SWR |
| Lane Confgurations | \%* | 1 |  |  | $\%$ | $\uparrow \uparrow$ |  |  | 44 | 1 |
| Traffic Volume (vph) | 210 | 200 | 0 | 0 | 585 | 590 | 0 | 0 | 875 | 0 |
| Future Volume (vph) | 210 | 200 | 0 | 0 | 585 | 590 | 0 | 0 | 875 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 4.0 |  |  | 6.0 | 6.0 |  |  | 6.0 |  |
| Lane Util. Factor | 0.97 | 1.00 |  |  | 1.00 | 0.95 |  |  | 0.95 |  |
| Frt | 1.00 | 0.85 |  |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Flt Protected | 0.95 | 1.00 |  |  | 0.95 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (grot) | 3242 | 1495 |  |  | 1719 | 3438 |  |  | 3505 |  |
| Fll Permitted | 0.95 | 1.00 |  |  | 0.95 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (perm) | 3242 | 1495 |  |  | 1719 | 3438 |  |  | 3505 |  |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.92 | 0.92 | 0.94 | 0.94 | 0.94 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 239 | 227 | 0 | 0 | 622 | 628 | 0 | 0 | 951 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (voh) | 239 | 227 | 0 | 0 | 622 | 628 | 0 | 0 | 951 | 0 |
| Heary Vehicles (\%) | 8\% | 8\% | 2\% | 2\% | 5\% | 5\% | 5\% | 3\% | 3\% | $3 \%$ |
| Tum Type | Prot | Free |  |  | Prot | NA |  |  | NA | Free |
| Protected Phases | 2 |  |  |  | 7 | 4 |  |  | 8 |  |
| Permitted Phases |  | Free |  |  |  |  |  |  |  | Free |
| Actuated Green, G (s) | 12.9 | 100.0 |  |  | 41.1 | 75.1 |  |  | 28.0 |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 12.9 | 100.0 |  |  | 41.1 | 75.1 |  |  | 28.0 |  |
| Actuated g/C Ratio | 0.13 | 1.00 |  |  | 0.41 | 0.75 |  |  | 0.28 |  |
| Clearance Time (s) | 6.0 |  |  |  | 6.0 | 6.0 |  |  | 6.0 |  |
| Vehide Extension (s) | 3.0 |  |  |  | 3.0 | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) | 418 | 1495 |  |  | $70 \hat{3}$ | 2581 |  |  | 981 |  |
| vis Ratio Prot | c0.07 |  |  |  | c0.36 | 0.18 |  |  | 00.27 |  |
| vis Ratio Perm |  | 0.15 |  |  |  |  |  |  |  |  |
| víc Ratio | 0.57 | 0.15 |  |  | 0.88 | 0.24 |  |  | 0.97 |  |
| Uniform Delay, d1 | 41.0 | 0.0 |  |  | 27.2 | 3.8 |  |  | 35.6 |  |
| Progression Factor | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 | 5.6 | 0.2 |  |  | 12.4 | 0.0 |  |  | 21.3 |  |
| Delay (s) | 46.5 | 0.2 |  |  | 39.6 | 3.8 |  |  | 56.9 |  |
| Level of Service | D | A |  |  | D | A |  |  | E |  |
| Approach Delay (s) | 24.0 |  | 0.0 |  |  | 21.6 |  |  | 56.9 |  |
| Approach LOS | c |  | A |  |  | C |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 34.6 | HCM 2000 Level of Service |  |  |  |  | C |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.86 |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 | Sum of lost time (s) |  |  |  |  | 18.0 |  |
| Intersection Capacity Utiolization |  |  | 84.6\% | ICU Level of Service |  |  |  |  | E |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |



|  | $\Rightarrow$ |  |  | 6 | $\leftarrow$ |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | S8R |
| Lane Configurations | 7 | 个个 |  |  | 4个 | ＊ | ＊ |  | $\overline{7}$ |  |  |  |
| Traffic Volume（vph） | 240 | 740 | 0 | 0 | 540 | 740 | 300 | 0 | 110 | 0 | 0 | 0 |
| Future Volume（vph） | 240 | 740 | 0 | 0 | 540 | 740 | 300 | 0 | 110 | 0 | 0 | 0 |
| Ideal Flow（vohpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost ime（s） | 6.0 | 6.0 |  |  | 6.0 | 4.0 | 6.0 |  | 4.0 |  |  |  |
| Lane Uti．Factor | 1.00 | 0.95 |  |  | 0.95 | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Fit | 1.00 | 1.00 |  |  | 1.00 | 0.85 | 1.00 |  | 0.85 |  |  |  |
| Fil Protected | 0.95 | 1.00 |  |  | 1.00 | 1.00 | 0.95 |  | 1.00 |  |  |  |
| Sald．Flow（prot） | 1641 | 3282 |  |  | 3438 | 1538 | 1656 |  | 1482 |  |  |  |
| Fil Permitted | 0.95 | 1.00 |  |  | 1.00 | 1.00 | 0.95 |  | 1.00 |  |  |  |
| Sand．Flow（perm） | 1641 | 3282 |  |  | 3438 | 1538 | 1656 |  | 1482 |  |  |  |
| Peak－hour factor，PHF | 0.87 | 0.87 | 0.87 | 0.90 | 0.90 | 0.90 | 0.78 | 0.78 | 0.78 | 0.92 | 0.92 | 0.92 |
| Adj．Flow（vph） | 276 | 851 | 0 | 0 | 600 | 822 | 385 | 0 | 141 | 0 | 0 | 0 |
| RTOR Reduction（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow（vph） | 276 | 851 | 0 | 0 | 600 | 822 | 385 | 0 | 141 | 0 | 0 | 0 |
| Heary Vehicles（\％） | 10\％ | 10\％ | 10\％ | 5\％ | 5\％ | 5\％ | 9\％ | 9\％ | 9\％ | 2\％ | 2\％ | 2\％ |
| Tum Type | Prot | NA |  |  | NA | Free | Prot |  | Free |  |  |  |
| Protected Phases | 5 | 2 |  |  | 6 |  | 8 |  |  |  |  |  |
| Permited Phases |  | 2 |  |  | 6 | Free |  |  | Free |  |  |  |
| Actuated Green，G（s） | 15.7 | 46.6 |  |  | 24.9 | 80.0 | 21.4 |  | 80.0 |  |  |  |
| Effective Green， g （s） | 15.7 | 46.6 |  |  | 24.9 | 80.0 | 21.4 |  | 80.0 |  |  |  |
| Actuated g／C Ratio | 0.20 | 0.58 |  |  | 0.31 | 1.00 | 0.27 |  | 1.00 |  |  |  |
| Clearance Time（s） | 6.0 | 6.0 |  |  | 6.0 |  | 6.0 |  |  |  |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  |  | 3.0 |  | 3.0 |  |  |  |  |  |
| Lane Grp Cap（vph） | 322 | 1911 |  |  | 1070 | 1538 | 442 |  | 1482 |  |  |  |
| w／s Ratio Prot | 0.17 | 0.26 |  |  | 0.17 |  | 00.23 |  |  |  |  |  |
| w／s Ratio Perm |  |  |  |  |  | c0．53 |  |  | 0.10 |  |  |  |
| vic Ratio | 0.86 | 0.45 |  |  | 0.56 | 0.53 | 0.87 |  | 0.10 |  |  |  |
| Uniform Delay，d1 | 31.1 | 9.4 |  |  | 23.0 | 0.0 | 28.0 |  | 0.0 |  |  |  |
| Progression Factor | 1.05 | 0.16 |  |  | 1.00 | 1.00 | 1.00 |  | 1.00 |  |  |  |
| Incremental Delay， 02 | 16.2 | 0.6 |  |  | 2.1 | 1.3 | 16.9 |  | 0.1 |  |  |  |
| Delay（s） | 49.0 | 2.1 |  |  | 25.1 | 1.3 | 44.9 |  | 0.1 |  |  |  |
| Level of Service | D | A |  |  | c | A | D |  | A |  |  |  |
| Approach Delay（s） |  | 13.6 |  |  | 11.4 |  |  | 32.9 |  |  | 0.0 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 15.9 |  | HCM 2000 | evel of S | ervice |  | B |  |  |  |
| HCM 2000 Control Delay HCM 2000 Volume to Capacity ratio |  |  | 0.78 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 80.0 |  | Sum of lost | lime（s） |  |  | 18.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 65．7\％ |  | CU Level | Service |  |  | C |  |  |  |
| Análysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |





| Turn Type | Prot | NA | Prot | NA | Prot | NA | Prot | NA | Perm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Protected Phases | 5 | 2 | 1 | 6 | 3 | 8 | 7 | 4 |  |
| Permitted Phases |  |  |  |  |  |  |  |  | 4 |
| Actuated Green, G (s) | 6.0 | 29.3 | 3.4 | 26.7 | 4.0 | 17.5 | 4.0 | 17.5 | 17.5 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 6.0 | 29.3 | 3.4 | 26.7 | 4.0 | 17.5 | 4.0 | 17.5 | 17.5 |
| Actuated g/C Ratio | 0.08 | 0.37 | 0.04 | 0.34 | 0.05 | 0.22 | 0.05 | 0.22 | 0.22 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 127 | 630 | 74 | 596 | 87 | 396 | 87 | 401 | 341 |
| vis Ratio Prot wis Ratio Perm | c0.07 | 0.16 | 0.02 | co. 28 | 0.04 | co. 20 | c0.05 | 0.14 | 0.02 |
| v/c Ratio | 0.86 | 0.42 | 0.50 | 0.82 | 0.82 | 0.87 | 0.89 | 0.63 | 0.08 |
| Uniform Delay, d1 | 35.7 | 18.1 | 36.6 | 23.5 | 36.7 | 29.3 | 36.9 | 27.4 | 24.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 40.1 | 0.5 | 5.2 | 8.4 | 42.3 | 18.7 | 59.7 | 3.2 | 0.1 |
| Delay (s) | 75.7 | 18.6 | 41.8 | 31.9 | 79.0 | 48.0 | 96.6 | 30.7 | 24.1 |
| Level of Service | E | B | D | c | E | D | F | c | C |
| Approach Delay (s) |  | 34.7 |  | 32.6 |  | 53.2 |  | 40.4 |  |
| Approach LOS |  | C |  | C |  | D |  | D |  |

