

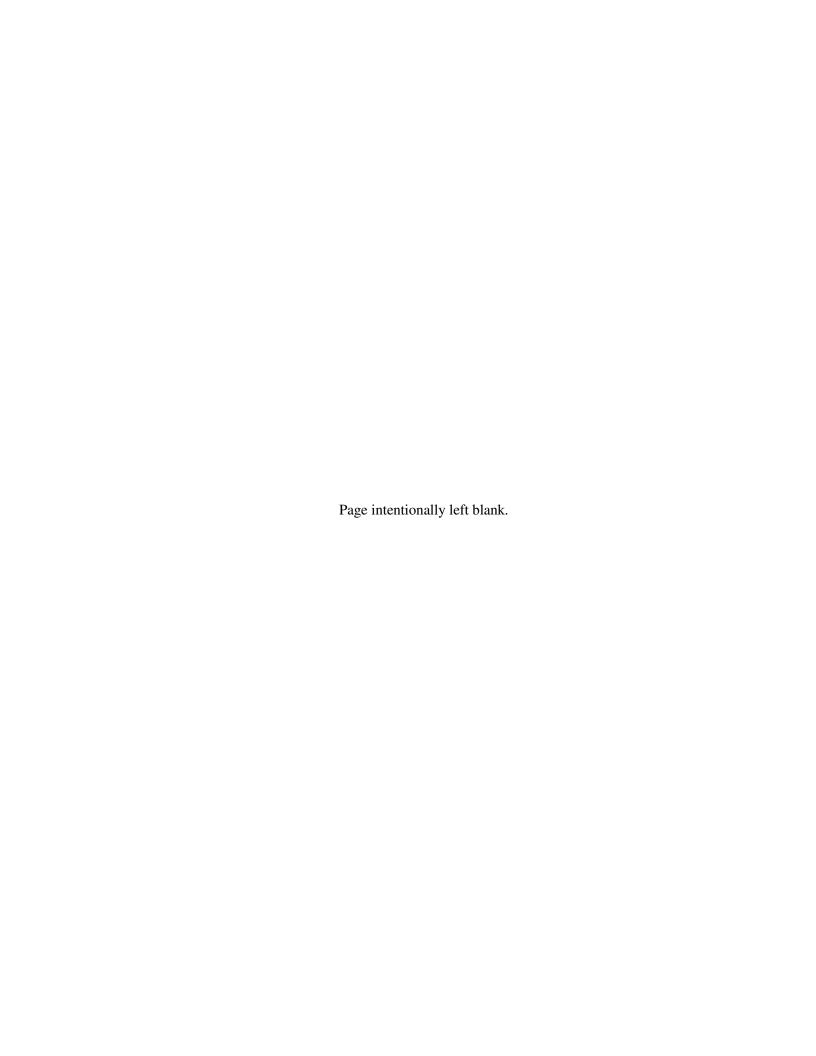
Bridge Design Manual Chapter 10 Non-Bridge Structures

January 2015 – v 2.0 (Revised August 2019)



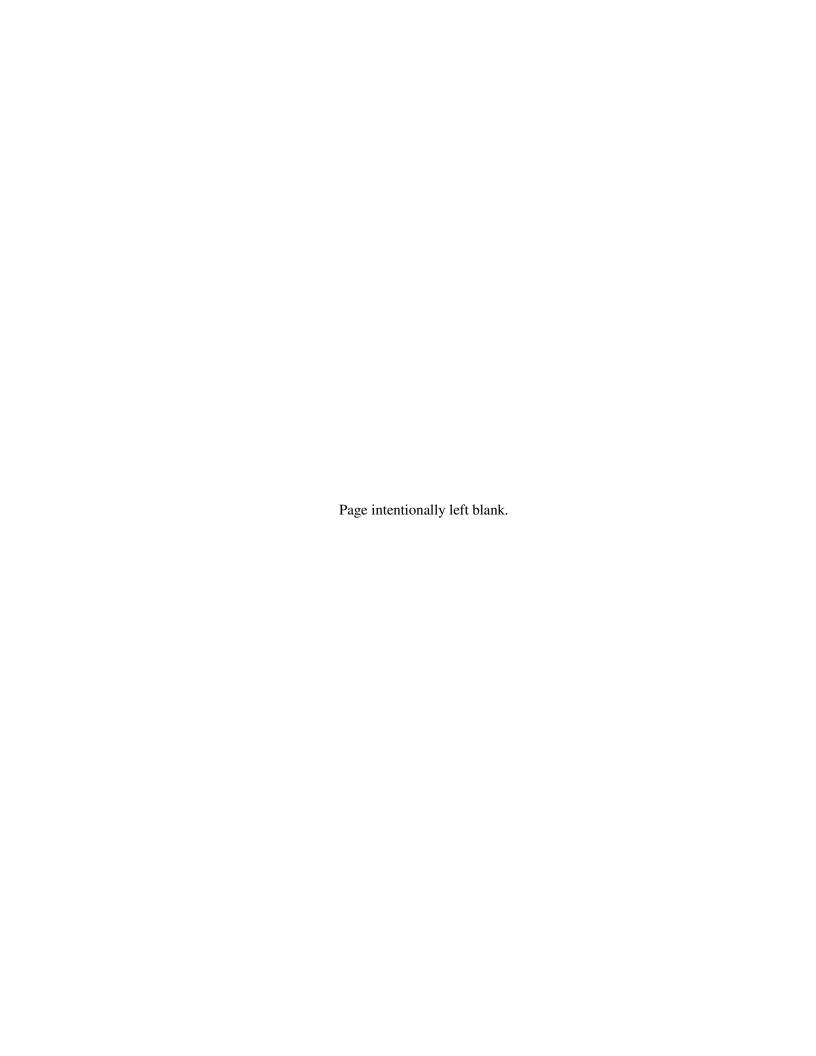






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Chapter 10

Non-Bridge Structures

10.1 General

The Bureau of Bridge Design provides design support for miscellaneous structures that are part of projects from other bureaus such as Highway Design, Traffic, Transportation Management Center (TMC) and Districts. These structures include overhead sign structures, bridge-mounted sign supports, non-standard traffic signal support structures, intelligent transportation systems (Closed Circuit Television, Road and Weather Information Station Systems and Non-Invasive Pavement Sensor Systems), support structures, and soundwalls. Design assistance should be requested through the Administrator of the Bureau of Bridge Design or through the Design Chiefs.

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10.2 Loads

A. General

Overhead signs, bridge-mounted signs, non-standard traffic signals, intelligent transportation systems (CCTV, Road and Weather Information Station Systems, and Non-Invasive Pavement Sensor Systems), luminaire support structures, and the foundations shall be designed in accordance with the current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims, NHDOT Standard Specifications for Road and Bridge Construction, NHDOT Bridge Design Manual, and any special provisions.

B. Dead Loads

Sign

(Incl. weight of sign & attachments (3 psf [14.6 kg/m²]) and weight of W6x9 sign support (typically avg. 2 psf [9.8 kg/m²])

 $5.0 \text{ psf} (24.4 \text{ kg/m}^2)$

- Dynamic Message Sign (DMS)
- Variable Speed Limit Sign (VSLS)
- Luminaire
- Standard Signal Head
- Bridge Mounted Sign Supports
- Structural Members
- Maintenance Walkway
- Closed Circuit Television

per manufacturer

per manufacturer per manufacturer

per manufacturer

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C. Wind Loads

- The 3-second wind gust map in the AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals shows the basic wind speed to be used when computing design wind pressure.
- Basic wind speed of 100-mph (160-km/hr) shall be used for the entire state of NH except in the Special Wind Region (i.e. regions along the NH-VT border and Franconia Notch) as shown in AASHTO Specifications, Fig. 3.8.3-5. The maximum-recorded wind speed in this area shall be used as the basic wind speed if it is greater than the NH basic wind speed of 100-mph (160-km/hr). See the wind speed map located at http://www.windspeedbyzip.com/, Appendix 10.2-A1, and weather stations in the special wind region for recorded wind speeds.
- D. Design Life and Recurrence Interval (*Table 3.8.3-1,2,3 AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals*)
 - 50 years for all overhead sign structures (i.e. bridge or cantilevered), bridge-mounted sign supports, traffic signal mast arms with/without luminaires (all heights), ITS support poles, and lighting poles when the horizontal distance from roadway to pole ≤ height of pole.
 - 25 years for ITS support poles, lighting poles when the horizontal distance from roadway to pole > height of pole, and soundwalls.

E. Ice Loads

- 3-psf (14.6-kg/m²) applied around all the surfaces of the structure and attachments but applied to only one face of sign panels per AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals.
- 3-psf (14.6-kg/m²) applied to the top, ends, and one face of a DMS or VSLS.

F. Snow Loads

• 40-psf (195.3-kg/m²) applied simultaneously with ice load to the top panel and any other nearly horizontal projection surfaces of a DMS or VSLS.

G. Fatigue Design:

Fatigue design shall conform to AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals and the following categories:

- 1) Cantilevered Fatigue Category I:
 - All overhead cantilever sign structures
 - ⇒ Galloping loads may be excluded for fatigue design of overhead cantilevered sign structures with four-chord horizontal trusses.
 - All bridge-mounted sign supports
 - High-mast lighting poles (horizontal distance from roadway to pole ≤ height of pole)
 - ITS support poles (horizontal distance from roadway to pole ≤ height of pole)
 - Typical lighting poles with mast arm (horizontal distance from roadway to pole ≤ height of pole)
- 2) Cantilevered Fatigue Category II:
 - All traffic signal supports (mast arms)
 - \Rightarrow Natural Wind Gust loading shall be <u>included</u>.
 - ⇒ Truck Induced Gust loading and Gallop loading may be <u>excluded</u>
 - ITS support poles (horizontal distance from roadway to pole > height of pole)
 - Typical lighting poles with mast arm (horizontal distance from roadway to pole > height of pole)
 - High-level (high-mast) lighting poles (horizontal distance from roadway to pole > height of pole)
- 3) Non-Cantilevered Fatigue Category I:
 - Overhead bridge sign structures located along the Turnpike, Interstate, and Interstate ramps
- 4) Non-Cantilevered Fatigue Category II:
 - Overhead bridge sign structures located on non-Turnpike, non-Interstate, NH, and US numbered routes
- H. Live Load: A live load consisting of a single load of 500-lbs. (226.8-kg) distributed over 2.0-ft. (0.6-m) transversely to the member shall be used for designing members for walkways and platforms (See AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, Section 3.6).

Support structures shall be designed using the maximum of the four load groups noted in AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, Section 3.4 and Table 3.4-1.

10.3 Overhead Sign Structures

10.3.1 General

The design of overhead sign structures is a combined effort between the Bureau of Bridge Design and the supplier of the structure. Bridge Design is responsible for the preliminary and final design of the foundations for overhead sign structures for In-House projects. Consultants are responsible for the preliminary and final design of the foundations, with the guidance from Bridge Design, for Consultant projects. The supplier of overhead sign structures is responsible for the design of the structure and submits shop drawings to the Department for approval. The supplier's calculations and shop plans are reviewed for general conformity with Contract Plans and NHDOT's policies and specifications.

10.3.2 NHDOT Design Requirements

A. Structure

- Overhead sign structures shall be designed to accommodate sign surface areas 30 percent greater than those shown on the plans, unless otherwise noted.
- The structures shall be galvanized steel in accordance with NHDOT Specification 550.2.9.
- Provide a 3-foot (1-meter) walkway with OSHA approved railing for access to any electronic message signs on overhead structures. The walkway shall extend to the edge of pavement to provide access to the DMS without having to use a bucket truck over the travel lane, or having to shut down travel lanes.
- The structure shop plans and calculations shall be prepared and stamped by a professional engineer licensed in the state of New Hampshire.
- 25 percent of the base plate-to-post weld shall be inspected by magnetic particle testing per AASHTO Specifications. This requirement shall be noted on the shop plans.
- Sign support members (W6x9) shall not be greater in length than the sign height.
- The Fabricator shall furnish a complete set of shop drawings and design calculations, along with the design forces and offsets, as noted in Special Provision Amendment to Section 615, Traffic Signs.
- The connection of the structure to the foundation shall be a double-nut moment connection.
- Lock washers shall <u>not</u> be used with the installation of high strength bolts per FHWA Guidelines.
- Triangular truss and tubular arch type overhead sign structures, as shown below, are <u>not</u> permitted due to concerns with their susceptibility to fatigue cracking.





- NHDOT permitted sign structure types include the following (see Figure 10.3.2-1):
 - 1) truss upright, truss horizontal
 - 2) monotube upright, truss horizontal
 - 3) monotube upright, monotube horizontal



monotube upright, truss horizontal



monotube upright, monotube horizontal



truss upright, truss horizontal



truss upright, truss horizontal

NHDOT Sign Structure Types

Figure 10.3.2-1

B. Foundation

- Spread footing foundations shall be used for all sign structures, unless directed otherwise by the Geotechnical Engineer.
- NHDOT policy for maximum allowed area of footing with uplift shall be the following:
 - \Rightarrow Sign bridge structure = 5 % of footing area.
 - \Rightarrow Cantilevered sign structure = 1 % of footing area.
- Use the same reinforcing bar size for both directions in the footing.
- The vertical stem reinforcing bars shall be checked for development length, into both the stem and footing.
- The overlap length of the vertical reinforcing bar and anchor rod shall be checked that the length is equivalent to a class c splice of the reinforcing bar.
- The distance from the top of the concrete stem to the bottom of the sign structure base plate shall equal the nut height plus 1-inch (25-mm) (preferred) or nut height plus the anchor rod diameter (maximum). (Note the nut height equals the rod diameter.)
- Anchor rods shall conform to the requirements of ASTM F1554 Grade 55 (minimum).
 ASTM A615 reinforcing steel is not permitted. Galvanize the entire anchor rod per
 ASTM A153. Each anchor rod shall be supplied with a minimum of two hex nuts
 (ASTM A563 or ASTM A194) and a minimum of two flat hardened washers (ASTM F436).
- Anchor rods shall include hardened washers. Lock washers shall not be used as they do
 not prevent loss of the anchor bolt preload, and their variability of deformation under
 load does not provide for proper bolt tension during installation.
- Anchor rod size and layout shall be designed by the structure Fabricator and shall be identical for both left and right footings.
- For sign structures that are designed for Cantilevered Fatigue Category I, the anchor rods shall be designed for wind-induced cyclic loads per *AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, 5.17.3.4.*
- Each monotube upright post shall have a minimum of eight (8) foundation anchor rods. Each post of a multi post upright (truss) shall have a minimum of four (4) foundation anchor rods per post.
- The connection of the structure to the foundation shall be a double-nut moment connection.
- Grout shall <u>not</u> be used between the structure base plate and the top of the footing. The grout on existing footings has cracked, allowing water and chlorides to stay in the cracks and not dry out, which has led to corrosion of the anchor rods.
- A stainless steel standard grade wire cloth (1/4-in. (6.4 mm) maximum opening with minimum wire diameter of AWG No. 16) shall be installed around the structure base plate and top of footing with a 2-inch (51 mm) lap as shown and noted on the footing plans. The screen is to prevent debris from collecting beneath the base plate, keep animals out, and protect the electrical wires.
- Typical NHDOT sign footing plan is shown in Appendix 10.3-B1.
- Cofferdams, Item 503.20x may be required if there is insufficient room to excavate for the footing using 1.5:1 cut slopes. Cofferdams with Sheeting Left-in-Place, Item 503.30x, should be used when its removal would create a stability problem with adjacent

structures of any type, including roadways and drainage, the sign structure itself or as required by the geotechnical engineer.





Typical NHDOT Sign Structure Footing

Figure 10.3.2-2

C. Geometry

- The top of the concrete stem shall be placed 3-inches \pm (76-mm) higher than the adjacent highest finished grade.
- The bottom of the foundation shall be placed a minimum of 5'-0" (1.5-m) below the lowest finished grade (normal to the ground surface) for frost cover.
- The upright face of the sign structure which is closest to traffic shall be located outside the clear zone. However, if the sign structure cannot located outside the clear zone, the upright face closest to traffic shall be located a minimum of 10-ft. (3-m) behind the guardrail for any Interstate or Turnpike location. Any exception to this shall be approved by the Bureau of Traffic.
- Overhead signs shall provide a vertical clearance of 17'-6" (5.3-m) [18'-0" (5.5-m) preferred by Bureau of Traffic] over the entire width of the travel way and shoulders.
- The maximum overhead cantilever sign structure span is 50-ft. (15-m). Any exception to this shall be approved by the Design Chief, Bureau of Bridge Design.
- The foundation and structure shall be located within the state owned right-of-way, and without interference with utilities, drainage pipes, or structures.

10.3.3 Installation

- The foundation shall be constructed and the sign structure installed according to NHDOT Standard Specifications for Road and Bridge Construction, Section 615 Traffic Signs, and the Special Provision, Amendment to Section 615 Traffic Signs.
- The Special Provision, Amendment to Section 615 Traffic Signs, shall be included in all project proposals that have a sign structure. This special provision addresses the anchor rod installation and pretensioning procedures for the double-nut connection to the foundation.
- The structure shall not be placed onto the leveling nuts until the foundation concrete has cured for at least 7 days or attained at least 80 percent of its design compressive strength.
- Sign mounting brackets shall be attached to the structure utilizing only bolted connections, which allow complete lateral and vertical adjustment of the sign over the roadway, as noted in Section 615.
- Foundation must be backfilled to the elevation shown on the plans, prior to installation of the sign structure.
- When the sign panels are not installed immediately upon installation of the structure, an equivalent loading, such as dampers, shall be installed temporarily for mono-tube cantilever structures only.