Intersection Summary

| HCM 2000 Control Delay | 39.9 | HCM 2000 Level of Service | D |
| :--- | ---: | :--- | ---: |
| HCM 2000 Volume to Capacity ratio | 0.84 |  |  |
| Actuated Cycle Length (s) | 78.2 | Sum of lost time (s) | 24.0 |
| Intersection Capacity Utizzation | $70.9 \%$ | ICU Level of Service | C |
| Analysis Period (min) | 15 |  |  |

c Critical Lane Group

|  | $\cdots$ | $\uparrow$ | ${ }^{\prime}$ | L | $\downarrow$ | $\downarrow$ | 4 | 7 | $\uparrow$ | $\checkmark$ | $\checkmark$ | $\uparrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SER | NEL | NET | NER | SW | SWT | SWR |
| Lane Configurations | 1 | 个个 | 7 | 栜 | $\uparrow \uparrow$ | 1 | ${ }^{*}$ | $\uparrow$ | 1 | ${ }^{*}$ | $\uparrow$ | \％ |
| Traffic Volume（vph） | 20 | 230 | 135 | 310 | 220 | 145 | 135 | 170 | 20 | 125 | 290 | 370 |
| Future Volume（vph） | 20 | 230 | 135 | 310 | 220 | 145 | 135 | 170 | 20 | 125 | 290 | 370 |
| Ideal Flow（yphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost ime（s） | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lane Unll．Factor | 1.00 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fit Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Sald．Flow（prot） | 1736 | 3471 | 1553 | 3335 | 3438 | 1538 | 1752 | 1845 | 1568 | 1752 | 1845 | 1568 |
| Fit Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Saxd．Flow（perm） | 1736 | 3471 | 1553 | 3335 | 3438 | 1538 | 1752 | 1845 | 1568 | 1752 | 1845 | 1568 |
| Peak－hour factor，PHF | 0.84 | 0.84 | 0.84 | 0.79 | 0.79 | 0.79 | 0.86 | 0.86 | 0.86 | 0.99 | 0.99 | 0.99 |
| Adj．Flow（vph） | 24 | 274 | 161 | 392 | 278 | 184 | 157 | 198 | 23 | 126 | 293 | 374 |
| RTOR Reduction（vph） | ， | 0 | 113 | 0 | 0 | 114 | 0 | 0 | O | 0 | ， | 155 |
| Lane Group Flow（vph） | 24 | 274 | 48 | 392 | 278 | 70 | 157 | 198 | 23 | 126 | 293 | 219 |
| Heavy Vehicles（\％） | 4\％ | 4\％ | 4\％ | 5\％ | 5\％ | 5\％ | 3\％ | 3\％ | 3\％ | 3\％ | 3\％ | 3\％ |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | Free |  | NA | $\mathrm{pl}+\mathrm{or}$ |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 | 81 |
| Permitted Phases |  | 2 | 2 |  | 6 | 6 |  | 4 | Free |  | 8 |  |
| Actuated Green，G（s） | 8.0 | 26.8 | 26.8 | 15.2 | 34.0 | 34.0 | 9.0 | 15.3 | 90.0 | 8.7 | 15.0 | 36.2 |
| Effective Green， g （s） | 8.0 | 26.8 | 26.8 | 15.2 | 34.0 | 34.0 | 9.0 | 15.3 | 90.0 | 8.7 | 15.0 | 362 |
| Actuated g／＇Ratio | 0.09 | 0.30 | 0.30 | 0.17 | 0.38 | 0.38 | 0.10 | 0.17 | 1.00 | 0.10 | 0.17 | 0.40 |
| Clearance Time（s） | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap（vph） | 154 | 1033 | 462 | 563 | 1298 | 581 | $175$ | 313 | 1568 | 169 | 307 | 630 |
| w／s Ratio Prot | 0.01 | c0．08 |  | 0.12 | 0.08 |  | $00.09$ | 0.11 |  | 0.07 | c0．16 | 0.14 |
| w／s Ratio Perm |  |  | 0.03 |  |  | 0.05 |  |  | c0．01 |  |  |  |
| vic Ratio | 0.16 | 0.27 | 0.10 | 0.70 | 0.21 | 0.12 | 0.90 | 0.63 | 0.01 | 0.75 | 0.95 | 0.35 |
| Unilorm Delay，d1 | 37.9 | 24.1 | 22.9 | 35.2 | 19.0 | 18.2 | 40.0 | 34.7 | 0.0 | 39.6 | 37.2 | 18.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 21 | 0.6 | 0.5 | 3.7 | 0.4 | 0.4 | 39.8 | 4.1 | 0.0 | 163 | 39.0 | 0.3 |
| Delay（s） | 40.0 | 24.7 | 23.3 | 39.0 | 19.3 | 18.7 | 79.8 | 38.9 | 0.0 | 55.9 | 76.1 | 19.0 |
| Level or Service | D | C | C | D | B | B | E | D | A | E | E | B |
| Approach Delay（s） |  | 25.0 |  |  | 28.2 |  |  | 53.5 |  |  | 46.0 |  |
| Approach LOS |  | c |  |  | C |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control DelayHCM 2000 Volume to Capacity ratio |  |  | 37.1 | HCM 2000 Level of Service |  |  |  |  | 0 |  |  |  |
|  |  |  | 0.61 | Sum of lost time（s） |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 90.0 |  |  |  |  |  | 24.0 |  |  |  |
| Intersection Capacity Uttization Analysis Period（min） |  |  | 58．3\％ | ICU Level of Service |  |  |  |  |  |  |  |  |
|  |  |  | 15 |  |  |  |  |  | B |  |  |  |

c Critical Lane Group


|  | \% | $\rightarrow$ |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | K1 | 个 4 |  | \% | $\uparrow$ |  | \% | 今 |  | \% | $\uparrow$ | F |
| Trafic Volume (vph) | 100 | 630 | 5 | 5 | 610 | 220 | 10 | 5 | 5 | 180 | 5 | 100 |
| Future Volume (vph) | 100 | 630 | 5 | 5 | 610 | 220 | 10 | 5 | 5 | 180 | 5 | 100 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 60 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Lane Util. Factor | 0.97 | 0.95 |  | 1.00 | 0.95 |  | 1.00 | 1.00 |  | 0.95 | 0.95 | 1.00 |
| Fit | 1.00 | 1.00 |  | 1.00 | 0.96 |  | 1.00 | 0.93 |  | 1.00 | 1.00 | 0.85 |
| Fit Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 0.96 | 1.00 |
| Satd. Flow (prot) | 3303 | 3402 |  | 1736 | 3333 |  | 1805 | 1758 |  | 1665 | 1674 | 1568 |
| Fit Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 0.96 | 1.00 |
| Satd. Flow (perm) | 3303 | 3402 |  | 1736 | 3333 |  | 1805 | 1758 |  | 1665 | 1674 | 1568 |
| Peak-hour factor, PHF | 0.83 | 0.83 | 0.83 | 0.97 | 0.97 | 0.97 | 0.67 | 0.67 | 0.67 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 120 | 759 | 6 | 5 | 629 | 227 | 15 | 7 | 7 | 200 | 6 | 111 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 41 | 0 | 0 | 7 |  | 0 | 0 | 81 |
| Lane Group Flow (vph) | 120 | 765 | 0 | 5 | 815 | 0 | 15 | 7 | 0 | 102 | 104 | 30 |
| Heavy Vehicles (\%) | 6\% | 6\% | 6\% | 4\% | 4\% | 4\% | 0\% | 0\% | 0\% | 3\% | 3\% | 3\% |
| Turn Type | Prot | NA |  | Prot | NA |  | Split | NA |  | Split | NA | pltor |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 3 | 3 |  | 4 | 4 | 45 |
| Permitted Phases |  |  |  |  |  |  |  | 3 |  |  |  | 45 |
| Actuated Green, G (s) | 8.0 | 50.2 |  | 1.0 | 43.2 |  | 4.1 | 4.1 |  | 10.7 | 10.7 | 24.7 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 8.0 | 50.2 |  | 1.0 | 43.2 |  | 4.1 | 4.1 |  | 10.7 | 10.7 | 24.7 |
| Acluated g/C Ratio | 0.09 | 0.56 |  | 0.01 | 0.48 |  | 0.05 | 0.05 |  | 0.12 | 0.12 | 0.27 |
| Clearance Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 293 | 1897 |  | 19 | 1599 |  | 82 | 80 |  | 197 | 199 | 430 |
| w/s Ratio Prot w/s Ratio Perm | 00.04 | c0.22 |  | 0.00 | co. 24 |  | 00.01 | 0.00 |  | 0.06 | c0.06 | 0.02 |
| wc Ratio | 0.41 | 0.40 |  | 0.26 | 0.51 |  | 0.18 | 0.09 |  | 0.52 | 0.52 | 0.07 |
| Uniform Delay, d1 | 38.8 | 11.4 |  | 44.1 | 16.1 |  | 41.3 | 41.2 |  | 37.2 | 37.3 | 24.2 |
| Progression Factor | 1.00 | 1.00 |  | 1.52 | 0.60 |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.9 | 0.1 |  | 6.9 | 1.1 |  | 1.1 | 0.5 |  | 2.3 | 2.5 | 0.1 |
| Delay (s) | 39.7 | 11.5 |  | 73.9 | 10.8 |  | 42.4 | 41.7 |  | 39.5 | 39.7 | 24.2 |
| Level of Service | D | B |  | E | B |  | D | D |  | D | 0 | C |
| Approach Delay (s) |  | 15.3 |  |  | 11.2 |  |  | 42.1 |  |  | 34.2 |  |
| Approach LOS |  | B |  |  | B |  |  | D |  |  | C |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 16.9 | HCM 2000 Level of Service | B |
| HCM 2000 Volume to Capacity ratio | 0.48 |  | 24.0 |
| Actuated Cycle Length (s) | 90.0 | Sum of lost time (s) | A |
| Intersection Capacity UEtization | $54.8 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |


| Movement | NBL | NBT | NER | SBL | SBT | SBR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | ち |  | 7 | $\uparrow$ | 7 | 7 | 今 |  | 7 | F |  |
| Traffic Volume (vph) | 100 | 220 | 20 | 25 | 210 | 255 | 120 | 100 | 80 | 80 | 270 | 90 |
| Future Volume (vph) | 100 | 220 | 20 | 25 | 210 | 255 | 120 | 100 | 80 | 80 | 270 | 90 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.93 |  | 1.00 | 0.96 |  |
| Fit Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Sald. Flow (prot) | 1752 | 1822 |  | 1736 | 1827 | 1553 | 1770 | 1738 |  | 1787 | 1811 |  |
| Fit Permitted | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) | 1752 | 1822 |  | 1736 | 1827 | 1553 | 1770 | 1738 |  | 1787 | 1811 |  |
| Peak-hour factor, PHF | 0.82 | 0.82 | 0.82 | 0.81 | 0.81 | 0.81 | 0.68 | 0.68 | 0.68 | 0.78 | 0.78 | 0.78 |
| Adj. Flow (vph) | 122 | 268 | 24 | 31 | 259 | 315 | 176 | 147 | 118 | 103 | 346 | 115 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 121 | 0 | 34 | 0 | 0 | 15 | 0 |
| Lane Group Flow (yph) | 122 | 288 | 0 | 31 | 259 | 194 | 176 | 231 | 0 | 103 | 447 | 0 |
| Heavy Vehicles (\%) | 3\% | 3\% | 3\% | 4\% | 4\% | 4\% | 2\% | 2\% | $2 \%$ | 1\% | 1\% | 1\% |
| Tum Type | Prot | NA |  | Prot | NA | pt+ov | Prot | NA |  | Prot | NA |  |
| Protected Phases | 1 | 6 |  | 5 | 2 | 23 | 3 | . |  | 7 | 4 |  |
| Permited Phases 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Green, G (s) | 8.0 | 21.8 |  | 3.2 | 17.0 | 32.0 | 9.0 | 23.4 |  | 7.6 | 22.0 |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 8.0 | 21.8 |  | 3.2 | 17.0 | 32.0 | 9.0 | 23.4 |  | 7.6 | 22.0 |  |
| Actuated g/C Ratio | 0.10 | 0.27 |  | 0.04 | 0.21 | 0.40 | 0.11 | 0.29 |  | 0.09 | 0.28 |  |
| Clearance Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 175 | 496 |  | 69 | 388 | 621 | 199 | 508 |  | 169 | 498 |  |
| n's Raso Prot | 00.07 | c0.16 |  | 0.02 | c0.14 | 0.12 | 0.10 | 0.13 |  | 0.06 | co. 25 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| vic Rato | 0.70 | 0.58 |  | 0.45 | 0.67 | 0.31 | 0.88 | 0.45 |  | 0.61 | 0.90 |  |
| Uniform Delay, d1 | 34.8 | 25.2 |  | 37.5 | 28.9 | 16.5 | 35.0 | 23.1 |  | 34.8 | 27.9 |  |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 11.4 | 1.7 |  | 4.6 | 8.8 | 0.3 | 33.9 | 0.6 |  | 6.1 | 18.5 |  |
| Delay (s) | 46.3 | 26.9 |  | 42.1 | 37.7 | 16.7 | 68.9 | 23.7 |  | 40.9 | 46.4 |  |
| Level of Service | D | c |  | D | D | B | E | C |  | D | D |  |
| Approach Delay (s) |  | 32.6 |  |  | 27.0 |  |  | 41.7 |  |  | 45.4 |  |
| Approach LOS |  | C |  |  | C |  |  | D |  |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 36.5 | HCM 2000 Level of Service | D |
| HCM 2000 Volume to Capacity ratio | 0.80 |  | 24.0 |
| Actuated Cycle Length (s) | 80.0 | Sum of lost time (s) | C |
| Intersection Capacity Utilization | $65.8 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |




|  | $\dagger$ | $\rightarrow$ |  | 7 | $\longleftarrow$ |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ $\uparrow$ | \％ | ${ }^{*}$ | 个个 |  |  |  |  | ＊＊ |  | 「 |
| Traffic Volume（vph） | 0 | 650 | 280 | 135 | 490 | 0 | 0 | 0 | 0 | 645 | 0 | 265 |
| Future Volume（yph） | 0 | 650 | 280 | 135 | 490 | 0 | 0 | 0 | 0 | 645 | 0 | 265 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） |  | 6.0 | 4.0 | 6.0 | 6.0 |  |  |  |  | 6.0 |  | 6.0 |
| Lane Util．Factor |  | 0.95 | 1.00 | 1.00 | 0.95 |  |  |  |  | 0.97 |  | 1.00 |
| Frt |  | 1.00 | 0.85 | 1.00 | 1.00 |  |  |  |  | 1.00 |  | 0.85 |
| Fit Protected |  | 1.00 | 1.00 | 0.95 | 1.00 |  |  |  |  | 0.95 |  | 1.00 |
| Satd．Flow（prot） |  | 3471 | 1553 | 1719 | 3438 |  |  |  |  | 3367 |  | 1553 |
| Flt Permitted |  | 1.00 | 1.00 | 0.95 | 1.00 |  |  |  |  | 0.95 |  | 1.00 |
| Satd．Flow（perm） |  | 3471 | 1553 | 1719 | 3438 |  |  |  |  | 3367 |  | 1553 |
| Peak－hour factor，PHF | 0.87 | 0.87 | 0.87 | 0.85 | 0.86 | 0.85 | 0.92 | 0.92 | 0.92 | 0.91 | 0.91 | 0.91 |
| Adj．Flow（vph） | 0 | 747 | 322 | 157 | 570 | 0 | 0 |  | 0 | 709 | 0 | 291 |
| RTOR Reduction（vph） | 0 | 0 | ， | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 197 |
| Lane Group Flow（vph） | 0 | 747 | 322 | 157 | 570 | 0 | 0 | 0 | 0 | 709 | 0 | 94 |
| Heavy Vehides（\％） | 4\％ | 4\％ | 4\％ | 5\％ | 5\％ | 5\％ | 2\％ | $2 \%$ | 2\％ | 4\％ | 4\％ | 4\％ |
| Turn Type |  | NA | Free | Prot | NA |  |  |  |  | Prot |  | Prot |
| Protected Phases |  | 2 |  | 1 | 6 |  |  |  |  | 4 |  | 4 |
| Permitted Phases |  |  | Free |  | 1 |  |  |  |  |  |  |  |
| Actuated Green，G（s） |  | 38.5 | 100.0 | 14.7 | 59.2 |  |  |  |  | 28.8 |  | 28.8 |
| Effective Green， g （ s ） |  | 38.5 | 100.0 | 14.7 | 59.2 |  |  |  |  | 28.8 |  | 28.8 |
| Actuated g／C Raso |  | 0.38 | 1.00 | 0.15 | 0.59 |  |  |  |  | 0.29 |  | 0.29 |
| Clearance Time（s） |  | 6.0 |  | 6.0 | 6.0 |  |  |  |  | 6.0 |  | 6.0 |
| Vehide Extension（s） |  | 4.0 |  | 4.0 | 4.0 |  |  |  |  | 4.0 |  | 4.0 |
| Lane Grp Cap（vph） |  | 1336 | 1553 | 252 | 2035 |  |  |  |  | 969 |  | 447 |
| vis Ratio Prot |  | 00．22 |  | c0．09 | 0.17 |  |  |  |  | c0．21 |  | 0.06 |
| vis Ratio Perm |  |  | 0.21 |  |  |  |  |  |  |  |  |  |
| vic Ratio |  | 0.56 | 0.21 | 0.62 | 0.28 |  |  |  |  | 0.73 |  | 0.21 |
| Uniform Delay，d1 |  | 24.1 | 0.0 | 40.0 | 10.0 |  |  |  |  | 32.1 |  | 27.0 |
| Progression Faclor |  | 1.00 | 1.00 | 0.90 | 0.42 |  |  |  |  | 1.00 |  | 1.00 |
| Incremental Delay，d2 |  | 1.7 | 0.3 | 4.9 | 0.1 |  |  |  |  | 3.1 |  | 0.3 |
| Delay（s） |  | 25.8 | 0.3 | 40.7 | 4.3 |  |  |  |  | 35.2 |  | 27.3 |
| Level of Service |  | C | A | D | A |  |  |  |  | 0 |  | C |
| Approach Delay（s） |  | 18.1 |  |  | 12.1 |  |  | 0.0 |  |  | 32.9 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 21.8 |  | CM 2000 | evel of S | ervice |  | C |  |  |  |
| HCM 2000 Control Delay HCM 2000 Volume to Capacity ratio |  |  | 0.63 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 100.0 |  | Sum of lost | lime（s） |  |  | 18.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 58．8\％ |  | CU Level | Service |  |  | B |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |





|  | 9 | $\uparrow$ | $\stackrel{1}{1}$ | $\checkmark$ | $\downarrow$ | $\downarrow$ | 4 | $\triangle$ | $\downarrow$ | $\downarrow$ | $\checkmark$ | $\vartheta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | NBL | NBT | NBR | SBL | SBT | SBR | NEL | NET |  | SWL | SWT | SWR |
| Lane Configurations | \% | $\uparrow \uparrow$ | \% | \% ${ }^{*}$ | $\uparrow$ | 7 | $\dagger$ | $\uparrow$ | 7 | \% | $\uparrow$ | $\overline{7}$ |
| Traffic Volume (vph) | 80 | 360 | 150 | 520 | 430 | 190 | 240 | 320 | 90 | 150 | 220 | 380 |
| Future Volume (yph) | 80 | 360 | 150 | 520 | 430 | 190 | 240 | 320 | 90 | 150 | 220 | 380 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fit Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | 3433 | 1863 | 1583 | 1770 | 1863 | 1583 | 1787 | 1881 | 1599 |
| Fit Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1770 | 3539 | 1583 | 3433 | 1863 | 1583 | 1770 | 1863 | 1583 | 1787 | 1881 | 1599 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.94 | 0.94 | 0.94 | 0.96 | 0.96 | 0.96 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 87 | 391 | 163 | 553 | 457 | 202 | 250 | 333 | 94 | 158 | 232 | 400 |
| RTOR Reduction (vph) | O | 0 | 121 | 0 | 0 | 125 | 0 | 0 | 71 | 0 | 0 | 89 |
| Lane Group Flow (vph) | 87 | 391 | 42 | 553 | 457 | 77 | 250 | 333 | 23 | 158 | 232 | 311 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 1\% | 1\% | 1\% |
| Turn Type | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | pm+or |
| Protected Phases | 5 | 2 |  | 1 | 6 |  | 7 | 4 |  | 3 | 8 | 1 |
| Permitted Phases |  |  | 2 |  |  |  |  |  | 4 |  |  | 8 |
| Actuated Green, G (s) | 9.8 | 29.4 | 29.4 | 24.3 | 43.9 | 43.9 | 18.4 | 28.3 | 28.3 | 9.0 | 18.9 | 43.2 |
| Effective Green, g (s) | 9.8 | 29.4 | 29.4 | 24.3 | 43.9 | 43.9 | 18.4 | 28.3 | 28.3 | 9.0 | 18.9 | 43.2 |
| Actuated g/C Ratio | 0.09 | 0.26 | 0.26 | 0.21 | 0.38 | 0.38 | 0.16 | 0.25 | 0.25 | 0.08 | 0.16 | 0.38 |
| Clearance Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 150 | 904 | 404 | 725 | 711 | 604 | 283 | 458 | 389 | 139 | 309 | 684 |
| w/s Ratio Prot | 0.05 | 0.11 |  | c0. 16 | $\infty .25$ |  | 00.14 | c0.18 |  | 0.09 | 0.12 | 0.10 |
| w/s Ratio Perm |  |  | 0.03 |  |  | 0.05 |  |  | 0.01 |  |  | 0.10 |
| wic Ratio | 0.58 | 0.43 | 0.10 | 0.76 | 0.64 | 0.13 | 0.88 | 0.73 | 0.06 | 1.14 | 0.75 | 0.46 |
| Uniform Delay, di | 50.6 | 35.8 | 32.7 | 42.6 | 29.1 | 23.1 | 47.3 | 39.8 | 33.2 | 53.0 | 45.8 | 27.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 5.4 | 1.5 | 0.5 | 4.8 | 2.0 | 0.1 | 26.0 | 5.7 | 0.1 | 117.8 | 9.8 | 0.5 |
| Delay (s) | 56.0 | 37.3 | 33.2 | 47.4 | 31.1 | 23.2 | 73.3 | 45.5 | 33.2 | 170.8 | 55.6 | 27.5 |
| Level of Service | E | D | C | D | C | C | E | D | C | F | E | C |
| Approach Delay (s) |  | 38.8 |  |  | 37.2 |  |  | 54.0 |  |  | 64.4 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 47.4 |  | HCM 2000 L | evel of S | ervice |  | D |  |  |  |
| HCM 2000 Volume to Capacity rato |  |  | 0.78 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 115.0 |  | Sum of lost | ime (s) |  |  | 24.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 74.5\% |  | CU Level of | Service |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |





## APPENDIX H: GOOGLE MAPS PRINTOUT OF TRAFFIC CONDITIONS - DERRY AREA - JANUARY 2018









Thursday, January 25, 2018



APPENDIX I: HCM PRINTOUTS - UNSIGNALIZED INTERSECTION CAPACITY ANALYSES - 2015 AM AND PM PEAK HCM PRINTOUTS


| Major/Minor | Minor2 |  | Minor1 |  |  |  | Major |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1942 | 1943 | 1198 | 1940 | 1954 | 568 | 1212 | 0 | 0 | 571 | 0 | 0 |
| Stage 1 | 1209 | 1209 | . | 731 | 731 | . | . | . | . | . | . |  |
| Stage 2 | 733 | 734 | - | 1209 | 1223 | - | - | - | . | - | - |  |
| Critical Howy | 7.12 | 6.52 | 6.22 | 7.1 | 6.5 | 6.2 | 4.12 | - | - | 4.12 | - |  |
| Critical Howy Stg 1 | 6.12 | 5.52 | . | 6.1 | 5.5 | . | . | - | - | . | - |  |
| Critical Howy Stg 2 | 6.12 | 5.52 | - | 6.1 | 5.5 | - | $\cdot$ | - | - | $\cdot$ | - |  |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.5 | 4 | 3.3 | 2218 | - | - | 2.218 | . |  |
| Pot Cap-1 Maneuver | 49 | 65 | 226 | 50 | 65 | 526 | 576 | - | - | 1002 | - |  |
| Stage 1 | 223 | 256 | . | 416 | 430 | . | . | - | - | . | . |  |
| Stage 2 | 412 | 420 | - | 225 | 254 | - | - | - | - | - | . |  |
| Platoon blocked, \% |  |  |  |  |  |  |  | - | - |  | . |  |
| Mov Cap-1 Maneuver | 43 | 55 | 226 | 22 | 55 | 526 | 576 | - | - | 1002 | - |  |
| Mov Cap-2 Maneuver | 43 | 55 | . | 22 | 55 | . | . | . | . | . | . |  |
| Stage 1 | 191 | 252 |  | 357 | 369 | - | - | - | - | - | - |  |
| Stage 2 | 351 | 355 | - | 110 | 250 | - | - | - | . | - | - | - |


| Approach | SE | NW | NE | SW |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, | 43 | 11.9 | 1.5 | 0 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | M |  |  | $\uparrow$ | † |  |
| Traffic Vol, veh/h | 180 | 10 | 5 | 125 | 175 | 230 |
| Future Vol, veh/h | 180 | 10 | 5 | 125 | 175 | 230 |
| Conficting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channeized | . | None | - | None | . | None |
| Storage Length | 0 | . | - | . | - | . |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | $\cdot$ | - | 0 | 0 | - |
| Peak Hour Factor | 89 | 89 | 91 | 91 | 93 | 93 |
| Heavy Vehides, \% | 5 | 5 | 4 | 4 | 2 | 2 |
| Munt Flow | 202 | 11 | 5 | 137 | 188 | 247 |


| MajorMinor | Minor2 |  | Majort |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficing Flow All | 460 | 312 | 435 | 0 | . | 0 |
| Stage 1 | 312 | . | . | - | - | . |
| Stage 2 | 148 | $\cdot$ | $\cdot$ | - | - | - |
| Critical Hdwy | 6.45 | 6.25 | 4.14 | - | - | - |
| Critical Hdwy Stg 1 | 5.45 | . | . | . | - | . |
| Critical Hdwy Sigg 2 | 5.45 | $\cdot$ | $\cdot$ | - | - | - |
| Folow-up Hdwy | 3.545 | 3.345 | 2.236 | - | - | - |
| Pot Cap. 1 Maneuver | 554 | 721 | 1114 | - | - | - |
| Stage 1 | 735 | . | . | . | - | - |
| Stage 2 | 872 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | . | - | - |
| Mow Cap-1 Maneuver | 551 | 721 | 1114 | - | - | - |
| Mow Cap-2 Maneuver | 551 | . | . | - | - | - |
| Stage 1 | 735 | - | - | . | - | . |
| Stage 2 | 868 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | :--- | :---: |
| HCM Control Delay, s | 15.4 | 0.3 | 0 |


| Minor Lane/Major Mumt | NBL | NBT EBLL1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (vehhh) | 1114 | -558 | $:$ | $:$ |  |
| HCM Lane V/C Ratio | 0.005 | -0.383 | $:$ | $:$ |  |
| HCM Control Delay (s) | 8.2 | 0 | 15.4 | $:$ | $:$ |
| HCM Lane LOS | A | A | C | $:$ | $:$ |
| HCM 95th \%tile Q(veh) | 0 | $\cdot$ | 1.8 | $\cdot$ | $:$ |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | S8R |
| Lane Configurations | \% |  |  | $\uparrow$ | ち |  |
| Traffic Vol, vehh | 10 | 0 | 0 | 310 | 400 | 20 |
| Future Vol, vehh | 10 | 0 | 0 | 310 | 400 | 20 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | . | None |
| Storage Length | 0 | . | . | . | - | . |
| Veh in Mecian Storage, \#\# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | . | . | 0 | 0 | . |
| Peak Hour Factor | 44 | 44 | 95 | 95 | 96 | 96 |
| Heavy Vehides, \% | 79 | 79 | 4 | 4 | 6 | 6 |
| Munt Flow | 23 | 0 | 0 | 326 | 417 | 21 |