10.3.4 Design Guidelines

A guideline for the review of the sign structure shop plans and design, and drawing of the foundation plan, can be found in Appendix 10.3-A1. A sample plan of a sign footing can be found in Appendix 10.3-B1.

If the site being considered for a sign structure has poor soil conditions, a decision must be made on whether to use a bridge sign structure with two foundations or a cantilevered sign structure

with one foundation on piles, a cost comparison will usually show that the cantilevered sign structure with one foundation on piles is approximately twice the cost of a bridge sign structure. The pile foundation cost is higher due to the cost of providing pile driving equipment.

10.3.5 Design Process and Coordination

- 1) Upon initiation of a design for a new sign structure, the lead Bureau shall request borings and shall provide the following to the Bureau of Materials and Research:
 - Roadway plan and cross-sections showing the proposed location of the structure(s) and boring location by station and offset.
 - One boring should be requested for each foundation. If poor soils are encountered, the designer shall be contacted to determine if a boring should be taken at another location (i.e., the location moved or a sign bridge structure could be used at the location instead of a cantilever structure).
- 2) The lead Bureau then requests a preliminary sign footing size and quantities from the Bureau of Bridge Design or the design Consultant. The request should include the following:
 - A "stick diagram" for each structure indicating the structure location, span, offset, signs, sign location on the structure, elevations, vertical clearance, dimensions, and any other attachments to the structure.
 - Roadway plan and cross-sections showing the proposed location of the structure(s).
 - Any other information that may affect the final location of the sign foundation.
- 3) In response to the Preliminary Sign Footing Request, the Bureau of Bridge Design or the design Consultant shall provide the following to the lead Bureau:
 - Approximate footing dimensions for each structure.
 - A cross-section of each structure with the preliminary footing drawn on the section, indicating the top and bottom footing elevations and showing cofferdams, if required.
 - Estimated quantities for construction of the footing:
 - ⇒ Item 206.1, Common Structure Excavation
 - ⇒ Item 503.20x, Cofferdams (if required)
 - ⇒ Item 503.30x, Cofferdams with Sheeting Left-in-Place (if required)
 - ⇒ Item 508, Structural Fill (if required)
 - ⇒ Item 520.2, Concrete Class B
 - ⇒ Item 544.1, Reinforcing Steel (Roadway)
 - Appendix 10.3-A2 provides tables of data for bridge and cantilever sign structures and their foundation that have been designed and constructed. This information is for reference only and can be used for preliminary estimates for footing dimensions and quantities.

4) Contract Plan Stage

The lead Bureau or design Consultant shall transfer the preliminary sign footing information onto the contract plans. The contract plans and/or proposal shall include the following:

- "Stick diagram" of each structure with the latest information showing the structure location, span, offset, signs, sign location on the structure, elevations, vertical clearance, dimensions, and any other attachments to the structure.
- Sign Text Layout Plan
- General Roadway Plan showing the structure and foundation locations
- Cross-sections showing the structures and foundations (transferred from the preliminary sign footing cross-section).
- Special Provision, Amendment to Section 615 Traffic Signs
- The project estimate shall include funds for structural steel inspection during fabrication of the sign structure (approximately \$2,000 for each structure).

5) Award of the Contract Stage

- The Contractor shall submit a complete set of sign structure shop drawings and design calculations, along with the design forces and offsets, as noted in Section 615.3.4.1.2, Structure Requirements, of the Special Provision Amendment to 615, Traffic Signs.
- The Bureau of Bridge Design, or the design Consultant, shall review the Fabricator's sign structure calculations and shop plans for conformity with the contract plans, proposal, specifications, and NHDOT policy. The shop plans shall be stamped "Approved", "Approved Except as Noted", or "Disapproved" and returned to the Bureau of Construction for distribution to the Contractor, Traffic Bureau, Steel Fabrication Inspector, and Fabricator.

The review shall conform to the requirements of the following:

- Contract plans
- o Addendums
- Specifications
- Special Provision, Amendment to Section 615
- o NHDOT Bridge Design Manual, Chapter 10 Non-Bridge Structures
- o Sign Structure and Footing Design Guidelines (Appendix 10.3-A1)

•	The Bureau of Bridge Design or the design Consultant will design the sign
	structure footing(s) using the design loads provided by the Fabricator of the sign
	structure. A footing plan shall be prepared (See Appendix 10.3-B1 for a sample
	Sign Structure Footing Plan) and shall include the following:

Plan, elevation, and sectional view of footing
Reinforcing layout and schedule
Item numbers and quantities
Item number of structure
Notes
Detailed description of the footing location (obtain from the Bureau of
Traffic; the description shall be more than the structure stationing)
Traffic Inventory Number (obtain from the Bureau of Traffic)

		 □ Plan file number (Assign file number as instructed in the Sign Footing File Number document [S:\Bridge-Design\FORMS\PROJECT\Sign Footing Plan File Number.xls]) □ Anchor Rod detail as shown on the sample footing plan □ Pay limits of Items 206.1 and 508 (if required) 	
6)	Distrib	ution of Plans	
	 Distribute the following to the <u>Bureau of Construction</u>: Electronic copy of the sign structure footing plan(s). Electronic copy of "Approved" stamped sign structure shop plans. 		
	•	Distribute the following to the <u>Fabrication Engineer</u> , <u>Bureau of Bridge Design</u> : One (1) paper or electronic copy of the "Approved" stamped sign structure shop plans with a transmittal letter noting the project name, number, sign structure location, name of fabricator, and noting that the copy is to be distributed to the shop inspector.	
	•	Email the <u>Bureau of Traffic Engineering Section</u> , noting that a copy of the "Approved" stamped sign structure shop plans and foundation drawings were scanned and placed as noted below in "Archiving the Plans".	
7)	Archiv	ing the Plans	
		gn structure shop plans and footing plans are stored in the Bureau of Bridge. The following shall be filed in Bridge Design for future reference:	
		One (1) full size plan(s) of the sign structure footing, filed in the tub per the file number.	
		A folder labeled with the sign structure project name and project number, and placed in the Sign Structure file cabinet. The folder shall contain the following: □ Half-size paper copy of the "Approved" stamped sign structure shop plans ⇒ Mark the Traffic Inventory Number for the structure on the corresponding shop plans for future reference □ Design calculations of the sign structure and footing □ Half-size paper copy of the sign structure footing plans □ "Stick Diagrams" of each structure from the contract plans □ Cross-section of each structure from the contract plans (Note: The final footing needs to be sketched on the cross-sections and noted since the cross-section shows the preliminary footing) □ Copy of any addendums or special provisions □ Half-size copy of the General Roadway Plans showing the structure locations □ Geotechnical Report and Boring Logs □ Half-size copy of the Sign Text Layout Plan from the contract plans	
		Save an electronic copy of the "Approved" stamped sign structure shop plans and foundation drawings. □ Save the scanned documents in the V:\ directory (V:\Bureaus\B54-Traffic\ENGINEERING&RESEARCH\OHSS\Plans (Structure & Footing). □ Create a sub-folder with the structure inventory number. □ Save the documents in the sub-folder. The scanned structure shop plans should be named with the year approved (i.e., structure 2012 pdf). The	

scanned footing plans should also be named with the year designed (i.e., footing 2012.pdf). Include the word "original if a new structure and/or footing.

- 8) Recording Sign Structure and Footing Details
 - The sign structure and footing details shall be entered into the Bureau of Bridge Design Database by the project engineer as described in the Sign Structure and Footing Design Guidelines (Appendix 10.3-A1).
 - If Bridge Design was not the lead Bureau of the sign structure project, the lead Bureau or design Consultant shall forward the plans and information as noted above (Archiving the Plans) to the Bureau of Bridge Design for archiving and recording.

10.3.6 Adding New Signs to an Existing Overhead Sign Structure

Existing sign structures and foundations that were constructed since 1975 have been designed to accommodate a total sign surface area 30% greater than the proposed sign area. If a sign(s) needs to be replaced or added to an existing overhead sign structure, the Bureau of Traffic shall coordinate the following:

- 1) The Traffic Engineer shall determine, from the existing project folder calculations and shop plans, the total sign surface area for which the structure and foundation were designed. If the Bureau of Traffic does not have a copy of the calculations and shop plans, the Traffic Engineer shall contact the Bureau of Bridge Design for a copy. Since the existing signs on the structure may not be the actual signs for which the structure was designed, the actual designed sign surface area needs to be confirmed by the design calculations and shop plans. The Bureau of Traffic has created a sign structure database to inventory each structure and its signs. Information regarding the total designed sign surface area for the structure will be added to the database for future reference.
- 2) For overhead sign structures where the centroid of each sign remains coincident with the mid-height of the horizontal truss, does not lower the vertical clearance and does not move laterally:
 - a) If the new total sign surface area is *less than* the total *designed* sign surface area (original sign surface area plus 30%), the Traffic Engineer can replace the existing sign with the new sign *without* any further analysis.
 - b) If the new total sign surface area is *greater than* the total *designed* sign surface area (original sign surface area plus 30%), the Traffic Engineer shall contact the Bureau of Bridge Design for analysis of the existing structure and foundation with the new loading.
- 3) For overhead sign structures where the centroid of an existing or new sign moves vertically from the mid-height of the horizontal truss and/or moves laterally to a different location on the horizontal, the Traffic Engineer shall contact the Bureau of Bridge Design for analysis of the existing structure and foundation with the new loading, *regardless* of whether the total sign area increases *or* decreases.
- 4) Any change of the sign(s) on the structure or the structure itself shall be updated in the Bridge Design Database.

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10.4 Bridge-Mounted Sign Supports

10.4.1 General

Bridge-mounted sign supports shall be designed, fabricated, and constructed in accordance with the current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims; NHDOT Standard Specifications for Road and Bridge Construction, Section 615 – Traffic Signs; the Bridge Design Manual, NHDOT Detail Plan and any special provisions.

A standard design for bridge mounted sign support is provided on the NHDOT Bridge Design Detail Sheets located at:

 $\underline{http://www.nh.gov/dot/org/projectdevelopment/bridgedesign/detailsheets/index.htm} \;.$

- The standard design shown on the detail sheet has been designed in accordance with the criteria noted on the plan (See Appendix 10.4-B1).
- If the proposed sign support meets the standard design criteria, the detail sheet title box shall be filled out and the sheet can be included in the contract plans.
- If the proposed sign and/or support exceeds any of the standard design criteria (support dimensions, sign dimensions, sign weight, skew angle), the sign support members and anchors will need to be *redesigned*, the girder (to which it is attached) evaluated for the load, *and* a new plan prepared to include in the contract plans. This work shall be performed by Bridge Design if the project is an In-House project or by the Consultant if the project is a Consultant project.

If the bridge has an existing road identification sign attached to the deck coping, use Item 615.35801, Reset Bridge Mounted Traffic Sign Type BB to re-attached the sign to the bridge. See Figure 10.4.2-2 for a typical road identification sign attached to a bridge.

10.4.2 Coordination

- 1) Once the contract is awarded, the Contractor shall submit shop drawings indicating the member sizes, lengths, and materials, to the Bureau of Bridge Design for approval, in accordance with Section 105.02 of the NHDOT Standard Specifications.
 - The Bureau of Bridge Design or the design Consultant shall review the Fabricator's shop plans for conformity with the contract plans, proposal, specifications, and NHDOT policy. The shop plans shall be stamped "Approved", "Approved Except as Noted" or "Disapproved", and returned to the Bureau of Construction for distribution to the Contractor and Fabricator.

2) Distribution of Plans:

- Distribute the following to the Bureau of Construction:
 - \Box Four (4) copies of the stamped shop plans.
- Distribute the following to the <u>Fabrication Engineer</u>, <u>Bureau of Bridge Design</u>:
 - ☐ One (1) copy of the "Approved" stamped shop plans with a transmittal letter noting the project name, number, sign support location and noting that the copy is to be distributed to the shop inspector.

• Email the <u>Bureau of Traffic Engineering Section</u>, noting that a copy of the "Approved" stamped shop plans were scanned and placed as noted below in "Archiving the Plans".

4) Archiving the Plans:

- If the bridge-mounted sign support is part of a bridge project:
 - ☐ File one (1) half-size copy of the "Approved" stamped shop plans along with any correspondence, in the bridge project folder and in the Sign Structures file cabinet located in the Bureau of Bridge Design.
 - □ Scan a copy of the "Approved" stamped shop plans. Place the scanned documents in the V:\Towns directory under the town in which the bridge is located, the bridge inspection maintenance folder, the bridge number, and shop drawings sub-folder (i.e. V:\Towns\Bow\BridgeInspMaint\136_160\Shop Drawings).

(i.e. V:\Towns\Bow\BridgeInspMaint\136_160\Shop Drawings). The scanned shop plans should be named with the year, description, and project number (i.e., 2012 bridge mounted sign supports_12567.pdf).

- If the bridge-mounted sign is not part of a bridge project:
 - ☐ File one (1) half-size copy of the "Approved" stamped shop plans, along with any correspondence, in a folder with the town name and bridge number in the beginning of the Sign Structures files cabinet located in the Bureau of Bridge Design.
 - ☐ Scan a copy of the "Approved" stamped shop plans. Save the scanned documents in the V:\Towns directory under the town in which the bridge is located, the bridge inspection maintenance folder, the bridge number, and shop drawings sub-folder

(i.e. V:\Towns\Bow\BridgeInspMaint\136_160\Shop Drawings). The scanned shop plans should be named with the year, description, and project number (i.e., 2012 bridge mounted sign supports_12567.pdf).



Typical NHDOT Bridge Mounted Sign Supports

Figure 10.4.2-1





Typical NHDOT Road Identification Sign

Figure 10.4.2-2

Non-	Bridge	Struc	ctures

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10.5 Traffic Signal Supports (Mast Arms)

10.5.1 General

The traffic signal supports (mast arms) and foundations shall be designed, fabricated, and constructed in accordance with the current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims; NHDOT Standard Specifications for Road and Bridge Construction Section 616 – Traffic Signals; and the NHDOT Standard Plans for Road Construction and any special provisions.

10.5.2 Design Process

- 1) The Bureau of Traffic will contact the Bureau of Materials and Research, Geotechnical Section as to whether the geotechnical capacity of the soils providing foundation support satisfies the design requirements of the standard foundation plans for the project site.
- 2) The contract plans will indicate mast arm dimensions and type required as directed by the Bureau of Traffic. The maximum mast arm length is 60-ft. (18.3-m).
- 3) The revised standard mast arm structure plan, TS-7, shows configurations of the traffic signal supports with combinations of signals, attachments, and luminaire. The corresponding revised foundation type that shall be used with each configuration is shown on the traffic standard plan TS-1, TS-2, TS-3, or TS-4. The plans are currently under review. Once approved, the Traffic Standard Plans will be included in the *NHDOT Standard Plans for Road Construction* and can be found at: http://www.nh.gov/dot/org/projectdevelopment/highwaydesign/standardplans/index.htm



Typical NHDOT Traffic Signal Support (Mast Arm)

Figure 10.5.2-1

Chapter 10		Non-Bridge Structures
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10.6 Intelligent Transportation Systems (ITS), Dynamic Message Sign (DMS), and Luminaire Support Structures

10.6.1 Intelligent Transportation Systems (ITS) Support Structures

Support structures and foundations for all intelligent transportation systems [Closed Circuit Television Cameras (CCTV), Road and Weather Information Station (RWIS) Systems, and Non-Invasive Pavement Sensor Systems] shall be designed, fabricated, and constructed in accordance with the current edition of *AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals*, including interims; and the current NHDOT Special Provisions, Section 677.xx – Intelligent Transportation Systems (ITS) Equipment.

A. Closed Circuit Television Cameras (CCTV)

The design of CCTV systems is a combined effort between the Transportation Management Center, the Bureau of Bridge Design, Bureau of Materials and Research, and the supplier of the structure. Bridge Design and Materials and Research are responsible for the preliminary and final design of the CCTV pole foundation for In-House projects. For Consultant projects, Consultants are responsible for the preliminary and final design of the foundation, with the guidance from Materials and Research and Bridge Design. The supplier of the pole is responsible for the design of the pole and submits shop drawings (through the Contractor) to the Department or the Consultant for approval. The supplier's calculations and shop plans (stamped by a NH PE) are reviewed for general conformance with the Contract Plans and NHDOT policies and specifications. See Figure 10.6.1-3 for a typical CCTV.

B. Road and Weather Information Station (RWIS)

The design of Road and Weather Information Station Systems is a combined effort between the Transportation Management Center, the Bureau of Bridge Design, and the supplier of the structure and foundation. The supplier of the pole is responsible for the design of the pole and foundation and submits shop drawings and calculations to the Department for approval. Bridge Design is responsible for reviewing the pole and foundation shop plans and calculations (stamped by a NH PE) for general conformity, for In-House projects. For Consultant projects, the design Consultant is responsible for reviewing the pole and foundation shop plans and calculations (stamped by a NH PE) for general conformity. See Figure 10.6.1-1 for a typical RWIS.