| MajorMinor | Minor2 |  | Major 1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficting Flow All | 753 | 427 | 438 | 0 | - | 0 |
| Stage 1 | 427 | . | . | . | - | . |
| Stage 2 | 326 | - | - | - | - | - |
| Critical Hdwy | 7.19 | 6.99 | 4.14 | - | - | - |
| Critical Hdwy Stg 1 | 6.19 | . | . | - | - | - |
| Critical Hdwy Stg 2 | 6.19 | - | - | - | - | - |
| Folow-up Howy | 4.211 | 4.011 | 2.236 | - | - | - |
| Pot Cap-1 Maneuver | 286 | 492 | 1111 | - | - | - |
| Stage 1 | 521 | . | . | . | . | . |
| Stage 2 | 587 | - | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mow Cap-1 Maneuver | 285 | 492 | 1111 | - | - | - |
| Mow Cap-2 Maneuver | $28 \%$ | . | . | . | . | . |
| Stage 1 | 521 | - | - | - | - | - |
| Stage 2 | 587 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | :---: | :---: |
| HCM Control Delay, S | 18.7 | 0 | 0 |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1111 | 286 | $\cdot$ | $\cdot$ |
| HCM Lane VIC Ratio | $\cdot$ | -0.079 | $\cdot$ | $:$ |
| HCM Control Delay (s) | 0 | $\cdot 18.7$ | $\cdot$ | $:$ |
| HCM Lane LOS | A | $\cdot$ | C | $\cdot$ |
| HCM 95th \%Ble Q(veh) | 0 | $\cdot$ | 0.3 | $\cdot$ |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL EBT |  | EBR | WBL | WBT | WBR |  |  | SER |  | NWT NWR |  |
| Lane Configurations |  | t |  |  | ¢ |  |  | 4 |  |  | 4 |  |
| Traffic Vol, veh/h | 35 | 270 | 5 | 30 | 385 | 10 | 10 | 5 | 30 | 10 | 5 | 35 |
| Future Vol, veh/h | 35 | 270 | 5 | 30 | 385 | 10 | 10 | 5 | 30 | 10 | 5 | 35 |
| Conficicing Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Slop |
| RT Channelized | - |  | None |  | - | None | . | . | Yield | . |  | None |
| Storage Length | - | - | . | - | - | . | . | . | . | . | . |  |
| Veh in Median Storage, \#t | - | 0 | - | - | 0 | - | - | 0 |  |  | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 89 | 89 | 89 | 96 | 96 | 96 | 65 | 65 | 65 | 67 | 67 | 67 |
| Heavy Vehicles, \% | 7 | 7 | 7 | 5 | 5 | 5 | 2 | 2 | 2 | 0 | 0 | 0 |
| Mumt Flow | 39 | 303 | 6 | 31 | 401 | 10 | 15 | 8 | 46 | 15 | 7 |  |


| Major/Minor | Major1 | Major2 |  |  |  | Minor2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficting Flow All | 411 | 0 | 0 | 309 | 0 | 0 | 884 | 857 | 406 | 858 | 859 | 306 |
| Stage 1 | . | - | . | . | . | - | 469 | 469 | . | 385 | 385 |  |
| Stage 2 | - | - | - | - | - | - | 415 | 388 | - | 473 | 474 |  |
| Critical Howy | 4.17 | - | - | 4.15 | - | - | 7.12 | 6.52 | 6.22 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | . | - | - | . | - | - | 6.12 | 5.52 | . | 6.1 | 5.5 | . |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | $\cdot$ | 6.1 | 5.5 | . |
| Follow-up Hdwy | 2.263 | - | - | 2.245 | - | - | 3518 | 4.018 | 3.318 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1121 | . | - | 1235 | . | . | 266 | 295 | 645 | 279 | 296 | 739 |
| Stage 1 | . | - | - | . | - | . | 575 | 561 | . | 642 | 614 |  |
| Stage 2 | - | . | - | - | - | - | 615 | 609 | - | 576 | 561 |  |
| Platoon blocked, \% |  | - | - |  | - | . |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1121 | - | - | 1235 | . | . | 228 | 273 | 645 | 239 | 274 | 739 |
| Mov Cap-2 Maneuver | . | - | - | . | - | . | 228 | 273 | . | 239 | 274 |  |
| Slage 1 | - | - | - | - | . | - | 551 | 542 |  | 615 | 588 |  |
| Stage 2 | - | - | - | - | - | - | 541 | 583 | - | 510 | 542 | - |


| Approach | EB | WB | SE | NW |
| :--- | :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 0.9 | 0.6 | 10.5 | 14.2 |
| HCM LOS |  | $B$ | B |  |


| Minor Lane/Major Mumt | NWLn 1 | EBL | EBT | EBR | WBL | WBT | WBR | SELn1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (vehhh) | 465 | 1121 | - | . | 1235 | . | - | 724 |
| HCM Lane V/C Ratio | 0.16 | 0.035 | - | - | 0.025 | . | - | 0.096 |
| HCM Control Delay (s) | 14.2 | 8.3 | - | . | 8 | 0 | - | 10.5 |
| HCM Lane LOS | B | A | - | - | A | A | - | B |
| HCM 95th \%tile Q(veh) | 0.6 | 0.1 | - | - | 0.1 | . | - | 0.3 |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 22.6 |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL | SWT |
| Lane Configurations | \% | 7 | $\uparrow$ | F |  | ¢ $\uparrow$ |
| Traffic Vol, vehh | 215 | 80 | 370 | 245 | 80 | 570 |
| Future Vol, vehh | 215 | 80 | 370 | 245 | 80 | 570 |
| Conflicting Peds, \#thr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | . | None | . | Yield | . | None |
| Storage Length | $\cdot$ | 150 | - | 0 | - | - |
| Veh in Median Storage, \#\% | 0 | . | 0 | . | - | 0 |
| Grade, \% | 0 | - | 0 | $\cdot$ | - | 0 |
| Peak Hour Factor | 83 | 83 | 86 | 86 | 81 | 81 |
| Heavy Vehicles, \% | 2 | 2 | 3 | 3 | 2 | 2 |
| Munt Flow | 259 | 96 | 430 | 285 | 99 | 704 |



$\sim$ Volume exceeds capacity $\$$ : Delay exceeds 300 s $\quad+$ : Computation Not Defined $\quad$ : All major wolume in platoon

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 11.2 |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | 7 | $\uparrow$ | ち |  | M ${ }^{1}$ |  |
| Traffic Vol, vehh | 15 | 720 | 645 | 40 | 80 | 35 |
| Future Vol, veh/h | 15 | 720 | 645 | 40 | 80 | 35 |
| Conficising Peds, \#fihr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | . | None | . | None | . | None |
| Storage Length | 0 | - | - | . | 0 | . |
| Veh in Median Storage, \# | . | 0 | 0 | . | 0 |  |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 84 | 84 | 89 | 89 | 83 | 83 |
| Heavy Vehides, \% | 7 | 7 | 4 | 4 | 6 | 6 |
| Mumt Flow | 18 | 857 | 725 | 45 | 96 | 42 |


| MajoriMinor | Major1 |  | Major2 |  | Mnor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficting Flow Al | 770 | 0 | . | 0 | 1640 | 747 |
| Stage 1 | . | . | . | . | 747 | . |
| Stage 2 | - | - | - | - | 893 | $\cdot$ |
| Critical Hdwy | 4.17 | - | - | - | 6.46 | 6.26 |
| Cofitical Hdwy Stg 1 | . | - | - | - | 5.46 | . |
| Cntical Hdwy Stg 2 | - | - | . | - | 5.46 | . |
| Follow-up Hdwy | 2.263 | - | - | - | 3.554 | 3.354 |
| Pot Cap-1 Maneuver | 823 | - | - | - | 108 | 406 |
| Stage 1 | . | - | . | - | 461 | . |
| Stage 2 | - | - | . | - | 393 | - |
| Platoon blocked, \% |  | - | - | . |  |  |
| Mov Cap-1 Maneuver | 823 | . | - | - | 106 | 406 |
| Mou Cap-2 Maneuver | . | - | - | - | 106 | . |
| Stage 1 | - | - | - | - | 461 | . |
| Stage 2 | - | - | - | - | 384 | - |


| Approach | EB | WB | S8 |
| :--- | :--- | ---: | ---: |
| HCM Control Delay, s | 0.2 | 0 | 143.2 |
| HCM LOS |  | F |  |


| Minor LaneMajor Mumt | EBL | EBT | WBT | WBR SELn1 |
| :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 823 | - | - | 137 |
| HCM Lane VIC Ratio | 0.022 | - | . | - 1.011 |
| HCM Control Delay (s) | 9.5 | - | - | 143.2 |
| HCM Lane LOS | A | - | . | - F |
| HCM 95th \%ole Q (veh) | 0.1 | - | - | 7.3 |


| Intersection |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, sweh | 76.6 |  |  |  |  |  |  |  |  |  |
| Infersestion LOS | F | ZRR |  | Bypz8 |  | $\mathrm{Byp}^{28}$ |  | EB |  | 102 W/S |
| Bsproash |  | WB |  | NB |  | SB |  | NE |  | SW |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |  | 1 |
| Cofflicing Cirde Lanes |  | 1 |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Fiou, vehim |  | 516 |  | 436 |  | 557 |  | 617 |  | 397 |
| Demand Flow Rate, vebh |  | 530 |  | 450 |  | 596 |  | 666 |  | 424 |
| Vehides Crolazing, vehh |  | 788 |  | 673 |  | Q58 |  | 629 |  | 1005 |
| Vehides Exitig, vehin |  | 335 |  | 622 |  | 732 |  | 665 |  | 312 |
| Folow-Up Headway, s |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.186 |  | 3.185 |
| Ped Vol Crossing Leg, 㔙 |  | 0 |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Ad |  | 1.050 |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, sweh |  | 77.5 |  | 29.5 |  | 83.5 |  | 96.6 |  | 86.1 |
| Approsch LOS |  | F |  | D |  | F |  | F |  | F |
| Lane | Lefl |  | Left |  | Left |  | Left |  | Left |  |
| Desigrated Mones | LR |  | LTR |  | LTR |  | LTR |  | LTR |  |
| Ass-mes Moves | LR |  | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channeliced |  |  |  |  |  |  |  |  |  |  |
| Lane Ut | 1.000 |  | 1.050 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Critcal Heatway, s | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Enry Flow, velith | 530 |  | 450 |  | 595 |  | 666 |  | 424 |  |
| Cap Emry Lane, vehín | 514 |  | 576 |  | 562 |  | 602 |  | 413 |  |
| Enroy HV Adj Factor | 0.973 |  | 0.970 |  | 0.936 |  | 0.526 |  | 0.935 |  |
| Flow Entry, veh/'h | 516 |  | 436 |  | 557 |  | 617 |  | 395 |  |
| Cap Enty, veh/h | 500 |  | 569 |  | 526 |  | 558 |  | 385 |  |
| VIC Rajo | 1.031 |  | 0.781 |  | 1.058 |  | 1.106 |  | 1.026 |  |
| Control Delay, siveh | 77.5 |  | 29.5 |  | 83.5 |  | 96.6 |  | 86.1 |  |
| LOS | F |  | D |  | F |  | F |  | F |  |
| 95\% \%sle Cusue, veh | 15 |  | 7 |  | 16 |  | 19 |  | 13 |  |




| Apporach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | :--- |
| HCM Control Delay, s | 237 | F | F | 3.6 |
| HCM LOS | F |  | 0.3 |  |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2 L |  | ${ }^{\circ}$ | C |  | E |
| Movement | EBL | EBR | NBL | NBT | S8T | SBR |
| Lane Configurations | M |  |  | $\uparrow$ | p |  |
| Traffic Vol, veh/h | 95 | 0 | 15 | 165 | 320 | 300 |
| Future Vol, veh/h | 95 | 0 | 15 | 165 | 320 | 300 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | . | None | - | None |
| Storage Length | 0 | . | . | - | - | - |
| Veh in Median Storage, \#\# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 91 | 91 | 82 | 82 |
| Heavy Vehicles, \% | 2 | 2 | 11 | 11 | 2 | 2 |
| Mvmt Flow | 101 | 0 | 16 | 181 | 390 | 366 |





| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4 | 44.5 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | S8R |
| Lane Configurations | M |  |  | 4 | † |  |
| Traffic Vol, vehh | 420 | 5 | 5 | 290 | 170 | 265 |
| Future Vol, veh/h | 420 | 5 | 5 | 290 | 170 | 265 |
| Conflicting Peds, \#ht | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | . | None | . | None |
| Storage Length | 0 | . | . | . | . | . |
| Veh in Mestian Storage, \# | 0 | $\cdot$ | - | 0 | 0 |  |
| Grade, \% | 0 | - | - | 0 | 0 | $\cdot$ |
| Peak Hour Factor | 90 | 90 | 87 | 87 | 87 | 87 |
| Heavy Vehicles, \% | , | 1 | 2 | 2 | 1 | 1 |
| Mumt Flow | 467 | 6 | 6 | 333 | 195 | 305 |



| Minor Lane/Major Mumt | NBL | NBT EBL.n1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (vehh) | 1064 | -410 | $\cdot$ | $:$ |  |
| HCM Lane VIC Raso | 0.005 | -1.152 | $\cdot$ | $:$ |  |
| HCM Control Delay (s) | 8.4 | 0 | 123.5 | $\cdot$ | $:$ |
| HCM Lane LOS | A | A | F | $\cdot$ | $:$ |
| HCM 95th \%tile Q(veh) | 0 | -17.8 | $\cdot$ | $:$ |  |

Notes
~: Volume exceeds capacity $\$$ : Delay exceeds 300 s $\quad+$ : Computation Not Defined *: All major volume in platoon


| Majorminor | Minor2 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1270 | 517 | 523 | 0 | . | 0 |
| Stage 1 | 517 | . | - | . | . | . |
| Stage 2 | 753 | $\cdot$ | $\cdot$ | - | - | - |
| Critical Hdwy | 6.46 | 6.26 | 4.11 | - | . | . |
| Critical Hdwy Stg 1 | 5.46 | . | . | . | . | . |
| Crifical Hodwy Stg 2 | 5.46 | $\cdot$ | - | - | - | - |
| Follow-up Hdwy | 3.554 | 3.354 | 2.209 | - | - | . |
| Pot Cap-1 Maneuver | 182 | 550 | 1049 | - | - | - |
| Stage 1 | 590 | . | . | - | - | - |
| Stage 2 | 458 | $\cdot$ | - | - | - | - |
| Platoon blocked, \% |  |  |  | - | - | - |
| Mor Cap. 1 Maneuver | 182 | 550 | 1049 | - | - | . |
| Mov Cap-2 Maneuver | 182 | . | . | - | - | - |
| Stage 1 | 590 | - | - | . | - | - |
| Slage 2 | 458 | - | - | - | - | - |


| Approach | EB | NB | SB |
| :--- | ---: | ---: | :---: |
| HCM Control Delay, s | 27.2 | 0 | 0 |


| Minor Lane/Major Mumt | NBL | NBTEBLT 1 | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 1049 | 182 | - | . |
| HCM Lane V/C Ratio | . | 0.11 | - | - |
| HCIM Control Delay (s) | 0 | - 27.2 | - | - |
| HCM Lane LOS | A | D | - | - |
| HCM 95th \%tile Q(veh) | 0 | 0.4 |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WER | SEL | SET | SER | NWL NWT |  | NWR |
| Lane Configurations |  | 4 |  |  | $\pm$ |  |  | $\dagger$ |  |  | 4 |  |
| Traffic Vol, veh/h | 45 | 665 | 5 | 30 | 375 | 20 | 20 | 10 | 70 | 5 | 10 | 50 |
| Future Vd, veh/h | 45 | 665 | 5 | 30 | 375 | 20 | 20 | 10 | 70 | 5 | 10 | 50 |
| Conflicting Peds, 期r | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | . | . | None | . | . | Yield | , | Siop | None |
| Slorage Length | - | - | . | - | - | . | - | - | . | - | - | . |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | . |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | . |
| Peak Hour Factor | 94 | 94 | 94 | 88 | 88 | 88 | 67 | 67 | 67 | 82 | 82 | 82 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mumt Flow | 48 | 707 | 5 | 34 | 426 | 23 | 30 | 15 | 104 | 6 | 12 | 61 |


| MajorMinor | Majort |  | Major2 |  |  | Minot2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficting Flow All | 449 | 0 | 0 | 713 | 0 | 0 | 1348 | 1315 | 438 | 1319 | 1323 | 710 |
| Stage 1 | - | - | - | . | . | . | 506 | 506 | . | 806 | 806 |  |
| Stage 2 | - | - | - | - | - | - | 842 | 809 | - | 513 | 517 |  |
| Critical Hdwy | 4.11 | - | - | 4.12 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | . | - | - | . | - | - | 6.1 | 55 | . | 6.1 | 5.5 | . |
| Critical Hdwy Stg 2 | - | - | - | $\cdot$ | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Folow-up Hdwy | 2.209 | - | - | 2.218 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1117 | - | - | 887 | - | - | 129 | 159 | 623 | 135 | 158 | 437 |
| Stage 1 | . | . | - | . | . | . | 552 | 543 | . | 379 | 398 | . |
| Stage 2 | $\cdot$ | - | - | - | - | - | 362 | 390 | - | 548 | 537 | . |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1117 | - | - | 887 | - | - | 94 | 140 | 623 | 94 | 139 | 437 |
| Mov Cap-2 Maneuver | . | - | - | . | . | . | 94 | 140 | . | 94 | 139 | . |
| Stage 1 | - | - | - | - | - | - | 513 | 515 | - | 352 | 370 |  |
| Stage 2 | - | - | - | - | - | - | 280 | 368 | $\cdot$ | 420 | 510 | - |


| Approach | EB | WB | SE | NW |
| :--- | ---: | :---: | ---: | :---: |
| HCM Control Delay, s | 0.5 | 0.7 | 22.5 | 23.7 |
| HCM LOS |  |  | C | C |


| Minor Lane/Major Mumt | NWLin | EBL | EBT | EBR | WBL | WBT | WBR SELIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Capacity (veh/h) | 271 | 1117 | - | . | 887 | . | 352 |
| HCM Lane VIC Ratio | 0.293 | 0.043 | - | - | 0.038 | - | - 0.424 |
| HCM Control Delay (s) | 23.7 | 8.4 | 0 | - | 9.2 | 0 | - 225 |
| HCM Lane LOS | C | A | A | - | A | A | - C |
| HCM 95\%n \%tie Q(veh) | 1.2 | 0.1 | . | - | 0.1 | . | , |


| $\begin{array}{ll} \text { Intersection } & \\ \hline \text { Int Delay, s/veh } & 28.8 \end{array}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| Movement | NWL | NWR | NET | NER | SWL |  |
| Lane Configurations | $\%$ | 7 | $\uparrow$ | ${ }^{7}$ |  | 4个 |
| Traffic Vol, veh/h | 180 | 120 | 580 | 410 | 115 | 570 |
| Future Vol, veh/h | 180 | 120 | 580 | 410 | 115 | 570 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channeized | . | None | . | Yield |  | None |
| Storage Length | - | 150 | - | - | . | . |
| Veh in Median Storage, \# | 0 | . | 0 | . | - | 0 |
| Grade, \% | 0 | - | 0 | - | . | 0 |
| Peak Hour Factor | 86 | 86 | 96 | 96 | 85 | 85 |
| Heavy Vehides, \% | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 209 | 140 | 604 | 427 | 135 |  |