C. Non-Invasive Pavement Sensor Systems

The design of Non-Invasive Pavement Sensor Systems is a combined effort between the Transportation Management Center, the Bureau of Bridge Design, and the supplier of the structure and foundation. The supplier of the pole is responsible for the design of the pole and foundation and submits shop drawings and calculations to the Department for approval. Bridge Design is responsible for reviewing the pole and foundation shop plans and calculations (stamped by a NH PE) for general conformity, for In-House projects. For Consultant projects, the design Consultant is responsible for reviewing the pole and foundation shop plans and calculations (stamped by a NH PE) for general conformity. See Figure 10.6.1-2 for a typical Non-Invasive Pavement Sensor.

D. Coordination of CCTV Support Pole and Foundation

1) Once the contract is awarded, the Contractor shall submit shop drawings of the CCTV support pole(s), design calculations, and top of foundation reactions for each pole location to the Bureau of Bridge Design for approval in accordance with Section 105.02 of the *NHDOT*

Standard Specifications and the special provision. The Contractor shall also indicate which foundation he will be installing: spread footing or drilled shaft foundation.

- ⇒ The Bureau of Bridge Design or the design Consultant will use the top of foundation reactions from the fabricator to verify or modify the preliminary foundation design that was included in the contract, for a final design.
- ⇒ The Bureau of Bridge Design or the design Consultant shall review the Fabricator's shop plans for conformity with the contract plans, proposal, specifications, and NHDOT policy. The shop plans shall be stamped "Approved", "Approved Except as Noted" or "Disapproved", and returned to the Bureau of Construction for distribution to the Contractor and Fabricator.

Distribution of Plans

\Rightarrow	Distrib	ute the following to the <u>Bureau of Construction</u> :
		Four (4) copies of "Approved" stamped structure shop plans
		Four (4) copies of the foundation plan stamped "Final Design".
\Rightarrow		one (1) copy of the "Approved" stamped structure shop plans with a transmittal noting the project name, number, fabricator, location, and noting that the copy is to be distributed to the shop inspector.
\Rightarrow		one (1) copy of "Approved" stamped structure shop plans One (1) copy of "Approved" stamped foundation shop plans stamped "Final Design"

3) Archiving the Plans:

- ⇒ Archive the foundation support structure plans in the Bureau of Bridge Design:
 - ☐ A folder labeled with the project name and number containing one (1) half-size copy of the "Approved" stamped shop plans, foundation plans, and any correspondence and shall be placed in the project folder (if applicable). A copy should also be filed in the ITS file cabinet located in the Bureau of Bridge Design.



Typical NHDOT RWIS

Figure 10.6.1-1



Typical NHDOT Non-Invasive Pavement Sensor System

Figure 10.6.1-2



Typical NHDOT CCTV

Figure 10.6.1-3

10.6.2 Dynamic Message Sign (DMS) Overhead Structures

All dynamic message sign (DMS) overhead structures and foundations shall be designed, fabricated, and constructed in accordance with the current edition of *AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals*, including interims, *NHDOT Bridge Design Manual Chapter 10*, and the current NHDOT Special Provisions, Section 677.xx – Permanent Fixed Location Dynamic Message Sign System.

The design of DMS overhead structures is a combined effort between the Transportation Management Center, the Bureau of Bridge Design, and the Manufacturer of the structure. Bridge Design is responsible for the preliminary and final design of the foundations for In-House projects. Consultants are responsible for the preliminary and final design of the foundations, with the guidance of Bridge Design and Materials and Research, for Consultant projects. The Manufacturer of the structure is responsible for the design of the structure and shall submit shop drawings to the Department (through the Contractor) for approval. The Manufacturer's calculations and shop plans are reviewed for general conformity with Contract Plans and NHDOT policies and specifications.

The design process and coordination shall be as noted in Chapter 10, Section 10.3.5. The Department will furnish the foundation design plans for the DMS overhead structure to the Contractor after approval of the overhead structure shop drawings.



Typical NHDOT DMS Overhead Structure

Figure 10.6.2-1

10.6.3 Luminaire Support Structures

A. Light Poles with Mast Arm

The typical light poles with mast arm and foundation (light pole bases) shall be designed, fabricated, and constructed in accordance with the current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims; the current NHDOT Standard Specifications for Road and Bridge Construction, Section 625, Light Pole Bases; and any special provision.

Standard foundation designs for typical light pole bases are provided in the *NHDOT Standard Plans for Road Construction*, SL-2, Concrete Foundations and Light Pole Base Type B located at: http://www.nh.gov/dot/org/projectdevelopment/highwaydesign/standardplans/index.htm.

B. High-mast Light Poles

High-mast light poles (towers) shall be designed, fabricated, and constructed in accordance with the current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims; and the current NHDOT Standard Specifications for Road and Bridge Construction and any special provisions.





Typical NHDOT Light Pole with Mast Arm

Figure 10.6.3-1

Typical NHDOT High-mast Light Poles

Figure 10.6.3-2

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10.7 Soundwalls

10.7.1 General

Soundwalls shall be designed, fabricated, and constructed according to the current AASHTO LRFD Bridge Design Specifications Section 15, Design of Sound Barriers; NHDOT Bridge Design Manual, and NHDOT Special Provision Section 594 – Sound Abatement Wall. See Figures 10.7.2-1, 2 & 3 for NHDOT soundwalls.

10.7.2 Types

A. Wood Panel Soundwall Detail Sheets

A standard design for wood panel soundwalls is provided on the NHDOT Bridge Detail Sheets located at: http://www.nh.gov/dot/org/projectdevelopment/bridgedesign/detailsheets/index.htm.

- The wood panel soundwall and foundation detail sheets provide a design for the soundwall system utilizing wood panels, precast concrete posts, and drilled shaft foundations for wall heights up to **25-ft**. (7.6 m) meeting the design criteria noted on the Bridge Detail Sheets (see Appendix 10.7-B1 for a sample plan of the Soundwall Detail Sheets).
- If any part of the proposed soundwall does not meet these design criteria, the soundwall will need to be designed by the Bureau of Bridge Design or the design Consultant.
- Borings shall be requested by the lead Bureau.
- The designer (Bureau of Highway Design or Consultant) shall develop an alignment and elevation plan for the soundwall.
- The designer shall provide the Bureau of Materials and Research Geotechnical Section with design loads at the top of each drilled shaft.
 - The soundwall <u>foundation</u> will be designed with the criteria specific to the project (i.e., exposure height, wind pressure), independent of the soundwall design. This allows more efficiency for the design of the drilled shaft.
 - ➤ The designer shall work with the geotechnical engineer in determining what design criteria shall be used for calculating design loads at the top of the foundation.
 - The Geotechnical Section will determine the drilled shaft lengths required and provide them to the designer to place on the plans.
 - ➤ The designer shall create a plan with a soundwall location chart that includes the following:

Post/shaft number
Coordinates of post foundation
Finished grade elevation
Minimum top of wall elevation
Wall height

B. Soundwall located on a MSE Wall

• If a soundwall is located over a MSE wall or some other obstruction where the drilled shaft foundation is not feasible, a concrete moment slab or spread footing shall be utilized.

- The concrete moment slab or spread footing and anchorage system, shall be designed by Bridge Design or the design Consultant with the criteria specific to the project (e.g., exposure height, wind pressure), independent of the soundwall design.
- The designer shall provide the Bureau of Materials and Research Geotechnical Section, with the proposed moment slab or spread footing design and associated bearing pressures.
 - ➤ The Geotechnical Section will check whether there is sufficient bearing resistance for the design.
 - ➤ If necessary, the designer shall work with the geotechnical engineer in redesigns until the bearing resistance is obtained.
- If the moment slab or spread footing is transferred to an underlying structure, the structural designer shall check the underlying structure's capacity to support any loading applied.
- If a vehicular collision (e.g., box truck tipping) to the soundwall would cause safety concerns regarding debris to the area below the MSE wall, the face of the soundwall wood panel shall be located greater than 4-ft. behind the face of the traffic barrier in accordance with AASHTO LRFD 15.8.4, unless the soundwall is designed for the vehicular collision load as noted in AASHTO LRFD 15.8.4. The barrier used in front of the soundwall shall meet a crash testing level of TL-4 in accordance with AASHTO Section 13.

Design loads, materials and specification notes
Foundation design notes
Coordinates of post foundation
Plan and elevation sheets
Moment slab or spread footing masonry and reinforcing details
Anchorage system
Soundwall post and moment slab/spread footing locations and elevations
Summary of quantities

The designer shall create contract plans which include the following:

C. Soundwall on a Bridge

□ Wall heights

- The soundwall detail sheet shall <u>not</u> be used for soundwalls located on a bridge. <u>All</u> soundwall components, including the anchor assembly, shall be designed by the Bureau of Bridge Design or the design Consultant for the project specific criteria (i.e., exposure height, wind pressure).
- The designer shall create contract plans that include information as noted in Section B above.
- The concrete bridge deck overhang shall be designed for the soundwall loading in accordance with AASHTO LRFD Bridge Design Specifications.
- The face of the soundwall wood panel shall be located greater than 4-ft. behind the face of the bridge steel traffic barrier in accordance with AASHTO 15.8.4, for roadway crossings or if a vehicular collision (e.g., box truck tipping) to the soundwall would cause safety concerns regarding debris to the area below the bridge. The bridge barrier shall be T3 steel bridge railing to meet the height requirements for a crash testing level of TL-4. (AASHTO Section 13).

D. Soundwall Sample Plans

• For soundwall examples, see NHDOT Sample Plans located at: http://www.nh.gov/dot/org/projectdevelopment/bridgedesign/sampleplans/index.htm.





NHDOT Soundwall on a Precast Leveling Panel

Figure 10.7.2-1

NHDOT Soundwall on a Moment Slab

Figure 10.7.2-2



NHDOT Soundwall on a Bridge

Figure 10.7.2-3

Non-Bridge	Structures

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Chapter 10

10.8 Inspection and Maintenance

10.8.1 Inspection

The Bureau of Traffic will be implementing an inspection program that will include visual inspections of the structure, and UT testing of the anchor rods for all auxiliary structures such as the following:

- Overhead sign and DMS structures
- Traffic signal supports (mast arms)

10.8.2 Maintenance

A. Overhead Sign Structures

The Bureau of Traffic maintains and inspects overhead sign and DMS structures. The Bureau of Traffic maintains a database that inventories each sign structure and the signs located on the structure.

B. Bridge-mounted Sign Supports

The Bureau of Bridge Design Bridge Inspectors inspect the bridge-mounted sign supports at the time the bridge is inspected. The condition of the bridge-mounted sign supports is noted on the last page of the bridge inspection report. If there is concern with the supports or signs, a copy of the inspection report is sent to the Bureau of Traffic for their review. The Bureau of Traffic maintains a database that inventories the bridge-mounted sign supports and the signs located on the sign structure.

C. Typical Light Poles and High-mast Light Poles

The Bureau of Turnpikes and the Bureau of Highway Maintenance maintain light poles and highmast light poles along the Turnpike, Interstate, Interstate ramps, and NH and US numbered routes, *within* the PSNH servicing area. Light poles and high-mast poles outside the PSNH servicing area are maintained by the servicing company that owns it. The Bureau of Highway Maintenance maintains an inventory of all light poles and high-mast light poles along the Turnpike, Interstate, Interstate ramps, and NH and US numbered routes.

D. ITS Camera Poles

The Bureau of Turnpikes and the Bureau of Highway Maintenance maintain ITS camera poles along the Turnpike, Interstate, Interstate ramps, and NH and US numbered routes. The Transportation Management Center (TMC) maintains the cameras and ITS equipment.

E. Traffic Signal Supports (Mast Arms)

The Bureau of Traffic maintains traffic signal mast arms along the Interstate ramps, and NH and US numbered routes.

Chapter 10		Non-Bridge Structures
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References

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- 2. American Association of State Highway and Transportation Officials (AASHTO), *Standard Specifications for Highway Bridges*, 17th Ed., 2002, Washington, D.C.
- 3. American Association of State Highway and Transportation Officials (AASHTO), Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, 6th Ed., 2013, Washington, D.C.
- 4. Federal Highway Administration (FHWA), FHWA Guidelines for the Installation, Inspection, Maintenance and Repair of Structural Supports for Highway Signs, Luminaires, and Traffic Signals, Publication No. FHWA NHI05-036, March 2005, Washington, D.C. Retrieved from http://www.fhwa.dot.gov/bridge/signinspection03.cfm#fig34
- 5. Johannessen & Leone Associates, WIND Speed by Zip Retrieved from http://www.windspeedbyzip.com/
- 6. New Hampshire Department of Transportation Bureau of Bridge Design, *Bridge Design Manual, October1*, 2000, Concord, NH
- 7. New Hampshire Department of Transportation Bureau of Highway Design, *Highway Design Manual*, 2007, Vol. 1, Concord, NH
- 8. New Hampshire Department of Transportation, NHDOT Standard Specifications for Road and Bridge Construction 2010, Concord, NH
- 9. Weather Underground, Inc., Weather Underground Map

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Non-Bridge Structure	s
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Bridge Design Manual

Chapter 10 – Appendix A

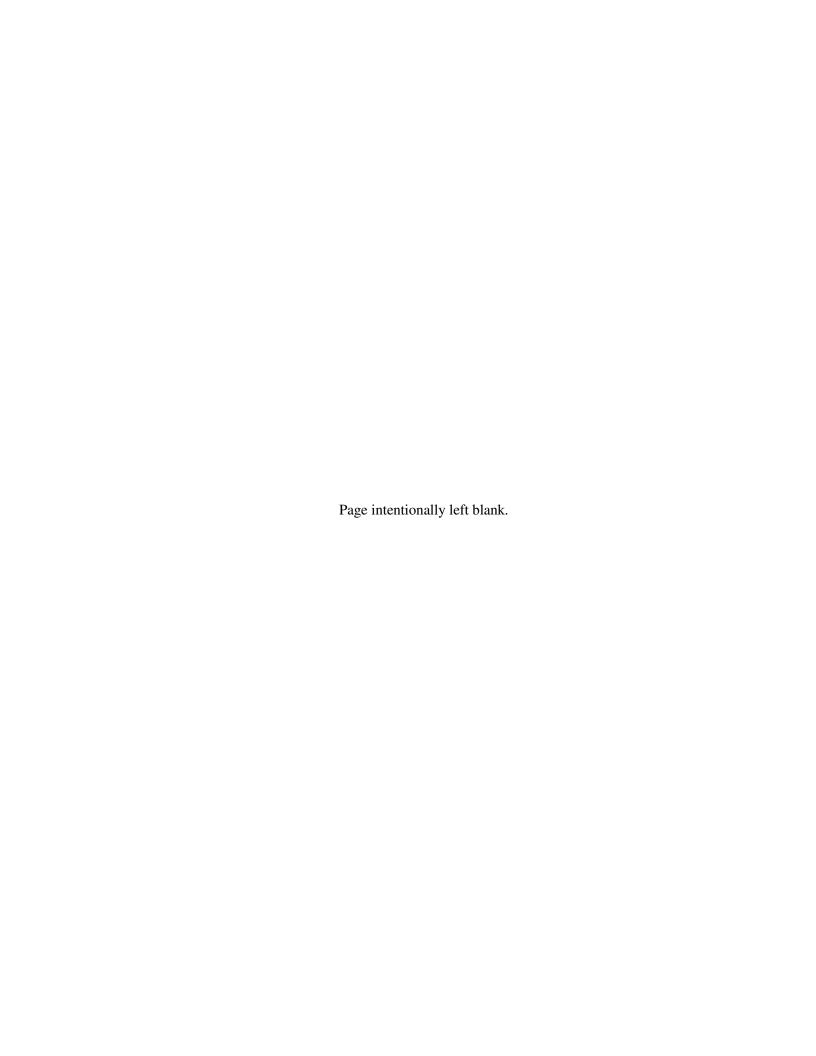
January 2015 - v 2.0

(Revised Feb. 2016)



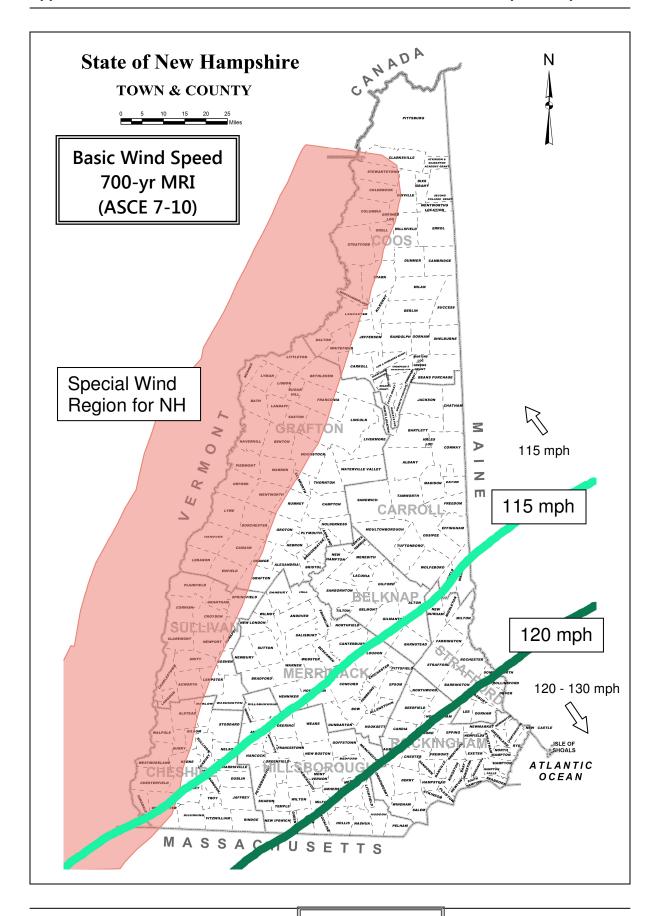






Basic Wind Speed Map for NH and Special Wind Region

- The map on the following page shows the 3-second gust basic wind speed and the Special Wind Region derived from AASHTO LRFD Figure 3.8.1.1.2-1 (ASCE 7-10, MRI 700-yrs.
- The MRI 700-yrs map shall be used for design of bridges, traffic signal mast arms, and soundwalls.
- The basic wind speed for the design of sign structures and CCTV pole supports shall be 100-mph (160-km.hr) as noted in Chapter 10, Section 10.2.
- For the Special Wind Region (i.e. regions along the NH-VT border and Franconia Notch) as shown in AASHTO LRFD Figure 3.8.1.1.2-1, the maximum-recorded wind speed in this area shall be used if it is greater than 115-mph (185-kph), else use 115-mph (185-kph). See Chapter 4, Section 4.3.11 Wind Loads, for additional information.
- For wind speeds in the Special Wind Region, weather station data can be accessed by clicking on the markers (weather stations) on the weather underground map located at: http://www.wunderground.com/wundermap/?lat=43.63526535&lon=-72.25418091&zoom=8&pin=Lebanon%2c%20NH



SIGN STRUCTURE & FOOTING DESIGN GUIDELINES

The Sign Structure and Footing Design Guidelines is a working document for use as a guide for reviewing sign structure shop plans, designing the foundation, and drawing the sign structure foundation plan. This guideline is intended to promote consistency and continuity of sign structure and foundation designs, and project coordination.

Overhead sign structures and foundations shall be designed or analyzed in accordance with the following, as appropriate:

- Current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims
- NHDOT Standard Specifications for Road and Bridge Construction
- NHDOT Bridge Design Manual
- Special Provision, Amendment to Section 615 Traffic Signs
- Special Provision Item 677.xx Permanent Fixed Location Dynamic Message Sign

A. Sign Structure Shop Drawings Check List □ Overhead signs shall provide a vertical clearance of not less than 17'-6" [5.3 m] (18'-0" [6.3 m] preferred by Bureau of Traffic) over the entire width of the pavement and shoulders. ☐ Check for any changes made after proposal (i.e., addendums). ☐ Check that signs are correctly oriented with respect to stationing (i.e., back of sign). ☐ Compare dimensions for signs and structure (post and truss lengths, sign dimensions, and offsets) with stick drawings, cross-sections, Prosecution of Work, addendums, and special provisions. ☐ Anchor rod size and layout shall be identical for both left and right footings, otherwise disapprove. ☐ Check that the anchor rods are galvanized, include hardened washers, not lock washers, and two nuts (one above and one below base plate) per rod, are shown for the double-nut moment connection to the sign structure. ☐ Check for a licensed N.H. P.E. stamp. \Box Check that the top of concrete stem elevation is 3-in. (75 mm) \pm higher than adjacent highest finished grade. □ 25 percent of the base plate-to-post weld shall be inspected by magnetic particle testing per AASHTO specification. This requirement shall be noted on the shop plans. ☐ Triangular truss type overhead sign structures shall not be allowed due to concerns with their susceptibility to fatigue cracking. ☐ Tubular arch type structures are not allowed due to concerns with their susceptibility to fatigue cracking. □ Sign support members (W6x9's) shall not be greater in length than the sign height. ☐ Check that the upright face closest to traffic of the sign structure support is a minimum of 10-ft. (3 m) behind the guardrail or is outside the clear zone, otherwise approval is required from Bureau of Traffic.

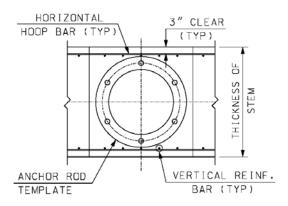
		The distance from the top of the concrete stem to the bottom of the sign structure base plate shall be the nut height plus 1-inch [25 mm] (preferred) or nut height plus the anchor rod diameter (maximum). If the shop plans are noted differently, cross-out the shop plan note and add in this note. See "Anchor Rod Detail" on Sign Footing Sample Plan.
		The connection of the structure to the foundation shall be a double-nut joint moment connection.
		The maximum overhead cantilever sign structure span is 50-ft. (15.2 m) Any exception to this shall be approved by the Design Chief of the Bureau of Bridge Design
		Anchor rods shall conform to the requirements of ASTM F1554 Grade 55 (minimum). ASTM A615 reinforcing steel is not permitted. Galvanize the entire rod per ASTM A153. Each anchor rod shall be supplied with a minimum of two hex nuts (ASTM A563 or ASTM A194) and a minimum of two flat hardened washers (ASTM F436).
		Each monotube upright post shall have a minimum of eight (8) foundation anchor rods. Each post of a multi post upright (truss) shall have a minimum of four (4) foundation anchor rods per post.
B.	Check	Input, Loads, and Reactions from Fabricator's Sign Structure Program
	incorre	have been many instances where computer programs have provided incorrect output and ct reactions (e.g. The values for the wind on the sign were 30% low, even though the ras correct.).
		Check for a licensed N.H. P.E. stamp.
		Check that the design was per the current edition of AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals, including interims
		Check that the Design Sign Area = 1.3 x Actual Sign Area
		Check input values and spot check output values. (See NHDOT Bridge Design Manual, Chapter 10, Section 10.2 Loads)
		Check that sign structures designed for Cantilevered Fatigue Category I, have the anchor rods designed for wind-induced cyclic loads per AASHTO Specifications Section 5.17.3.4.
C.	Check	Constructability of Footing.
		Check that the sign structure and foundation are located to avoid any interference with utilities, drainage pipes, or structures.

D. Review Geotechnical Report.

- ☐ Check allowable bearing pressure
- ☐ Check frost depth:
 - ⇒ The bottom of the foundation shall be placed a minimum of 5'-0" (1.5 m) below the lowest finished grade measured normal to the ground surface for frost cover.
- ☐ Check with the Design Chief to confirm the necessity of structural fill below the footing.
- ☐ Check to determine if rock anchors or any other foundation requirements are specified.

E. Footing Design Check List

- ☐ There are In-House Design programs for the foundation design located at: S:/Design/Programs/Sign
- \square Minimum thickness of stem = anchor rod template outside diameter + 2*(dia. vertical bar + dia. horizontal hoop bar + 3" [75 mm] clear)



- \square Length of stem base at top of footing = footing length 1 ft. (300 mm)
- \square Length of stem at top of pedestal = post spacing + stem thickness
- ☐ If left and right footing are similar, use *identical* footings.
- ☐ Design method: ASD (Allowable Stress Design) per AASHTO Standard Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals
- ☐ Grout shall <u>not</u> be used between the bottom of the structure base plate and the top of the footing.
- ☐ Cantilever sign structure with more than one (1) sign:

$$L_{\text{sign}} = \sum (A_{\text{sign}} \times L_{\text{sign}}) \div \sum A_{\text{sign}}$$

- \square Sign Bridge sign structure: If using Sign.Exe program, the input load $DL_{truss+signs}$ and $IL_{truss+signs}$ = reaction of one leg due to the DL or IL of total signs and truss. The designer needs to run two programs, one for each leg, if signs are not the same size and/or are not symmetrical.
- \Box Check bearing pressure: $Q_{max} < Q_{allow}$

If $Q_{\text{min}} < 0$ (negative soil pressure, footing uplift) use AASHTO Fig. 4.4.7.1.1.1C to calculate uplift.
NHDOT policy for maximum allowed footing area with uplift is the following: ⇒ Sign bridge structure = 5 % of footing area. ⇒ Cantilevered sign structure = 1 % of footing area.
If the area of footing having uplift is $> 5\%$ for sign bridge structure, or $> 1\%$ for cantilevered sign structure, <i>increase</i> footing size.
Design the footing reinforcing for loading in both the transverse and longitudinal direction. ⇒ Use the <i>same</i> size reinforcing bar for both directions, for ease of construction.
Check the development length for stem reinforcement at the footing interface both into the stem and into the footing.
Check that the overlap length of the vertical reinforcing bar and anchor rod is equivalent to a class c splice length of the reinforcing bar.
If sign structure is a cantilever structure, the stem design should be checked for torsion.
Check the area of reinforcing required for stem sections at the bottom , top , middle , and a distance down from the top of the stem , for both the transverse and longitudinal directions. (In some designs, the slope of the stem causes the bars to drop out of the section quickly, creating less area of steel at certain heights of the stem.) Make sure the stem design has adequate amount of reinf. required at all sections of the stem height.
If the footing is founded on bedrock and if rock anchor rods are required: ⇒ Check soils report for bearing capacity of bedrock ⇒ Check the pullout capacity of the ledge. Per AASHTO Table 5.7.6.2B, granite = 50 k/ft.(74.4 Tn/m), FS = 3 for anchors in rock. (If anchor is drilled four feet into granite, then the granite can resist 4 ft. x 50 k/ft. /3 = 66.6 k force.) ⇒ Check capacity of anchor = 0.55(F _y)(A _{bar}). ⇒ Rock anchors should be grade 60 ksi reinforcing steel. ⇒ Anchor should be set in drilled holes = ½" (12 mm) + Dia. bar. ⇒ Hole should be filled with an approved high-strength non-shrink grout, minimum 2 ft. (600 mm) deep.

F. Drafting Footing Plan Using CADD Macro: Sign Footing

- Enter MicroStation
- ➤ On the File Open splash screen, make sure the project is listed as "BRIDGE MISC ENGLISH" in the Workspace box.
 - ⇒ Open N:\CADD\Misc Accounts\BRD\Sign Footings
- Create a sub-folder with the project name and number
- ➤ Create a .dgn using the item number of the structure (e.g., 615_10001.dgn). If a sign bridge structure, add the designation of "LT" or "RT" to distinguish the file name (e.g., 615_10001_LT.dgn)
- Click on the "File" tab at the top of the File Open splash screen and click "New".
- > Double click on the .dgn to open the drawing
- > Open Level Manager, attach Library: BRC.csv, close out Level Manager
 - ⇒ This needs to be done every time a .dgn is created for the macro to run.
 - ⇒ N:\CADD\CADD\v8i_Workspace\Standards\dgnlib
- > Click on NHDOT (top menus), Sign Footing
- Macro input menu opens. Input values as applicable on the "Footing", "Rods", "Reinforcing Bars" and "Pay Limit Details" tabs.
- > Click on "Do It" once all input is complete.
- > Click on full screen view when macro is done.

	Chek on run sereen view when macro is done.
Edi	iting of the drawing may be required for job specific items.
	File number for new sign footing plans: 122-x-x (old files are 115-3 [2013 -11], 105-2 [2010 -2007], 77-5 [2006 -1999], 45-4 [1998 – prior]) Log file number in sign footing plan file document S:\Bridge-Design\FORMS\PROJECT\Sign Footing Plan File.xls
	Give a detailed description of the footing location (e.g., 250-ft. north from Exit 12, I-93 SB), not just a construction station location. Obtain this description from the Bureau of Traffic.
	Indicate on the plans near the title box, the Traffic Inventory Number for the structure. Call Bureau of Traffic to obtain the inventory number they have assigned to the structure.
	Check Item numbers and descriptions and check that they match the contract plans.
	Indicate the footing design bearing pressure in the Sign Footing Notes on the plan.
	Indicate the design sign area for each footing (including 30% increase) in the Sign Footing Notes on the plan.
	If bedrock exists, the macro does not draw the bedrock location. Its approximate location will need to be drawn manually and the rock excavation item number added to the quantity box and excavation quantities adjusted.
	Other minor editing may be required.
	The macro draws an anchor rod detail and a stainless steel wire cloth detail. A note is added stating, "For the installation and pretensioning of anchor rods, see Special Provision, Amendment to Section 615 – Traffic Signs.
	Check that all items shown on the sign footing plan are included in the proposal contract estimate, otherwise the item number on the plan needs to change to match the

contract estimate.

G. Pay Items and Limits

- ☐ Item 206.1, Common Structure Excavation
 - ⇒ Vertical pay limits shall extend from the bottom of footing (or structural fill) to the existing or proposed ground. If the existing ground is above the proposed ground line, excavation from existing ground to proposed ground is paid for under common excavation. Any additional excavation for the footing is paid for under common structure excavation (see Standard Specifications Section 203). No excavation payment shall be made if the sign footing is entirely above existing ground.
 - ⇒ Horizontal pay limits extend one foot (300 mm) beyond the footing limits on all sides unless founded on more than one foot (300 mm) of structural fill, or if cofferdams are used (see Appendix 10.3-B1).
- ☐ Item 206.1, Common Structure Excavation is measured to the nearest 1 CY
- ☐ Item 508, Structural Fill is measured to the nearest 1 CY
- ☐ Item 520.2, Concrete Class B is measured to the nearest 0.1 CY
- ☐ Item 544.1, Reinforcing Steel (Roadway) is measured to the nearest 1 LB
- □ No item is needed for fill since the same material excavated will usually be replaced. If ledge is excavated to construct the footing, check the contract estimate for a good draining replacement material such as Item 209.1, Granular Backfill. Quantify this item and include it in the quantity box on the footing plans.
- ☐ For DMS overhead sign structure and foundation, all items are subsidiary.

H. Inputting Sign Structure and Footing Data into the Database

- ➤ Go to "Add/Change Projects, Bridges or Signs" button.
- > Enter the project number
- ➤ If the project is past the advertising date, click on the "Unlock Project" button to enter information in the window.
- ➤ Click on the "Sign Footing" tab and enter in the year built, town, and inventory number for each sign structure.
- Close out window
- > Click on the "Misc Menu" tab on the main menu
- > Click on the "Sign Footing" tab
- > Click on the "Edit" tab and enter the sign footing information for each sign structure

I. Design Process and Coordination

See NHDOT Bridge Manual, Chapter 10, Section 10.3.5, Design Process and Coordination for the following:

- Design process and coordination of sign structures and foundations between bureaus and consultants
- Distribution of Plans
- Archiving Plans and Calculations

SIGN STRUCTURE & FOOTING REFERENCE TABLES

Appendix 10.3-A2 provides tables of data for bridge and cantilever sign structures and their foundation that have been designed and constructed. This information is for **reference only** and can be used for preliminary estimates for footing dimensions and quantities.