| Major/Minor | Majorl |  | Mejor2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Confficting Flow Al | 956 | 0 | . | 0 | 2191 | 867 |
| Stage 1 | . | . | . | . | 867 | . |
| Stage 2 | - | - | - | . | 1324 | . |
| Critical Howy | 4.12 | - | . | - | 6.43 | 6.23 |
| Critcal Howy Stg 1 | . | - | - | - | 5.43 | . |
| Critical Howy Stg 2 | - | - | . | . | 5.43 | . |
| Follow-up Hdwy | 2.218 | - | - | . | 3.527 | 3.327 |
| Pot Cap-1 Maneuver | 719 | - | . | . | $\sim 50$ | 351 |
| Stage 1 | . | - | - | - | 410 | . |
| Stage 2 | - | - | - | - | 247 | . |
| Platoon blecked, \% |  | . | - | . |  |  |
| Mov Cap-1 Maneuver | 719 | - | - | . | -47 | 351 |
| Mov Cap-2 Maneuver | - | - | - | - | -47 | . |
| Stage 1 | - | - | - | - | 410 | - |
| Stage 2 | - | - | - | - | 232 | . |


| Approach | E8 | WB | S8 |
| :--- | :--- | :---: | ---: |
| HCM Control Delay, s | 0.4 | 0 | $\$ 656.1$ |
| HCM LOS |  | $F$ |  |



Notes
$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad 4$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intesection |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, sweh | 153.6 |  |  |  |  |  |  |  |  |  |  |
| Intersection LOS | F |  | EDR |  | Bye2r |  | Byp 28 |  | 102 ES |  | 102 ws |
| Afproach |  | WB |  |  | NB |  | SB |  | NE |  | SW |
| Entry Lanes |  | 1 |  |  | 1 |  | 1 |  | 1 |  | 1 |
| Corficting Circle Lanes |  | 1 |  |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Apprcach Flow, veth |  | 544 |  |  | 489 |  | 804 |  | 688 |  | 264 |
| Demand Flow Rate, vehh |  | 549 |  |  | 499 |  | 811 |  | 695 |  | 268 |
| Vehides Croulaing, vehh |  | 823 |  |  | 1065 |  | 556 |  | 862 |  | 964 |
| Vehives Exting, vetim |  | 726 |  |  | 502 |  | 677 |  | 504 |  | 413 |
| Folow-Up Headway,s |  | 3.186 |  |  | 3.186 |  | 3.186 |  | 3.186 |  | 3185 |
| Ped Val Crossing Leg, 䉼 |  | 0 |  |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Ad |  | 1.050 |  |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, siveh |  | 103.3 |  |  | 169.4 |  | 146.4 |  | 240.0 |  | 24.6 |
| Approsich LOS |  | F |  |  | F |  | F |  | F |  | - |
| Lane | Leff |  |  | Let |  | Leff |  | Left |  | Left |  |
| Desigrated Moves | LR |  |  | LTR |  | LTR |  | LTR |  | LTR |  |
| Ass-med Moues | LR |  |  | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channeliced |  |  |  |  |  |  |  |  |  |  |  |
| Lane Ut | 1.000 |  |  | 1.050 |  | 1.000 |  | 1.050 |  | 1.000 |  |
| Critical Headway, s | 5.193 |  |  | 5.193 |  | 5.193 |  | 5.193 |  | 5.193 |  |
| Entry Flow, veth | 549 |  |  | 499 |  | 811 |  | 895 |  | 268 |  |
| Cap Eniry Lane, vehin | 494 |  |  | 393 |  | 649 |  | 477 |  | 431 |  |
| Enty HV Adj Factor | 0.991 |  |  | 0.980 |  | 0.991 |  | 0.980 |  | 0.983 |  |
| Flow Entry, velh'h | 544 |  |  | 489 |  | 803 |  | 688 |  | 263 |  |
| Cap Enry, vel/h | 489 |  |  | 385 |  | 643 |  | 473 |  | 424 |  |
| VIC Rajo | 1.112 |  |  | 1.268 |  | 1.250 |  | 1.456 |  | 0.622 |  |
| Control Delay, siveh | 1033 |  |  | 169.4 |  | $14 \hat{6} 4$ |  | 240.0 |  | 24.6 |  |
| LOS | F |  |  | F |  | F |  | F |  | c |  |
| 95\% \%fle Cuese, veh | 18 |  |  | 21 |  | 30 |  | 34 |  | 4 |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WER | NBL | NBT | NBR | SBL | SBT | S8R |
| Lane Configurations |  | $\uparrow$ | F' |  | $\dagger$ |  |  | ¢ |  |  | \$ |  |
| Traffic Vol, veh/n | 10 | 40 | 435 | 5 | 30 | 20 | 200 | 435 | 10 | 25 | 290 | 15 |
| Future Vol, veh/n | 10 | 40 | 435 | 5 | 30 | 20 | 200 | 435 | 10 | 25 | 290 | 15 |
| Conficting Peds, \#̈hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | . | . | None | - | . | None | . |  | None | . |  | None |
| Storage Length | - | - | 0 | - | - | . | - | - | . | . | . |  |
| Veh in Median Storage, \# | - | 0 | . | - | 0 | - | - | 0 | - |  | 0 |  |
| Grade, \% | $\cdot$ | 0 | - | $\cdot$ | 0 | - | $\cdot$ |  | $\cdot$ | - | 0 |  |
| Peak Hour Factor | 88 | 88 | 88 | 82 | 82 | 82 | 93 | 93 | 93 | 91 | 91 | 91 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 0 | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 |
| Mumt Flow | 11 | 45 | 494 | 6 | 37 | 24 | 215 | 468 | 11 | 27 | 319 | 16 |


| MajorMinor | Mnor2 |  |  | Minor1 |  |  | Majorl |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficting Flow All | 1316 | 1291 | 327 | 1308 | 1293 | 473 | 335 | 0 | 0 | 478 | 0 | 0 |
| Stage 1 | 382 | 382 | . | 903 | 903 | . | . | . | . | . | . |  |
| Stage 2 | 934 | 909 | . | 405 | 390 | . | . | - | . | . | . | . |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.1 | 6.5 | 6.2 | 4.11 | - | - | 4.11 | - |  |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.1 | 5.5 | . | . | - | - | . | - |  |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.1 | 5.5 | $\cdot$ | - | - | - | . | - | - |
| Follow-up Howy | 3.518 | 4.018 | 3.318 | 3.5 | 4 | 3.3 | 2.209 | . | . | 2.209 | . | - |
| Pot Cap-1 Maneuver | 135 | 163 | 714 | 138 | 164 | 595 | 1230 | - | - | 1090 | - |  |
| Stage 1 | 640 | 613 | . | 335 | 359 | . | . | - | - | . | - |  |
| Stage 2 | 319 | 354 | $\cdot$ | 626 | 611 | - | - | - | - | - | . | - |
| Fatoon blocked, \% |  |  |  |  |  |  |  | - | - |  | - | - |
| Mov Cap-1 Maneuver | 80 | 120 | 714 | 24 | 121 | 595 | 1230 | - | - | 1090 | - |  |
| Mow Cap-2 Maneuver | 80 | 120 | . | 24 | 121 | . | . | - | - | . | - |  |
| Stage 1 | 488 | 594 | - | 255 | 274 | - | - | - | - | - | - |  |
| Stage 2 | 202 | 270 | - | 172 | 592 | . | - | - | - | - | . | - |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 25.6 |  |  | 76.5 |  |  | 2.6 |  |  | 0.6 |  |  |
| HCM LOS | D |  |  | F |  |  |  |  |  |  |  |  |