/111.	nina	пу	е: П	Su	П	iai	T	s 1	T	T	о Г	ou N	nş T	3 (T	T	Т	T	T	OI	1S		nc	1 q	Įu: T	an T	u T	Т	s. 		Т	Т	Т	Γ	П	Т	Т	Γ		П	Т		Т	Т	Α	Α	> 3	A
	Designer/ Checker							l		L						1		L							L	ļ							L	Ц	L						L	1		ABH/AE	ABH/AE	ABH/AEW	ABH/AB
	Anchor Bolts per post			4-1.75" Ø, 20" circle	4-1.75" Ø, 20" circle	4-1.75" Ø, 18 Circle	4-1.5" Ø 18" circle	4-1.5" Ø. 18" circle	4-1.25" Ø, 14" circle	4-1.25" Ø, 14" circle	4-1.25" Ø, 16" circle	4-1.25" Ø, 16" circle		8-1.25" Ø, 22" circle	8-1.25 Ø, 22 GIGIE	8-1.25 Ø, 22 circle	2000	4-1.75" Ø, 24" circle	4-1.75" Ø, 24" circle		4-1.75" Ø, 24" circle	4-1.75" Ø, 24" circle	4-1.5" Ø, 24" circle	4-1.5 'Ø, 24 CIrcle	4-1 5" Ø 29" circle	4-1 5" Ø 22" circle	4-1.25" Ø, 16" circle	4-1.25" Ø, 16" circle	4-1.25" Ø, 20" circle	4-1.25" Ø, 20" circle	4-1.25" Ø, 14" circle 4-1.25" Ø 14" circle	6 6 6	4-1.25" Ø, 20" circle	4-1.25" Ø, 20" circle	4 1 26" Ø 10 5"	4-1.25" Ø. 10.5" square	4-1.25" Ø, 10.5" square	4-1.25" Ø, 10.5" square	4-1.25" Ø, 10.5" square	4-1.25" Ø, 10.5" square	A 4 75" Ø 44" compa	4-1.75" Ø, 14" square	the square	4-2" Ø, 18" square	4-2" Ø, 18" square	4-2.25" Ø, 18" square	4-2.25" Ø, 18" square
	Rebar Quantity	(sql)		5334	5334	4911	5194	5194	3320	3320	3413	3413		5223	5223	2002		18222	18222		11823	11823	12227	12221	6404	6404	3543	3543	2897	5897	2418	0 1	0889	6830	1000	2631	2509	2509	2509	5209	2075	7075	200	8498	8498	5534	6363
	Structural Fill Quantity	(CY)																																													
	Concrete Quantity	(CY)		50.9	50.9	2.14	38.4	38.4	36.8	36.8	30.3	30.3		63.3	5.50	51.0	i	87	87		79.7	79.7	73.3	/3.3	65.8	65.8	39.5	39.5	58.9	58.9	30.74	100	9.59	9:29	1 20	35.1	33.5	33.5	33.5	33.5	67.0	67.9	9	72.1	72.1	39	44.8
	Excavation Quantity	(CV)																550	550																120	170	240	240	190	190						200	502
	Footing Thick-	(tt)		0 0	4	v 0	٥ د	1 0	2 2	2	2	2		2 0	y c	v 0		2	2		2	2	2 6	7	٥	٥	2 2	2	2	0 0	α α	1	2	2	ç	2 2	2	2	2	2	c	Ν 0	4	2	2	4	7
	ax Footing Height	(#)		9.05	9.05	= =	_ α	0	9	10	7	7		9	٥	n 0	,	H	10	ł	8.5	_	o (4	o	σ	, ω	8	6	o (o o	,	8.5	8.5	0	+	8	8	ω	80	c	n σ	-	10	10	+	4
	Omin/Omax	(kst)																0.14/2.64	0.14/2.64				-0.32/2.6	-0.32/2.6											0.04/0.40	-0.04/2.18	0.1/1.77	0.1/1.77								-0.57/3.39	-0.42/3.21
	ка ка	(ft) (ft)		1	1	1	Ŧ	ļ	F	F			Ī	1	1	Ŧ			0.66 3.27				0.7 3.43	0.7 3.43	F	Ŧ	L			1	1	1	E	H	0 40			0.36 1.86		4	ļ	Ŧ]	E		0.84 4.19	37 4.32
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	Arm			3.5' × 3.5' T	3.5' × 3.5' I	3.5 × 3.5 T	35' × 35' T	35' x 3.5' T	3.5' x 3.5' T		4'×4' T	- 4× 4	+ × 4 -		5' × 5' T	5' x 5' T		5' x 5' T	5' x 5' T	5.5' × 4.5' T	5.5 × 4.5 I	5' x 5 5' T	F x 5 5' T	4'×5'T	4' × 5' T	4.5' x 5.5' T	4.5' × 5.5' T	4'×4.5'T	- 0.1	5' x 4.5' T	5' x 4.5' T	F 13 0 × 13 0	3.5' × 3.5' T	3.5' x 3.5' T	3.5' x 3.5' T	3.5' x 3.5' T	3.5' × 3.5' T	T 30 00 1	3.25 x 3.25 l	0.50 ^ 0.50	4.75' x 4.75' T	4.75' x 4.75' T	5.25' × 5.5' T	5.25 X 5.5° I			
	Height	(#)		22	23.75	28.25	21.5	24.6	22.81	24.9	52	25.5	İ	26.6	1.62	24.4		10.75	32.75		28.5	59	53	R	25.36	26.56	24.01	29.25	24.31	29.1	21.03	20:02	26.5	25.75	N 13319	36.5	26.25	24	24.75	23.75	3 00	32.25	05:20	п		25.5	S
	Design Sign Area	(# ₂)																																	. HAMPTC							I		2064	2064	2640	2640
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	Description		NASHUA 10624F	615.10011 L	615.10011 K	615.10012 L	615 10013	615.10013 B	615.10014 L	615.10014 R	615.10015 L	615.10015 R 2000 79	STRATHAM-E)	615.10002 L	615.10002 H	615.10003 L	CONCORD 13572	615.10001 L	615.10001 R	MANCHESTER	615.10001 L	615.10001 R 2002	615.10002 L	MANICHESTER 40440B	615 10001 I	615 10001 B	615.10002 L	615.10002 R	615.10003 L	615.10003 R	615.10004 L	NASHUA - HUDSON 10624S	615.10001 L	615.10001 R	SEABHOOK - HAMPTON FALLS - HAMPTON - NO. HAMPT	615.10001 R	615.10002 L	615.10002 R	615.10003 L 2002 69 STEEL	615.10003 R	SEABFOOK TO	615.10001 L 2002	BEDFORD - HOOKSETT	615.10001 L	615.10001 R	615.10002 L	615.1000Z H

Controller Con	Description AANCHESTER				ror Reference Omy:				ה ה	<u> </u>	ıage	5	sign Bridge Footing Data	IIa							
1. 1. 1. 1. 1. 1. 1. 1.	AANCHESTER.	YR. Spa SUILT (ft)	-				Arm	Leg			\vdash	\vdash	Qmin/Qmax (ksf)		Footing Thick- ness (ft)	xcavation Quantity (CY)	Concrete Quantity F (CY)	Structural Fill Quantity (CY)	Rebar Quantity (Ibs)	Anchor Bolts per post	Designer/ Checker
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1856 23.5 C + C + C + C C + C + C + C + C + C	-	-	6 STEE	L	1520	27.75	4.5° × 4.5° ⊤	18" Ø x 0.313"	L	H	-			6.5	2		80		16157	4-1.5" Ø, 24" circle	
1866 27 6 6 4 5 1 1 1 1 20 0 0 1 20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-	-	6 STEE		1520	28.25	4.5' x 4.5' T	18" Ø x 0.313"	Ļ	18	24			6.5	2		80		16157	4-1.5" Ø, 24" circle	
1868 20.75 6.26.5 ct 1.0 ct 6.2.5 ct 2. 5 ct		2004 140.5	SB STEE	L	1856	_	6' x 5' T	20" Ø x 0.375"	2	16	30	L		8.5	2	Ī	101		15493	4-1.75" Ø, 26" circle	
145 145		2004 140.5	SB STEE	L	1856	_	6' x 5' T	18" Ø x 0.375"	L	H	30	L		8.5	2		101		15493	4-1.75" Ø, 26" circle	
348 45 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 68 88 68 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88 88		2004 223.	5 STEE		3152	_	6.25' x 5' T	24" Ø x 0.375"	L	H	30			15	2		74		25548	4-2.25" Ø, 30" circle	
2240 2373 6 5 4 5 7 7 7 7 7 7 0 0 0 0 0 0 0 0 0 0 0 0 0		2004 223.	5 STEE		3152	_	6.25' x 5' T	24" Ø x 0.375"	L	22	30			10	2		142		38991	4-2.25" Ø, 30" circle	
2240 235 6 5 4 7 1 70 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		2004 164.t	37 STEE		2240		6' x 5' T	20" Ø x 0.375"	_	⊢	_	-	0.43/1.87	10	2		144		33415	4-1.75" Ø, 26" circle	
2200 23.6 6.8 ct 2.7 2.0 Ct 0.2376 2 2 2 2 2 2 2 2 2		2004 164.t	37 STEE		2240	_	6' x 5' T	20" Ø x 0.375"	_	┢	_		0.43/1.87	10	2		144		33415	4-1.75" Ø, 26" circle	
18 18 18 18 18 18 18 18		2004 164.t	37 STEE	_	2240	_	6' x 5' T	20" Ø x 0.376"	L	22	28			8	2		118		28116	4-1.75" Ø, 26" circle	
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1800 31 45.44 T 1075 O A O 2070 2 3 3 4 4 4 4 4 4 4 4	15.10001 L	2004 66.5	8 STEE	Ļ	465	29.32	4.5' × 4'	10.75" Ø x 0.307"	L	H	18			8.5	2		56.94		6377.97	4-1.56" Ø, 16" circle	
35.32.8. 30.11 45.4.4T 107.0 0.0.0307 2 15.5 13.9 13.9 13.0 </td <td>15.10001 R</td> <td>2004 66.5</td> <td>8 STEE</td> <td></td> <td>465</td> <td>28.34</td> <td>4.5' × 4'</td> <td>10.75" Ø x 0.307"</td> <td>L</td> <td>H</td> <td>18</td> <td></td> <td></td> <td>8.5</td> <td>2</td> <td></td> <td>26.94</td> <td></td> <td>6377.97</td> <td>4-1.56" Ø, 16" circle</td> <td></td>	15.10001 R	2004 66.5	8 STEE		465	28.34	4.5' × 4'	10.75" Ø x 0.307"	L	H	18			8.5	2		26.94		6377.97	4-1.56" Ø, 16" circle	
1800 23.0 4.5.4.7 10.75 0 0 0 20.2 1.5	15.10002 L	2004 90.5	5 STEE		363.28	30.31	_	10.75" Ø x 0.307"	╄	۰	18	L		2	2		21.71		6104.6	4-1.56" Ø, 16" circle	
1360 23 4 × 4 T 15 0 × 10.25T 23 14 26 0.74 215 21	5.10002 B	2004 90.5	5 STEE	L	363.28	30.31	4.5' × 4'	10.75" Ø × 0.307"	╀	۰	18	ļ		8.5	2	Ī	21.71		6104.6	4-1.56" Ø. 16" circle	
1300 23 4.4.47 16.0 0.0 0.297 3 4 4 5 6 0.14 0.29 5 6 5 5 5 5 5 5 5 5	ANCHESTER	HAMPTON :	4163						4	1	1	1			1	1					
1360 28.5 4.x4 1.6 0 0.025 3 14 24 10 10 10 10 2 2 10 322 325 3490 4.2 0.15 0.44210 10 10 10 10 10 10 10	5 10001 1	2004 133	STEE	634	Н	_	4' x 4' T	20" Ø x 0 25"	3	14	Н		-0 16/2 32	8.5	0	285	39.5		3998	4-2" Ø 20" square	
1840 25.75 4.x57 16 0.x0.287 3 5 16 26 0.78 3.72 0.142.1 7.5 2 7.0 6.7 7.0	5 10001 E	2004 135	Z Z	234	┿	-	T.V.V.	18" Ø v 0 25"	, ,	1 4	_		0.102.02	G 4	1 0	130	30.0	Ì	3490	4-2" Ø 20" collara	
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6800 25 4 x 4 T 1 i i i i i i i i i i i i i i i i i i i	5 10002 B	2004 177	STEF	739	┿	-	4'×5'T	16" Ø x 0 25"	1	2 4	_		-0.14/2.6	2.5	1 0	205	36		3509	4-2" Ø 18" sollare	
13042 11.5 4.5 x 4.5 1.5 1.5 \text{ 1.	7.11 L	2004 133	STEE	72	┿	+	4' × 4' T	16" Ø x 0.281"	╀	t	_	3.53	-0.13/2.24	8	2	530	72.7		8276	4-2" Ø. 16" square	
	77.11 R	2004 133	STEE	72	┰	-	4' x 4' T	16" Ø x 0.25"	L	t	1	72 3.53	-0.13/2.24	8	2	530	72.7		8276	4-2" Ø, 16" square	
	DE 1	1																			
1.05 1.05	15.10001 L	2004 118	5 STEE	7	1304.2		1.5' x 4.5' ⊤	14" Ø x 0.375"	L	Н			-0.07/1.88	7.5	2	315	73		13512	4-2" Ø, 22" circle	
	15.10001 R	2004 118.	5 STEE	7	1304.2	27.5	4.5' x 4.5' T	16" Ø x 0.375"	Ĺ	H	-		-0.07/1.88	7.5	2	315	73		13512	4-2" Ø, 22" circle	
	15.10002 L	2004 125.	5 STEE	_	1285.44	22.5	4.5° × 4.5° ⊤	14" Ø x 0.375"	L	Н	-		-0.24/2.02	8	2	320	71.6		12960	4-2" Ø, 20" circle	
12 ALUM 626 613 630 62 613 630 62 613 630 62 613 630 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 613 62 62 613 62 62 62 62 62 62 62 6	15.10002 R	2004 125.	5 STEE	7	1285.44	20.5	7.5' x 4.5' T	14" Ø x 0.375"		Н	_		-0.24/2.02	8	2	320	71.6		12960	4-2" Ø, 20" circle	
ALUM, 626 6138 30.25 6 x x d	ONCORD P48(H6-																			
ALUM ASEA 813 8 30.25 8 * × 8* T 10° 0 × 0.05* 9 9 9 9 9 9 9 9 9 9 9 9 10° 0 × 0.05* 9			H'INN			30.25	8' x 8' T	12" Ø x 0.5"												4-1.75" Ø, 17" circle	MJZ/TMH
ALUM 459 596.7 30.75 12.0 × 0.05	15.0005 R	2005 128	. ALUN			30.25	8' x 8' T	12" Ø x 0.5"												4-1.75" Ø, 17" circle	MJZ/TMH
The color The	15.0007 L	2005 142	ALUN			30.75		12" Ø x 0.5"												4-1.75" Ø, 17" circle	MJZ/TMH
STEEL 305 22 35 35 12 18 0.47 22 0.021.91 8 2 0 22.55 15 155.0, 13333° square STEEL 306 397.8 32.7.3 3.5 x 3.5	15.0007 R	2005 142	ALUN		П	30.75		12" Ø x 0.5"		_										4-1.75" Ø, 17" circle	MJZ/TMH
2005 94.5 STEEL 306 39.78 27 35.x3.5°T 10.75°O x 0.307° 2 3 4 12 18 0.47 2.29 10.2019 1 8 2 2 5 0.25 15 195 1950 4-1.5°O, 1.3333° square 2005 94.5 STEEL 306 39.78 27.5 S.5.x3.5°T 10.75°O x 0.307° 2 2 2 3 12 18 19 19 19 19 19 19 19 19 19 19 19 19 19	NFIELD - LEBA	NON 14254																			
2005 94.5 STEEL 306 397.8 32.75 (10.75°0.×0.307* 2 3 12 18 0.47) 222 0.0021.31 8 2 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.31 8 2 2 0 0.021.32 333 square 2005 135 STEEL 492 1680 27.5 4.x4T 12.75°0.x0.23* 2 1.11 12 24 0.59 287 1185 5TEEL 45 89 85.7 STEEL 45 80 85.7 STEEL 4					┪			10.75" Ø x 0.307"	Ц	\forall	_		0.02/1.91	8	2	0	22.65	15	1950	4-1.5" Ø, 1.3333" square	ABH/RLK
2005 135 STEEL 492 1680 28.55 4"x4T 18"0 x 0.25° 2 14 22 8 8 2 188	15.10001 R	2005 94.:	STEE		\neg			10.75" Ø × 0.307"	4	12	\neg		0.02/1.91	8	2	0	22.65	15	1950	4-1.5" Ø, 1.3333" square	ABH/RLK
PRTH AMACHIA STORING TOWARD TO THE TAWARD TOWARD	15.30001	2005	4	4	╛				\exists	4	1	4			1	1	1				
2005 155 STEEL 492 168 2 166 62.3 7534 4-2° 0.16° square 2005 155 STEEL 492 1680 25.5 4×4.7 18° 0×0.25° 2 14 24 1 2 1 4 2 166 6.23 7534 4.2° 0.16° square 2005 143 STEEL 510 1760 28.5 4′×4.5 1 2 1 4 2 1.1 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 2 1 4 4 2 1 4 3 4 4 3 4 4 3 4 4 4 4 4 4 <td>AMPTON - NO</td> <td>чтн намрт</td> <td>ON 13760</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>ŀ</td> <td></td> <td></td> <td></td> <td>ŀ</td> <td></td> <td>ŀ</td> <td></td> <td></td> <td></td> <td></td>	AMPTON - NO	чтн намрт	ON 13760							-	ŀ				ŀ		ŀ				
2005 143 STEEL 49 754 44 754 44 754 42°0,18° square 2005 143 STEEL 180 27.5 4×4.5 1 20°0 × 0.02° 2 14 2 4 1 2 1 4 2 1 4 2 1 4 1 2 1 4 1 2 1 4 1 4 1 4 6 <td>15.10001 L</td> <td>2005 13</td> <td>STEE</td> <td>L 492</td> <td>1680</td> <td>26.75</td> <td></td> <td>18" Ø × 0.25"</td> <td>2</td> <td>14</td> <td>22</td> <td>1</td> <td></td> <td>8</td> <td>2</td> <td>122</td> <td>62.3</td> <td></td> <td>7534</td> <td>4-2" Ø, 18" square</td> <td></td>	15.10001 L	2005 13	STEE	L 492	1680	26.75		18" Ø × 0.25"	2	14	22	1		8	2	122	62.3		7534	4-2" Ø, 18" square	
2005 143 STEEL 510 7760 28.5 4 '.4.5'T 200 'x 0.22°T 2 14 24 0.39 3.2 0.186 7.5 2 118 3.5 2.0 4.055 4.2°C 0.20°c quare AFTINGALIA STREEL 2005 1.3.5 STEEL 4.35 800 27.25 4 '.4.4.5 1.11 1.2 24 0.39 2.87 -0.11.56 6.5 2 1185 28 16.5 1887 4-7.75'0.16' circle 2005 7.3.5 STEEL 4.35 800 27.25 4 '.4.4T 12.75'0.x0.23" 2 1.11 1.2 2.87 -0.01/1.56 6.5 2 1185 28 16.5 1887 4-1.75'0.16' circle 2005 2.35 STEEL 4.35 800 27.25 4'.47 1.25'0.x0.23" 2 1.11 1.2 2.87 -0.01/1.56 6.5 2 1185 28 16.5 1887 4-1.75'0.18' circle 2005 <	15.10001 R	2005 13	STEE	L 492	1680	27.5		18" Ø × 0.25"	2	14	22	_		8	2	166	62.3		7534	4-2" Ø, 18" square	
2005 73.5 STEEL 435 800 28.5 4.4.4.7 12.75°0.x0.237 2 1.11 12 24 0.59 12.8 0.011/1.56 6.5 2 118.5 28 14.8 101 8833 4-2°0.20°0.square 4.2°0.20°0.square 4.2°0.2	15.10002 L	2005 140	STEE	L 510	1760	28.5		20" Ø × 0.25"	4	14	54			88	2	118	32	50	4055	4-2" Ø, 20" square	
PHTSMOUTH DOVER HOOPERTER 1447 2005 73.5 STEEL 435 800 28.25 4"x4"T 12.75"0 x 0.33" 2 1.11 12 2 1.05 0.011.56 6.5 2 118.5 28 16.5 1867 4-1.75"0, 18" circle 2006 73.5 STEEL 435 800 28.25 4"x4"T 12.75"0 x 0.33" 2 1.11 12 2 1.05 0.011.56 6.5 2 118.5 28 16.5 1867 4-1.75"0, 18" circle 2006 73.5 STEEL 435 800 28.25 4"x4"T 12.75"0 x 0.33" 2 1.11 12 2 1.05 0.011.56 6.5 2 118.5 28 16.5 1867 4-1.75"0, 18" circle 2007 73.5 STEEL 435 800 28.25 8.55 T 14"x4"T 12.75"0 x 0.33" 2 1.11 12 2 1.05 0.011.56 6.5 2 118.5 28 16.5 1867 4-1.75"0, 18" circle 2008 73.5 STEEL 889 885.7 28.75 8.75 14"x4"T 12.75"0 x 0.33" 2 1.11 12 12.75"0 x 0.35" 2 1.11 12 12.75"0 x 0.35" 2 1.11 12 12.75"0 x 0.35" 2 1.11 12.75"0 x 0.35" 2 1.11 12.75"0 x 0.35" 2 1.11 12.75"0 x 0.35" 2 1.35	15.10002 R	2005 14	STEE	L 510	1760	28.5		20" Ø x 0.25"	4	50	54		0/1.86	7.5	5	321	44.8	101	8833	4-2" Ø, 20" square	
ZOOD 73.5 STEEL 43.5 SECTION A.2.5 CONTINUE B.S. CONTINUE A.2.5 CONTINUE B.S. CONTINUE A.2.5 CONTINUE A.2.5	AMPTON - PO	TISMOUTH	DOVER	ROCHE	STER 1414	_			H	ŀ	-			ŀ	ŀ		ŀ		-		
2005 72.55 STEEL 435 800 27.25 4×4°T 12.75°O×0.375 2 1.11 12 24 0.56 17.55 0.011/1.56 6.5 2 118.5 28 16.5 1867 4-1.75°O, 16°Order 2005 200	5.10001 L	2005 73.:	STEE		┪	\neg		12.75" Ø × 0.33"	4	┪	_	59 2.87	-0.01/1.56	4	2	118.5	88	16.5	1867	4-1.75" Ø, 18" circle	ABH/RLK
895.7 28.75 5×5.5°T 14"0×0.375" 2 4 14 26 0.6 2.91 0.0611.73 7 2 130 35.25 0 3744 42"0,20" circle 895.7 25.5 5×5.5°T 14"0×0.375" 2 4 14 26 0.6 2.91 0.0611.73 7 2 130 35.25 0 3744 42"0,20" circle	15.10001 R	2005 73.	STEE		⊣	_		12.75" Ø x 0.33"	-1	⊣	_	59 2.87	-0.01/1.56	4	2	118.5	58	16.5	1867	4-1.75" Ø, 18" circle	ABH/RLK
885.7 28.75 5 7 5.55 T 14" 0 x 0 x 3.75	DOKSETT TO	CONCORD 1	4099			100	i	2	ŀ	ŀ			2000	[,		200				1
טסטין בטוס טירטיס ויד טירטיסטיט ב יד יד בט טירט בטוס טירטיס יד בטוס טירטיס יד טירטיס יד יד או בט טירטיס יד יד טירטיסטיט יד יד יד או בט יד טירטיסטיט יד יד או בט יד טירטיסטיט יד יד יד או בט יד טירטיסטיט יד יד יד או בט יד טירטיסטיסטיסטיסטיסטיסטיסטיסטיסטיסטיסטיסטיסט	5 10001 E	2005	S C	889		20.73	0 × 0.0	14 Ø x 0.373	4	+	92 92	201	0.06/173	, ^	y 0	130	35.25		3744	4-2 Ø, 20 GIGB	JAT/BLK
		200	5	3		2	- 00	2000	1	1	2	23	000		1	3	23.00	,	5	3	N I I I I