## APPENDIX J: 2040 AWDT PEAK HOUR VOLUMES

|  | 22-8pe-2 | TA3LE1-1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | rrea 5-17.17 | Adusted 2090 ARWDT and Frak Hour No-Euild volumes based an 2015 cousts |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 180 9.14 .17 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Inom |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | Sxametreses |  |  | momaction Tuming VSverest Cound |  |  | 16, | \|swfeax | Suspak |  |  |  |  |  |  |
|  |  | 2xt4 $\times 2015$ | 1175 |  |  |  | Forlt |  | - asc | 195 |  |  |  |  |  |  |
|  |  | 2015-37015 | 1500 |  |  |  | Hang |  | 0.56 | 2.98 |  |  |  |  |  |  |
|  |  | 2<tts3013 | 0.575 |  |  |  | luse |  | 0.56 | 2.96 |  |  |  |  |  |  |
|  |  |  |  |  |  |  | 3/ver |  | 1.06 | - 0.95 |  |  |  |  |  |  |
|  |  |  |  |  |  |  | Sest |  | 0.55 | 2907 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | Naph 510 |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2715261 |  |  |
|  |  |  |  |  | Cosesed | 252005 |  | coumed | $22^{2065}$ |  | 30t5wner | 200 Aniot | $x$ | MNOT | 3200 | 2090 |
|  |  | count | Fana | A 52065 | ant Prak | AMFeat | 20¢Pxic | Fat Prek | Pur Fosk | FXPfes | Exselitodes | Nosblid | Grove | 2300) 05 | vosed | Noss |
|  | Conat Locrion | Montive | มuwat | ARNOT | Voume | volune | Soldandy | notume | volun | Narawat | Resics | Axsigs | $2215 \times 5$ | 280000 | LVPr | Phat |
| Dery |  | Nar-15 | 15,585 | 25.195 | E36 | 809 | 5285 | 1513 | 1370 | \$15\% | 12905 | 2012 | 23787 | 115,584 |  |  |
|  | Foboom 26 W ot NH 128 | N0.0.35 | 12.58 | 21708 | T12 | 347 | 639\% | 1159 | 215 | 9596 | ES50 | 50537 | 17.808 | 13,835 | 828 | 1388 |
|  | Prekerson St E of Tiermess | nemers | 30722 | tess | evs | 60 | 6388 | 3287 | 589 | 9545 | 5775 | 6.395 \| | 22728 | 7,655 | 4s6\| | 227 |
|  |  | 960,25 | 5582 | 5336 | 453 | 454 | Escs | 581 | 500 | 9298 | 5,068 | 987 | 60128 | 8.658 | 353 | s00 |
|  | Tremmeat i d Pilerson | Mars5 | 25812 | 14.537 | 1713 | 2088 | 7308 | 1239 | 5483 | 2ases: | 14.200 | 58375 | 125386 | 19,450 | 5420\| | 15537 |
|  | NT1ELE EfN- 283noss | Mer-35 | 7855 | 7230 | 585 | 512 | 7358 | 651 | 42 | 8.515 | 7,005 | 6135 | -12 280 | 6.328 | 439 | 565 |
|  | W4 is 9ra, N ot hasemy 0 or | Neres 36 | 8.515 | 1000 | 756 | 735 | 1505 | 881 | 963 | $30.17 \%$ | 2,358 | 2353 \| | -450008 | 3.275 | 339\| | 335 |
|  | k+293pra Not Tremears | varss | 22250 | 12940 | 398 | 358 | 50\% | 1231 | 177 | \$359x | 3,307 | 4002 | -35370 | 5238 | $4: 6$ | 511 |
|  |  | varsis | 24.302 | 13.988 | 1215 | 1065 | 7.826 | 2338 | 1364 | seex | 12.207 | 7,327 | 40.088 | 8379 | 633] | 317 |
|  |  | Age.3e | 15623 | 15.830 | 1580 | 1737 | E17\% | 2228 | 1212 | 3215 | 15,008 | 2,330 | 15,60\% | 29,0es | 1299 | $120 \cdot$ |
|  |  | Age-st | 54.230 | 16.575 | 127 | 903 | 578 | 2128 | 1237 | 1305 | 12,128 | 1468 | 335150 | 29513 | 1312] | 1535 |
|  | Foedswy mer 3ewer Sood | 2xe-34 | 5500 | 5.838 | 511 | 358 | 7.0es | 482 | 005 | Esers | 5.124 | 3.511 | 71.350 | 13921 | 271 | 307 |
|  |  | Apese | 2735 | 2,800 | 159 | 125 | 5715 | 172 | 169 | sirs | 1,254 | 2999 \| | 56.2008 | 2375 | 358 | 260 |
|  | Rassizilondondery ismilio | Ase-st | 5955 | 7,130 | 407 | 2Ss | 5.488 | 72 | 72 | 20.09\% | 5,538 | 13,730 | 1373180 | :656s | 1256 | 1551 |
|  |  | 20.15 | 23.234 | 12,130 | 1235 | Ses | 750\% | 1176 | 1206 | E.4\% | 13, 215 | 12.253 | -30.823 | 20,399 | 780 | 834 |
|  |  | 20.25 | \$,200 | 3,200 | 54, | 600 | 817\% | 345 | 307 | 3865 | 30,839 | 12,78 | 17900 | 5.571 | 780 |  |
|  | nexat |  |  |  |  |  | 7.118 |  |  | 9.788 |  | $22, \mathrm{k}$ |  | 2,37 | $\cdots$ | Sse |
| -seny | NW 100, t efthenpoon or | 125 | 31,128 | 31,300 | 3438 | 2ST | 3288 | 2842 | 228 | 378 |  |  |  |  |  |  |
|  | SW500, Eet Exic |  |  | 25800 | 2100 |  | 7396 | 2505 |  | 3005 | 20115 | 32,416 | 5568 | 4.378 | 338 | 4350 |
|  | \|whseesa Doury Toun line | Merel 15 | 22,856 | 28.890 | 178 | 35es | 10tx | 1756 | 2750 | 757x | 22383 | 29.504 | 3278 | 29,763 | 3145 | 3338 |
|  | SW28at Sers Town live | Nusplis | 173,34 | 25935 | 2239 | 1238 | ग278 | 1582 | 2508 | 930\% | 15392 | 15,683 | - -535 | 13,621 | 490 | 236 |
|  |  | See 15 \| | 36.536 | 2esse | 5037 | 2335 | 8397 | 1207 | 2710 | 3078 | $15 \times 08$ | 34739 | 4378 | 13,359 | 1291 | 123 |
|  |  | menel25 | 305\% | 5.313 | eso | 658 | 6315 | 3308 | 589 | 12005 | 5,397 | 56,439 | 74908 | 17,174 | 1770 | 1138 |
|  |  |  |  | 4512 | 215 | 215 | 4585 | 4 SE | C/5 | 30.065 | 4.742 | $44^{3} 3$ | $17 \%$ | - 5301 | 1251 | 20.8 |
|  |  | J.e. 15 | 6502 | 6531 | 47 | ess | Esas | 73 | 583 | 30328 | 5,909 | S2000 | 235398 | 15512 | zove | 459 |
|  | average |  |  |  |  |  | 729\% |  |  | 9315 |  |  |  |  |  | 1500 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | vas-i6 | 20.263 | 3,993 | 435 | 545 | 4.186 | 1223 | 1599 | 278006 | 12,35s | 20215 | Scses6 | 29,484 | 813 | 2933 |
|  | bxt 4 secoram | 4592. 6 | 20303 | 12005 | 273 | 1535 | 12388 | \$12 | 7s\% | 7328 | 9,550 | 2, 2631 | 123, 2580 | 22,43 | 2915 | 1773 |
|  | bet 453 cos | vap: 6 | 5 sec | 3, $6 \times 5$ | 733 | 723 | 7588 | 58 | 933 | E7cs | 3.150 | 15.349 | 1235958 | 21.593 | 1625 | 3099 |
|  | fat 438 Cncamp 63 2053 | vaple | 5.300 | 5.177 | 573 | 505 | 1228\% | 312 | 3cs | 5355 | 4,900 | 12778 | 129, $55 \times 8$ | 11301 | 1413 | 520 |
|  | Ext4sa On-amp-we cosa | Mop-16 | 4 SET | 5.688 | 537 | 505 | 11.125 | 344 | 23 | 5168 | 3,630 | 7,488 | 153530 | 9.850 | 2059 | tus |
|  | 2erata |  |  |  |  |  | 9.128 |  |  | E13\% |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Eat5x30tamp | Nope 15 | 5.745 | 5.5001 | 450 | 336 | 6ssk | 472 | 259 | 827\% | 2,438 | 5,421 | 45.508 | 33 | 55 | 665 |
|  | Fal $5 \times 30 \mathrm{comm}$ | Nap 15 | 3.580 | 2341 | 958 | 552 | 30.1\% | 73 | 77 | 3.328 | 2.500 | 13, 258 \| | 58337 | 21.355 | 1612 | 1152 |
|  | Faks 53 Otramo | Nop-15 | $3 \times 20$ | 9282 | 781 | 750 | *085 | 939 | 920 | 30.5 | 5238 | 13,577 | 47039 | 13,6es | 1153 | 1353 |
|  | feit5sacomen | Mept 15 | 5,655 | 5.508 | S3 | cse | 95S6 | 487 | $4: 8$ | 7.5\% | 3319 | 5884 | 50243 | 5,254 | 748 | 628 |
|  | avoze: |  |  |  |  |  | 8543 |  |  | 358\% |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 193, south er eret 4 \|Dat Paix |  |  | 71.060 |  | 5420] | 1599 |  | S*RO | 8.20x | 72373 | 123.509 | 54:383 | 215.183 | 8.504 | 5.545 |
|  | 38 |  |  | 35700 |  | 1580 | 35s\% |  | 3070 | Sx15 | $38 \leqslant 17$ | 59236 | cesse | \$3,138 | 3.283 | 5.502 |
|  | 58 |  |  | 35375 |  | 384 | 885s |  | 12050 | 42\% | 35.951 | 59,574 | 65958 | 53,6:0 | S8501 | 4042 |
|  | 153, buteena Exas 4 tod5 |  |  | 71000 |  | 5855 | 7348 |  | 5835 | \%28s | 7.152 | 120205 | 63906 | 179,508 | 5538 | 5.948 |
|  | s3 |  |  |  |  | 1930 | 45es |  | 30085 | sezs | 35.578 | 50.363 | 63.6880 | - | 4.483 | 5.051 |
|  | 53] |  |  |  |  | 3312 | 53.65 |  | 3870 | 43.85 | 35.500 | Se342 | 63728: | - | sess | 4899 |
|  | Y-33, norbe el bxi 5 |  |  | n,000 |  | 5435 | 12458 |  | 669 | 850\% | 38.139 | 134585 | 65.37* | 125,245 | 12550 | 12.130 |
|  | 53 |  |  |  |  | 3200 | 6958 |  | 3325 | 4978 | 20,250 | 50, 250 | 57.60x | - | 5.850 | 5,332 |
|  | 33) |  |  |  |  | 1225 | 502\% |  | 3395 | sark | 40,889 | 50.535 | 65.17x | . | 5,385 | 5,598 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  | Countrs | $2 \leq 52005$ |  | Coumber | 2612005 |  | 2015 NNDC | zeenwat | \% | mawat | 20es | 2200 |
|  |  |  |  | 2652015 | ane Peak | avPreak |  | PMineak | netmok | Puras | Sios Mosel | v2.3uat | Gxath | 20ans | Noab | Nasa |
|  |  |  |  | anmot | volume | nolume | Natawnat | valume | Volure | 5 StMENST | kajes | AuFter | 2685-09 | nasiot | AMFX | FMP\% |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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