	1	Harror MATU Actual Design BUILT Actual Chien Area														
10 10 11 11 11 11 11 11	Maintain	180 148.3 STEEL 932 1211.6 100 148.3 STEEL 932 1211.6 100 100 12				× £	-	-		ng Footing ht Thick- ness (ft)	Excavation Quantity (CY)	Concrete Quantity (CY)	Structural Fill Quantity (CY)	Rebar Quantity (lbs)	Anchor Bolts per post	Designer/ Checker
March Marc	Mary	106220. 2006 75.69 STEEL 136 176.8 2006 75.69 STEEL 136 176.8 2006 87.25 STEEL 136 176.8 2006 87.25 STEEL 225 292.5 2006 72.88 STEEL 225 292.5 2006 159.5 STEEL 225 292.5 2006 159.5 STEEL 649 843.7 2006 149.5 STEEL 649 843.7 2006 244.25 STEEL 1081 1793	ш	HH	HH	12.5			ш	Ш	117.5	33	25.5	8547	4-1.5" Ø, 24" circle 4-1.5" Ø, 24" circle	MAC/KGK MAC/KGK
1	Mail	2006 75.93 51TEEL 136 176.8 2006 87.25 51TEEL 136 176.8 2006 87.25 51TEEL 136 176.8 2006 72.88 51TEEL 225 292.5 2006 159.5 51TEEL 649 843.7 2006 159.5 51TEEL 649 843.7 2006 159.5 51TEEL 649 843.7 2006 244.25 51TEEL 1081 1799 2006 244.25 51TEEL 24	T :30 07:32 0	10 75" Ø 0 040"	-	404		L	ŀ	ŀ	2 22	ç	0	050	6 4 E" Ø 40 7E" circle	001/11
1 1 1 1 1 1 1 1 1 1	No.	2006 87.25 STEEL 136 176.8 2006 87.25 STEEL 136 176.8 2006 72.88 STEEL 225 292.5 2006 159.5 STEEL 649 843.7 2006 159.5 STEEL 649 843.7 2006 159.5 STEEL 649 843.7 2006 244.25 STEEL 1081 1789 2006 244.25 STEEL 1081 1789	7 75' V 9 25' T	12.7.3 Ø v 0.213	- - -	2.0		┸	+	+	25.55	5 5	o	920	6-1 5" Ø 18-75" circle	90/11
2008 1281 1281 1282	Mail	2006 87.25 STEEL 136 176.8 220.6 72.88 STEEL 225 292.5 2006 72.88 STEEL 265 292.5 2006 159.5 STEEL 649 843.7 2006 159.5 STEEL 649 843.7 2006 244.25 STEEL 1081 1789 2006 244.25 STEEL 1081 1789 2006 244.25 STEEL 1081 1789	3.75' x 3.25' T	12.75" Ø x 0.219"	- -	_			╀	+	147.5	10.5	22	728	6-1,5" Ø, 18,75" circle	JH/JPB
Mail	Main	2006 72.88 STEEL 225 292.5 2006 72.88 STEEL 225 292.5 2006 159.5 STEEL 649 843.7 2006 159.5 STEEL 649 843.7 1-MILTON 14232. 2006 244.25 STEEL 1081 1793 2006 244.25 STEEL 1081 1783	3.75' x 3.25' T	12.75" Ø x 0.219"	-		1.5	┺	╀	╀	147.5	10.5	77	728	6-1.5" Ø, 18.75" circle	JH/JPB
Main	10.00 1.00	2006 72.88 STEEL 225 292.5 2006 159.5 STEEL 649 843.7 2006 159.5 STEEL 649 843.7 1-MILTON 14222 2006 244.25 STEEL 1081 1793 2006 244.25 STEEL 1081 1793 2006 244.25 STEEL 1081 1793	3.75' x 3.25' T	12.75" Ø x 0.281"	-			上	┝	┞	88	12.5	20.5	900.5	6-1.5" Ø, 18.75" circle	JH/JPB
Mail	Main	2006 159.5 STEEL 649 843.7 2006 159.5 STEEL 649 843.7 2006 244.25 STEEL 1081 1799 2006 244.25 STEEL 1081 1799 2006 244.25 STEEL 1081 7092	3.75' x 3.25' T	12.75" Ø x 0.219"	-				L	H	88	12.5	20.5	900.5	6-1.5" Ø, 18.75" circle	JH/JPB
Mail	March State Stat	2006 193.5 SIEEL 649 843.7 -MILTON 14232 -2006 244.25 STEEL 1081 1793 -2006 244.25 STEEL 1081 1793 -2006 244.26 STEEL 1081 7793	3.75' x 3.25' T	10.75" Ø x 0.25"	2 1				7 7 7 7	2	184	19	50.5	2264.5	4-1.5" Ø, 12" square	JH/JPB
No.	Mail	1-MILLON 14232 2006 244.25 STEEL 1081 1793 2006 244.25 STEEL 1081 1793 2006 244.25 STEEL 1081 2032	3.75' x 3.25' T	12.75" Ø × 0.219"	1]	- 1	7 8 7	2	184	19	50.5	2264.5	4-1.5" Ø, 12" square	JH/JPB
Mail	March Marc	2006 244.25 STEEL 1081 1793 2006 244.25 STEEL 1081 1793	F 13 7 11 2	1.50 0 0 10 4	ŀ		1	L	ŀ	0	0.0	200		4007	10 10 10 10 10 10 10 10 10 10 10 10 10 1	OGWOX IN
March Marc	1 1 1 1 1 1 1 1 1 1	2000 234.05 CTEEL 14477 2005.0	5 6 × 4.3 -	18" Ø v 0.25	+		0.70	4	+	v 6	153.5	35.5		4067	4-2 Ø, 16 square	BI KWPS
Mail	Mail	0.00/	375' x 325' T	10 75" Ø x 0 188"	+		0.7.9	_	+	1 0	72.5	18.8		1527	-" Ø "sallare	BIKWPS
State Column Co	Control Cont	2006 324.25 STEEL 1477 2285.8	3.75' x 3.25' T	18" Ø × 0.312"	╀	0.16	0.8		╀	╀	168.5	41.6		7245	-" Ø, " square	RLK/WPS
2000 8875 STEEL 474 616.2 250 3775 4.2227 1075 0.04287 2 2 10 19 0.51 2.23 0.1122.34 9 2 2 956 2.25 11 18435 18435 9 1.5 0.12 cause 2000 8875 STEEL 426 6.262 0.25 175 4.2227 1075 0.04287 2 2 10 18 0.52 2.57 0.1122.34 9 2 2 9 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 2 9 9 197 1.25 1690 5 9 1.25 0.12 cause 2000 1.25 0.12 c	20.00 20.0	4253			4				1	1					-	
10.0 10.0	No. 1	88.75 STEEL 474 616.2	3.75' x 3.25' T	10.75" Ø x 0.25"	L	⊢	0.51	⊢	┡	2	95.5	22.5	11	1843.5	8-1.5" Ø, 12" square	SDF/ACJ
Mary Street 420 State	2007 110 STEEL 420 5646 5625 577 4 529 1 0776 0 6 20 29 2 2 1 1 1 2 2 2 3 4 4 5 5 5 5 5 5 5 5	88.75 STEEL 474 616.2	3.75' x 3.25' T	10.75" Ø x 0.25"	L	⊢	0.51	_	L	2	95.5	22.5	11	1843.5	8-1.5" Ø, 12" square	SDF/ACJ
2000 145 1516 145 24	2007 1455 51E6 420 546 543 5	110 STEEL 420 546	3.75' x 3.25' T	10.75" Ø x 0.219"	L	-	0.52		Ц	L	66	19.7	12.5	1608.5	8-1.25" Ø, 12" square	SDF/ACJ
865. 1435 STEEL 426 5638 75 75 77 1077 0 × 1018° C C C C C C C C C C C C C C C C C C C	Section 14.5 STEEL 426 5638 75 3.75 7.377 10.75 0.0188 1.25 0.0188	110 STEEL 420 546	3.75' x 3.25' T	10.75" Ø x 0.219"		Н	0.52				66	19.7	12.5	1608.5	8-1.25" Ø, 12" square	SDF/ACJ
State 14.55 Street 4.69 50.50 Street 4.69 50.50 Street 4.69 50.50 Street 4.69 Stre	Supplementary Street Accordance Accode Accordance Accordance Accordance Accordance Accordan	143.5 STEEL 426 553.8	3.75' x 3.75' T	10.75" Ø x 0.188"	_	L	F			L					8-1.25" Ø, "	
Substitivity Subs	Control Cont	07 143.5 STEEL 426 553.8	3.75' x 3.75' T	10.75" Ø x 0.188"			L								8-1.25" Ø, "	
MONTHESTER 1989 C	Note Continue Co	1885														
Composition	Non-First First Part Non-First Part	2008														
2008 2008	2008 2008 2008 2008 2009	NCHESTER 13933C				H										
State Stat	2008 Section 1.5 Section 1	2008			2	_	24		11		175	41.35	17.5	2570	4-1.75" Ø, 13.5" square	GME/TSB
1500 1.5	Suppose Supp	2008			2	_	54	+	=	က	175	41.35	17.5	2570	.75" Ø, 13.5"	GME/TSB
2009 115 STEEL	2009 115 STEEL	4501			-	-	ŀ	-		-				ŀ		-
889 145 STEEL	1.5 STEEL	2008			$\frac{1}{2}$		4	$\frac{1}{2}$	$\frac{1}{2}$					1		
2009 115 STEEL 996 26.8 3.75 x 3.25 T 1.25 x 0 x 0.21 g 2.15 to 1.65 to 1.35 square 2009 115 STEEL 996 26.8 3.75 x 3.25 T 1.25 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0 x 0.21 g 2.15 to 1.65 to 1.35 x 0 x 0 x 0 x 0 x 0 x 0 x 0 x 0 x 0 x	1.				ŀ		Ī		ŀ	ŀ						
2009 145 STEEL	2009 145 STEEL	115 STEEL 936	3.75' × 3.25' T	12.75" Ø × 0.219"	+		9.6		-	4	116.5	24.5	11.5	2150	4-1.5" Ø, 13.5" square	SDF/WPS
2009 146 STECL 7331 23.535 3.75 x 3.257 1 L2.75 Ox Oz19T 2 L3 10.5 20.86 13.5 2.566 13.5 2.549 4-1.75 O, 13.5 square 2009 146 STECL 7387 2.836.0 of 4 2.81 2.866 of 18.5 2.856 of 18.5 2.85	14 STEEL 7337 23.55 1.67.7 0.0 0.219 2 1.5 10.5 20.5 1.5 20.5 2.5	2009 115 SIEEL 936	3.75 × 3.25 I	12.75 Ø x 0.219"	+	10.5	0.55	2.73 2.597	- 1	4	116.5	24.5	11.5	2150	4-1.5" Ø, 13.5" square	SDE/WPS
2009	2009 142 SIEEL 143 SIEEL	2009 145 SIEEL 739.7	3.75 × 3.25 I	12.75 Ø X 0.219	+	0.0	0.38	2.87 2.393/	- 1	4	52	73.63	13.0	4627	4-1.5 Ø, 13.5 square	SDE/WPS
THE 18383G 104 STEEL 299 388.7 28.1 3.75'x3.25'T 10.75' Øx.0.188' Z 15 8 18 0.37 1.79 0.25'2.25 1 1 2 37 2.135 12.5 2009 4-1.5' G).12' square 112 STEEL 477 542.1 3.75'x3.25'T 10.75' Øx.0.28' Z 15 8 18 0.37 1.79 0.25'2.25 1 1 2 37 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.37 1.79 0.25'2.25 1 1 2 37 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.37 1.79 0.25'2.25 1 1 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.35' 2.25'S 11 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.35' 2.25'S 11 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.5' 2.44 0.15'2.36 11 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.5' 2.44 0.15'2.36 11 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25' Z 4 10 18 0.5' 2.44 0.15'2.36 11 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25'T 2.44 0.15'2.36 11 2 35 2.135 12.5 2009 4-1.5' O.12' square 112 STEEL 417 542.1 3.07'1 3.75'x3.25'T 10.75' Øx.0.25'T 10.75' Øx.0.25'T 10.75' Øx.0.25'T 10.75' Øx.0.25'T 10.75' Øx.0.25'T 10.75'T 10.75' Øx.0.25'T 10.75'T 10.75'	10620H 2009 2009 2009 2009 2009 2009 2009 2	2009 145 SIEEL /39.7	3.75 × 3.25 I	12.75 Ø x 0.219"	4	10.5	0.48	2.42 2.386,	- 1	4	123	52.65	13.5	5259	4-1.5" Ø, 13.5" square	SUF/WPS
2009 2009 2009 2009 2009 2009 2009 2009	2009 2009 2009 2009 2009 2009 2009 2009	10620H			-	-	-	-		-		-		ŀ		
2009 2009 2009 2009 2009 2009 2009 2009	2009 2009 2009 2009 2009 2009 2009 2009	2009			+	#	1	1	+	1		_		1		
2009 2009 10620K 6 6 6 6 6 7 6 7 7 8 1052 Mode 7 8 1052 Mode 8 8 1052 Mode 8 8 9	2009 2009 2009 2009 2009 2009 2009 2009	2009			+	†	1	1	+	1		1		1		
10620V. 2009 2.000 1.04 STEEL 299 388.7 28.1 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.12 STEEL 417 542.1 20.77 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 417 542.1 20.71 3.75 x.3.25T 1 0.75° 0.x0.28° 2.000 1.2 STEEL 415.2 STEEL 415.	10620K 2009 2009 2009 3009 3009 3009 3009 3009	2009			+	‡	7		+	1		1		1		
105GN 2009	Unbod/Net Unbo	2008			+	1	7	$\left \right $	$\left \right $	4				1		
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NOMESTER 138356 NOMESTER 1289 388.7 28.1 3.75 x 3.25 T 10.75 x 0.x0 188 T 200 1 12 STEL 299 388.7 30.31 3.75 x 3.25 T 10.75 x 0.x0 25 T 200 1 12 STEL 291 38.7 3.5 T 20.7	ANOHESTER 1383364 ANOHESTER 299 3887 28.1 3.75x 3.25T 10.75° 0 x 0.25F 2009 112 STEEL 417 542.1 285 3.75x 3.25T 10.75° 0 x 0.25F 2009 112 STEEL 417 542.1 287 3.25T 10.75° 0 x 0.25F 2009 112 STEEL 417 542.1 287 3.25T 10.75° 0 x 0.25F 2009 12 STEEL 417 542.1 287 3.75x 3.25T 10.75° 0 x 0.25F 2009 2.25F	6002			+	#	#	 	+	1		\downarrow		1		
MONHESTER 1383306. 2009 104 STEEL 299 388.7 28.1 3.75 x.3.25T 1 0.75 0.0.188 2 15 8 18 0.77 2.49 0.1512.89 10 2 62 17.8 11.5 1647 4-1.25 0.17 square 2009 112 STEEL 417 542.1 28.5 3.75 x.3.25T 1 0.75 0.0.25 2 4 10 18 0.37 1.79 0.252.2 1 1 2 8 2 3 5 2.13 1 2 2 3 5 2.13 1 2 2 3 5 2.13 1 2 2 3 5 2.13 1 2 2 3 5 2 2 2 2	MOHESTER 138336. MOHESTER 1289 388.7 28.1 3.75 x.3.25T 10.75 0 x.0.188 2 1.5 8 18 0.77 2.49 0.517.28 10 2 62 17.8 11.5 1647 4-1.25 0, 12° square 2009 112 STEEL 417 542.1 28.5 3.75 x.3.25T 10.75 0 x.0.28 2 4 10 18 0.37 1.79 0.25.28 11 2 8 7 21.35 12.5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 28.5 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.3 14.5 2.8 1 1 2 3 3 5 1.35 12.5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 28.5 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.3 14.5 0 15.2 8 1 1 2 3 3 5 1.3 5 12.5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 30.71 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.5 12.8 0 11 2 3 36 21.3 5 12.5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 30.71 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.5 12.4 0.15 2.8 6 11 2 3 36 21.3 5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 30.71 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.5 12.4 0.15 2.8 6 11 2 3 36 21.3 5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 30.71 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.5 12.4 0.15 2.8 6 11 2 3 36 21.3 5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 30.71 3.75 x.3.25T 10.75 0 x.0.25 2 4 10 18 0.5 12.2 36 21.3 5 2009 4-1.5 0, 17° square 2009 12 STEEL 417 542.1 30.71 3.75 x.0.25 2 4 10 18 0.5 12.5 36 21.3 5 2009 4-1.5 0, 17° square 2009 12 STEEL 415 0 x.0.2 5 2 STEEL 415 0 x.0.2 5 STE	2009			+	#	1			1						
National State 13500 104 STEEL 299 388.7 28.1 3.75 x 3.25 T 10.75 °0 x 0.188 2 1.5 8 18 0.77 2.49 0.51 2.89 10 2 62 77 8 1.5 1647 4-1.25 °0, 12° square 2009 112 STEEL 212 285 3.75 x 3.25 T 10.75 °0 x 0.188 2 1.5 8 18 0.43 1.64 0.172.37 10 2 65 1.78 11.5 1647 4-1.25 °0, 12° square 2009 1.2 STEEL 4.17 542.1 28.5 3.75 x 3.25 T 10.75 °0 x 0.25 ° 2 4 10 18 0.37 1.79 0.25 2.22 11 2 3.75 3.25 T 2.75 °0 x 0.25 ° 2 4 10 18 0.37 1.79 0.25 2.24 0.15 2.89 11 2 3.75 3.25 2.05 4-1.5° °0, 12° square 2.75	1	2009			$\frac{1}{2}$	1	7	+	+	$\frac{1}{2}$				1		
2009 104 SIEEL 299 388.7 28.1 3.5 x 3.25 T 10.75 Ø x 0.188 Z 1.5 8 18 0.77 2.49 C 5.15 8 18 0.77 2.49 C 5.15 8 18 0.77 2.49 C 5.25 C 5.2 C	2009 104 STEEL 299 3887 281 37.578.2327 10.75.0.0.0.188 2 11.5 164 0.77 249 10 2 65 77.8 11.5 1647 4-1.25.0.12 square 2009 112 STEEL 299 3887 2.81 37.578.2327 10.75.0.0.0.12 square 2009 112 STEEL 417 542.1 285 3.7578.2327 10.75.0.0.0.25.2 4 10 18 0.37 17.9 0.25.25.2 11 2 9 5 77.8 11.5 1647 4-1.25.0.12 square 2009 112 STEEL 417 542.1 285 3.7578.2327 10.75.0.0.0.25.2 4 10 18 0.5 12.7 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17		П.		ŀ	ļ		L	ŀ	ŀ				-		
2009 112 STEEL 477 542.1 30.71 3.75 x 3.25 T 10.75 0 x 0.25 T 2 4 10 18 0.37 1.75 0 2.52 S 1 1 2 37 2.13 1.55 1.64 4-1.5 0 x 1.75 square 2009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 0 x 0.25 T 2 1 4 10 18 0.5 2.44 -0.15 2.86 11 2 37 2.13 1.25 2.00 4-1.5 0, 12* square 3.00 4-1.5 0, 12* squa	2009 112 STEEL 477 542.1 30.71 3.75 x 3.25 T 10.75 \0.0 x 0.125 T 2 4 10 18 0.37 1.75 S 2.25 Z 5 4 10 18 0.37 1.75 S 2.25 Z 5 1 1 2 2 37 2.135 1.25 2.009 4.1.5 \0.0 x 0.25 Z 5 2 2 4 10 18 0.37 1.75 S 2.25 Z 5 2 4 10 18 0.37 1.75 S 2.25 Z 5 2 2 4 10 18 0.37 1.75 S 2.25 Z 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	104 SIEEL 299 388.7	П.	10.75" Ø × 0.188"	+	ω (0.77		+	4	29	17.8	11.5	1647	4-1.25" Ø, 12" square	DDI/SDF
2009 112 STEEL 417 542.1 28.5 3.75 x 3.25 T 10.75 0 x 0.25 T 2 4 10 18 0.37 1.79 0.25 2.2 37 21.35 12.5 2009 4-1.5 0, 12 square 2009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 0 x 0.25 T 2 4 10 18 0.5 2.44 0.15 2.86 11 2 36 2.135 12.5 2009 4-1.5 0, 12 square 3 NOHESTER 14838E 2009 1 1 2 36 2 2 3 3 2 2 3 3 3 3 3 3 3 3 3 3 3	2009 112 STEEL 417 542.1 28.5 3.75 x 3.25 T 10.75 Ø x 0.25 T 2 4 10 18 0.37 1.79 0.25 2.22 11 2 37 21.35 12.5 2009 4-1.5 Ø, 1 ² square 2009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 Ø x 0.25 T 2 4 10 18 0.5 2.44 Ø 0.15 2.86 11 2 36 21.35 12.5 2009 4-1.5 Ø, 1 ² square 10.009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 Ø x 0.25 T 2 4 10 18 0.5 2.44 Ø 0.15 2.86 11 2 36 21.35 12.5 2009 4-1.5 Ø, 1 ² square 10.009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 Ø x 0.25 T 2 4 10 18 0.5 2.44 Ø 0.15 2.86 11 2 36 21.35 12.5 2009 4-1.5 Ø, 1 ² square 10.009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 Ø x 0.25 T 2 4 10 18 0.5 2.44 Ø 0.15 2.86 11 2 36 21.35 12.5 2009 4-1.5 Ø, 1 ² square 10.009 112 STEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 Ø x 0.25 T 2 4 10 18 0.5 2.44 Ø x 0.15 2.86 T 1 2 36 21.35 12.5 2009 4-1.5 Ø, 1 ² square 10.009 112 STEEL 412 STEEL 41	104 SIEEL 299 388.7		10.75" Ø×0.188"	4	80	0.43	- 1	4	4	8	17.8	11.5	1647	4-1.25" Ø, 12" square	DD1/SDF
EEL 417 542.1 30.71 3.75 x 3.25 T 10.75° Ø x 0.25° 2 4 10 18 0.5 2.44 -0.150.286 11 2 36 21.35 12.5 2009 4-1.5° Ø, 12° square	FEEL 417 542.1 30.71 3.75 x 3.25 T 10.75 0 x 0.22 2 4 10 18 0.5 2.44 -0.15/2.86 11 2 36 21.35 12.5 2009 4-1.5 0.12 square 4-1.5 0.12 square	112 STEEL 417 542.1		10.75" Ø x 0.25"		-	0.37				37	21.35	12.5	2009	4-1.5" Ø, 12" square	DDT/SDF
MANCHESTER 14633E 2009		EEL 417 542.1	I. I	10.75" Ø x 0.25"	Ц	Н	0.5		Н	Н	36	21.35	12.5	2009	4-1.5" Ø, 12" square	DDT/SDF
2009		NCHESTER 14633E														
		2009			\dashv				-	\rfloor						

	Designer/ Crecker	xxx/xxx	xxx/xxx	xxx/xxx	xxx/xxx	- OV/02	JER/ACJ	JER/ACJ	JER/ACJ
	Anchor Bolts per post	4-1.25" Ø, 10.5" square	4-1.25" Ø, 10.5" square	4-1.25" Ø, 12" square	4-1.25" Ø, 12" square	4 4 0E" Ø 40 E" 0011020	4-1.25 Ø, 10.5 square	4-1.5" Ø, 12" square	4-1.5" Ø, 12" square
	Rebar Quantity (Ibs)	1030	1030	3042	3042	1000	9001	1434	2065
	Structural Fil Quantity (CY)	7.8	7.8	18.7	18.7	0 0	5.0	8.6	11.6
	Concrete Quantity (CY)	22.3	22.3	36.6	36.6	ų	15.1	21.6	24.8
	Excavation Quantity (CY)	71.3	81.7	143.8	143.8	C.	26.2	77.6	87.2
	Footing Thick- ness (ft)	H	3	Н	2	ŀ	7 6	╀	Н
Jala	max Footing Height (ft)	⊢	10 10	Н	.92	H	82 7	2.09 7.5	Н
. 6	eY Qmin/Jmax (ft) (ksf)	_	1.67 -0.08/2.68	-	2.19 -0.08/1		2.0.11/2.72		2.9 -0.16/1.71
Sign Bridge Footing Data	(£)	0.57	0.57	0.53	0.53	0 40	0.43	0.68	0.87
<u> </u>	X (f) Y	⊢	12 13	Н	12 16	Н	0 0	+	Н
500	Pressur e	⊢	1.5	Н	3	ŀ	יז כי	╀	2
	Туре		0.219" 2		0.188" 2	100	0 188" 2	0.219" 2	0.219" 2
	Be-J	8.625" Ø x	8.625" Ø x	10.75" Ø x 0.188"	10.75" Ø x	2000	8 625" Ø x	10.75" Ø x	10.75" Ø x
	Arm	.5' x 3.25' T	.5' x 3.25' T	3.5' x 3.25' T	.5' x 3.25' T	T :30 0C: T	75' x 3 25' T	75' x 3.25' T	3.75' x 3.25' T 10.75" Ø x 0.219"
	Height (ft)	_	19.39	-	27.18 3	00 30	24.44	22.35 3.	25.85 3.
	Design Sign Area (ft²)	469.3	469.3		518.7		390	Т	694.2
	"L Actual Sign Area (ft²)		ᆫ	EL 369	Ⅎ	ŀ	300	1	ш
מוונב	Span MAT'L (ft)	13933E 38 STEE	88 STEEL	100 STEEL	00 STEEL	13933H	84 STEEL	Т	
eler	YR. S	NCHESTER 2013	2013	2013 1	2013	NCHESTER 2014	2014	2014	2014
For Reference Only:	Description	SALEM TO MANCHESTER 13933E 615.10001 L 2013 88 S'	615.10001 R	615.10002 L	615.10002 R 2013 100 STEE	SALEM TO MA	615.10001 L	615.10002 L	615.10002 R

Description YR. BUILT	LT Span	MAT'L	Actual Sign Area (ft²)	Design F Sign Area (ft²)	Height (ff)	Arm	бет	Type	Soil Pressur e (tsf)	× £	(f) eX	(¥ e≼	Omin/Omax (ksf)	K Footing Height (ft)	Footing Thick- ness (ft)	Excavation Quantity (CY)	Concrete Quantity (CY)	Structural Fill Quantity (CY)	Rebar ty Quantity (lbs)		Archor Bolls per post	Designer/ Checker
HOLDERNESS - PLYMOUTH 11849 615.20001 2006 32.5 ST	YMOUTH 1	1849 STEEL	72		21.25	3,×3,⊥	18" Ø x 0.375"	1 1		0	0 0.48	0.73	0.12/2.44	╢┝	I L	78.7	15.1	0	1241	-	8-1.75" Ø. 24" circle	BLK/WPS
	2006 21.5 STEEL	STEEL	72	93.6	22.3	3'×3'T	18" Ø x 0.25	-	2			1.57	-0.06/1.65	6.5	2	47	12.3	0	1051	\perp	8-1.5" Ø, 24" circle	RLK/JWP
615.20003 200	96 28	STEEL	64		22.75	3,×3,1	18" Ø × 0.312"	1 1	4	0.1	0.1 0.55	1.38	0.09/1.39	н	Ц	58.7	15.7	0	1301	Н	" Ø, 24" circle	RLK/JW
HOOKSEII 12537 615.20001 200	16 36.4	STEEL		151.1	23	3,×3,⊥	18" Ø x 0.5'	-	2.5	14.8	1.5 0.65	1.62	-0.01/1.64		_	59.51	16.48		1263.9	L	8-1.75" Ø, 24" circle	JB/TAF
П	2006 47.9 STEEL 184	STEEL		—	25.4	3.5' × 4' T	30" Ø × 0.37		3	14.8	14.8 18.1 0.87	1.84	0.03/1.58	6.07	1.97	ш	24.33	33.1	1861.8	Ц	3-2" Ø, 36" circle	JB/TAF
5.20001 200	22C 16 51.67	51.67 STEEL	225	292.5 21.75	21.75	4' x 3.5' T	30"Ø×0.344"	1	-	12.5	12.5 17.5 0.86 2.37	3 2.37	/1.887	_	2	49.5	11.5	6.5	1206.5		6-2.25" Ø. 36" circle	JH/JPB
ANCHESTER - CC	NCORD 14	096B			4			1						┨				4				
5.20001 20C	16 52	STEEL 374.5	374.5	486.85	ш	4' x 3.75' T	30" Ø x 0.5	-	-	_		ш	-0.01/1.98	Ц	2	163.3	36.7	36.3	3614	Ц	12-2" Ø, 36" circle	WPS/SDF
615.20002 2006	96 40	40 STEEL 136 176.8 23.75	136	176.8		4'×3'T	20" Ø x 0.344"	- 4	1.5	10	14 0.76	0.76 1.49	-0.11/2.54	6	2 0	67.1	17.2	ig	1138	\perp	3-2" Ø, 24" circle	WPS/SDF
1832	45.25	SIEEL	4,05.5	61.726	_	4 × 3./0	30 XX V.3	┨	67:	2	2	6.5		10.5	4				4	CZ-1-91	w, iu square	WP5/SL
616.1 2007 60 STEEL	09 20	STEEL	П	26.25	21	14" x 0.25" P	17" Ø x 0.25"	5" 2	Ц	Ħ	H	Ц		Ц	Ц		L		Ц	L		TOO,
EENE - SWANZEY	10309H										-			-				-				
615.20001 2007	27 50	STEEL	327	1	24.41	4' × 3.75' T	30" Ø × 0.344"	., ,	1	#	+	1		4	\downarrow		1	\downarrow	1	6-2.25	6-2.25" Ø, 36" circle	
T		STEEL	33/	1		4' X 3.75' T	30"Ø×0.3/		1	‡	+	1		\downarrow	\downarrow		\downarrow	\downarrow	1	8-2.25	. 0, 36" circle	
615.20003 200		STEF	305	1	-	4 x 3.75 T	30" Ø x 0.34	, l.		‡	+	#		\downarrow	\downarrow			\downarrow	1	8.2.25	8-2-25" Ø 36" circle	
sc Eng District 3 1.	832H	1	200				100 × 20 00			1										2:50	5,0	
616.1 2007 60 STEEL	09 20	STEEL	Γ	26.25 21	21	14" × 0.25" P	17" Ø x 0.25"	2	L	F	F	L		L	L		L	L	L	L		TQQ/
STATEWIDE 14253								l ⊦			1 6											
615.20001 2007	77 46.5	46.5 STEEL	244 317.2	317.2	24.75	4'×4'	30" Ø × 0.344"	-4"	ω 4	13	19 1.04		1.94 -0.083/1.8/8	× ×	~ ~	119	37	16	2027	+	6-2.25" Ø, 36" circle 8-2.25" Ø. 36" sallare	SDF/ACJ SDF/ACJ
-											2									-		
615.20001 2008	98 20	50 STEEL 210	210	273	26.5	4' x 3.5' T	30" Ø x 0.375"	5" 1	4	14	22 1.0.	1.8	14 22 1.07 1.8 0.03/1.19	5.5	2	06	29.3	0	3202	Ц	6-2.25" Ø, 36" circle	JAS/DDT
SALEM TO MANCHESTER 13933C	ESTER 139	330			-		-	-		-	9			-	,	000	407	8	0101	-	elenie "Oc So	DATE
5.20001 L 200 5.20001 P 200	20 0	1	1	1	\dagger			- -		ο έ	27 8	1		=	N C	750 250	42.7	R 6	2020	+	8-2.25 Ø, 35 circle	GME/TSB
Ξ,	JESTER - L	SUDONDE	RRY - ME	RRIMACK	115121			1		-	77	1			7	250	45.7	03	000	4	S, Solicies	
615.20001 2009	37	STEEL	196	254.8	_	4.5' × 4.5' T	30" Ø × 0.37.	5" 1	3	⊢	⊢	2.71	0.136/1.24	_	L	136	27	15	2296	L	5" Ø, 36" circle	L
615.20002 200	40	STEEL	186			4.5' × 4.5' T	30" Ø × 0.375"	5" 1	ဗ	-	Н	2.52	0.176/1.203		2	72	27	15	2296		12-1.75" Ø, 36" circle	
5.20003 200	60	53.5 STEEL		439.4	29.74	5' x 5' T	36" Ø × 0.5"		1.5	17	22 0	2.87	0.157/1.225	5 7.5	2	193	38	21	3570	Ц	16-2" Ø, 42" circle	
CONCORD 15389	-	- LULIO	ļ			1100	0 00	ŀ		1	200		0,10,	L	ŀ	107	, ,	,	7000	1000		TAU LOO
5.20001 2009	9 40	SIEEL	1	2/0.4	27.25	3.75° × 3.25° I	26" Ø × 0.32	2	20	11.5	.8.5 0.92	0.92 2.15	-0.165/2.0/9	7.75	N	105	22.1	12	2001	6-2.25	6-2.25" Ø, 32" circle	SUF/WPS
CONCORD 13643		30 CTEE!	95.4	330.2	30	75. > 45. +	36" Ø > 0 375"	-	2 62		18	2 00	751 50 00 0 00 00 00 00 00 00 00 00 00 00 0	2 2 2	٥	197	24.7	47	3031	-	16.9" Ø 49" circlo	CDE/ IM/D
OCHESTER 10620			53				2000	_	_		200	2.00	0.0000			┚			500	\downarrow	2, 4	200
615.20001 2009	61				r			F	L	F	F	F		L	L				L	-		L
SALEM TO MANCHESTER 13933G	ESTER 139	33G						-			-								-			
615.20001 2009	99 46	46 STEEL	160	208	24.9	4'×3'T	24" Ø × 0.353"	3	2	Н	16 0.81	_	0.01/2.01	Н	2	86	28.5	0	1354	Н	6-2.25" Ø, 30" circle	DDT/SDF
П	9 20	STEEL	160		29.1	4'×3'T	24" Ø x 0.35	3 1	1.5	14		1.33	-0.08/2.67	11	5	22	27.4	15	2578		" Ø, 30" circle	DDT/SD
615.20003 200	9 45	45 STEEL 272	272		59.6	4' x 3.5' T	30" Ø × 0.37	- 2	1.5	41	18 1.41	1.83	-0.28/2.87	4	7	157	45	0	3040	4	8.2.25" Ø, 36" circle	DDT/SDF
5.20004 200	9 47.42	STEEL	202.664	263.6	27.31	4'×4'⊤	30" Ø × 0.38	-	1.596	44		1.46	0.02/2.56	Ξ	2	0	45.9	50	4070	4	" Ø, 36" circle	DDT/SDF
615,20001 2010 47.5 STEEL 264 343 24.1	0 47.5	STEEL	264	343		4.5' × 4.5' T	36" Ø × 0.375"		1.5	15	21 0	0.97	1 1.5 15 21 0 0.97 0.71/1.598	6	2	88	42	19	3426	L	12-2" Ø, 42" circle	xxx/xxx
PLYMOUTH - LINCOLN 16079	DLN 16079							1										4	-			
615.20001 2011		26 STEEL	166	216	27.75	216 27.75 3.5' x 2.75' T	T 20"Ø×0.312"	2" 1	1.5	10	16 0.54 1.84	1.84	0/2.22	6	2	100	19.2	11	1238	Ц	3-2" Ø, 26" circle	DDT/WPS
PORTSMOUTH 15892	92	200 200 200 CTEEL 002	300	2000	20 5			Ţ	,	4	4 40	4 70	40 40 470 045/040	20	c	440	0.80	ų,	0300	L	40 0" Q 47" closic	CANCEN A
												2/-	2							_	1	

Designer/ Checker		ACJ/KFD	ACJ/KFD	ACJ/KFD		ACJ/KFD	ACJ/KFD		Walpar	Walpar	Walpar	Walpar	Walpar	Walpar		Walpar	Walpar	VHB/VHB	VHB/VHB		xxx/xxx	XXX/XXX	xxx/xxx		JAS/ACJ	JAS/ACJ	3	CLD/CLD	CLD/CLD	JER/ACJ		
Anchor Bolts per post		6-2.25" Ø, 36" circle	8-2.25" Ø, 36" circle	8-2.25" Ø. 36" circle		8-2" Ø, 36" circle	8-2" Ø, 36" circle 12-1 75" Ø 42" circle		8-2.25" Ø, 36" circle	8-2.25" Ø, 36" circle	8-2.25 Ø, 36 Circle	8-2.25" Ø. 36" circle	8-2.25" Ø, 36" circle	8-2.25" Ø, 36" circle		12-2.25" Ø, 36" circle	12-2.25" Ø, 36" circle	8-2" Ø, 24" circle	8-2" Ø, 27.75" circle		6-2" Ø, 32" circle	6-2.25" Ø, 36" circle	6-2.25" Ø, 32" circle		8-1.75" Ø, 26" circle	9-1.73 Ø, 2.1067 GIGE 8-9" Ø 39" circle	2000	8-2.25" Ø, 36" circle	8-1.75" Ø, 36" circle	8-1.75" Ø, 30" circle		
Rebar Quantity (Ibs)		2429	2426	2412		1700	2090				1					2611	2479	2329	4467	, , ,	2631	2953	2335		1787	7565		3572	4491	1456		
Structural Fill Quantity (CY)		14	16	5 4		12	12											7.3	28.3	,	72	11.3	10.7		8.1	- 0	2	18	21	7.2		
Concrete Quantity (CY)		31.1	31.1	31.6		22.4	28			1	T	T				33.09	45.54	22.1	31.9	000	58.3	29.1	34.4		21.4	27.1		43	59	22.7		
Excavation Quantity (CY)		152	0	104		4	106				T							88.4	0	,	62.4	93.3	102.5		82.7	100	3	146	50	81.9		
Footing Thick- ness (ft)		2	2	2 2		2	α α		2.5	2.5	υ τ	5 10	1.5	1.5		5	е	3	2	,	2 0	v 0	8		2	7 0	·	2.75	2.75	2		
Footing Height (ft)		10	10	12	1	6	4	4	Н		م م	, _	9.5	11.5		7.5	8.5	9.5	10.75	000	+	9.75	┰	1 1	10	2 0		8.75	12.75	12		
Qmin/Qmax (ksf)		0.26/2.19	0.09/2.13	0.07/2.87		-0.07/2.28	-0.09/2.32		0.17/1.68	0.15/1.64	0.08/1.8/	0.07/1.58	0.13/1.94	0.1/2.39		0/1.64			0/2.69	0	0.18/1.88	0.06/2.38	0.21/2.35		0.1/2.31	0.22/20		2.1/	/1.7	3 10.5 13.5 0.9 1.38 -0.19/3.24		
(f) eY		ш	—	1.67		1.76	1.79		П	1	İ	İ	İ					1.59	7.08 5.69	Ī	4 4	1.41	1.33		1.45	1 36	2	1.97	1.17	1.38		
Xe (#)	-	0.87	$\boldsymbol{-}$	0.96	-	0.89	_	-	Ц	4	\downarrow	1	_			4	4	1.22	_	-	_	1.06	-		5 0.62	17.5 0.89 1.29	3	5 0.53	5 0.24	6.0		
× (f)	-	\vdash	\vdash	12 18 19	-	↦	12 20	-	ш	13 27	_	14 25	+	23 13	1 1	14 27	_		15 17	H	12	14 17	⊢		10.5 15.5 0.62	11.5 17	2	16.5 19.5 0.53	6.5 22.	0.5 13.		
Soil Pressur e (tsf)		Н	H	0 4	1	H	5. E	1	Н	+	+	4 C	+		11	1.5		r	1.5	l	†	າ ຕ	t		┪	0 0	1	П	1.5	₋		
Type	1	1		- -	1	-	- -		Н	\dagger	+	\dagger	+			-	-	-	-	-	- ,	- -	-		-	- -	1	-	-	-		
BeT		30" Ø x 0.386"	30" Ø × 0.386"	30" Ø × 0.386"		30" Ø × 0.375"	30" Ø × 0.375"		30" Ø × 0.386"	30" Ø × 0.386"	30. Ø × 0.386	30" Ø × 0.386"	30" Ø × 0.386"	30" Ø × 0.386"		30" Ø × 0.5"	30"Ø×0.5"	20" Ø x 0.375"	12.75" Ø x 0.219"		26" Ø × 0.32"	30" Ø × 0.386"	26" Ø x 0.32"		20" Ø × 0.375"	26" Ø v 0 32"	2000	30" Ø x 0.375"	24" Ø × 0.312"	24" Ø × 0.312"		
Arm		4' x 3.5' T	4' × 3.5' T	4 × 3.5 T		4' x 4' T	4' x 4' 45' x 45' T		3.75' x 3.75' T	3.75' x 3.75' T	3.75 × 3.75 I	3.75' x 3.75' T	3.75' x 3.75' T	3.75' x 3.75' T		3.75' x 3.75' T	3.75' x 3.75' T	3.5' x 3' T	3.5' x 3' T	i d	3.5 × 3.25 I	3.75' x 3.5' T	3.75' x 3.5' T		3.75' × 3.25' T	3.73 × 3.23 I		4' x 3.5' T	4' × 3.5' T	4'×3'⊤		
Height (ft)		22.83	23	25.46		25.75	25.57		ш	-		23.063		26.42		24.42		23.33	22.17	20.00	26.75	28.12	26.33		-	23.40		28.667	27.75	27.06		
Design Sign Area (ft²)		Н	_	332.8	1	218.4				263.6	$\overline{}$	263.6	$\overline{}$	_		244.9		173.9	286		_	304.2	-	1 1	_	2415	_	462.2	288.275	156 27.06		
Actual Sign Area (ft²)		240	256	256		168	+	١.,	н	_	-	202.32	-	202.8		244.9	_	-	220	l	+	234	┰		160	185.75	-	355.5	221.75	120		
MATIL	٥	STEEL	STEEL	STEEL	Ē.	STEEL	STEF	ONCORD	STEEL 202.92	STEEL		STEF		STEEL		STEEL	JEEL STEEL	STEEL	STEEL	žE STITI	SIEEL	STEEL	STEEL	_	STEEL	STEEL	-	STEEL				
Span (ft)	ER 13930	П	т	20 20	ER 14633		35 05	ER TO CO	46	Т	Т	48 4	Т	П	1. [46.75	46.75	50	50	ER 13930	- 1	20 20	20	ER 13930	Т	54 75		49.75 STEEL	34.667 STEEL FR 13933H	40 STEEL		
YR. BUILT	CHEST	2011	2011	2011	CHEST	2011	2011	CHESTE	2011	2011	2011	2011	2011	2011	NCONIA	2012	2012 DOVER	2013	2013	NCHEST	2013	2013	2013	NCHEST	2013	2013	١		2014 NCHESTE			
Description	SALEM TO MANCHESTER 13933D	615.20001	615.20002	Ť	SALEM TO MANCHESTER 14633F	П	615.20002	MAN	DMS-1	7	DMC-4	T		DMS-8	LINCOLN - FRANCONIA 15603	ı	7.11-2 -wington - I	615.20001 2013 50 8	5.20002	MAN	Ť	615.20003	615.20004	MAN	T	615.20002	TER	П	615.20002 2014 34.667 ST	615.20001 2014		



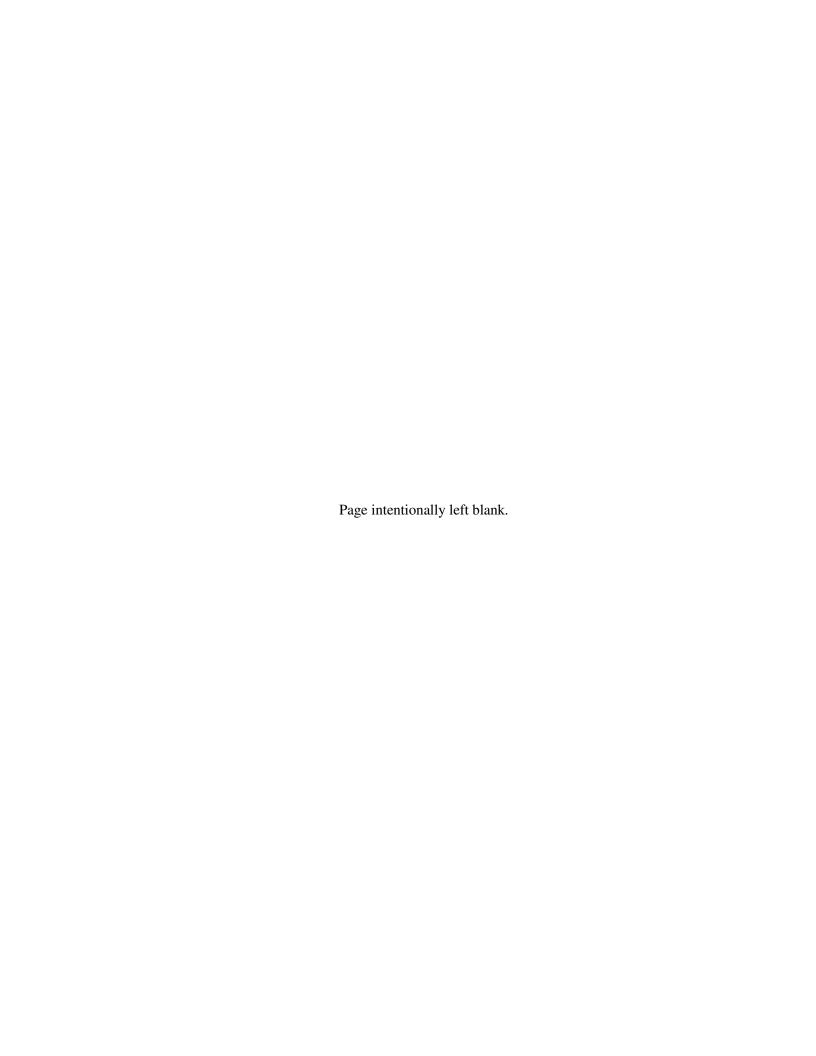
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January 2015 – v 2.0 (Revised August 2019)





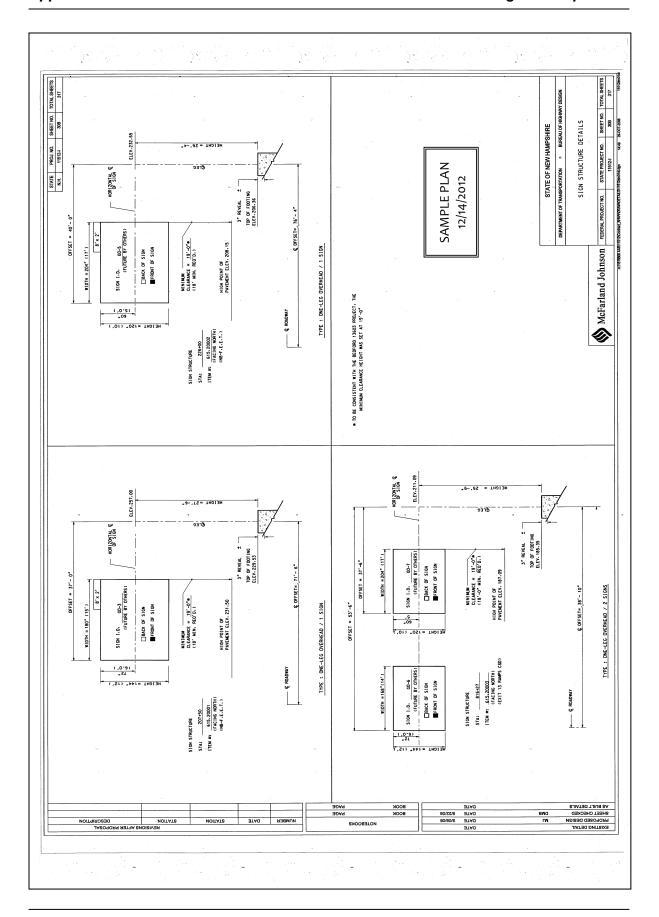




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Appendix 10.3-B2		Stick Figure Sample Plan
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The http://	bridge moun //www.nh.gov	ted sign sup //dot/org/pro	port detail jectdevelc	can be fo	und at NH dgedesigr	IDOT Bridg	je Design (ets/index.h	Detail She tm	ets web pag
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Appendix 10.4-B1	Bridge Mounted Sign Support Detail Sheet
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